# NASA Technical Memorandum 104549

# **LAGEOS Geodetic Analysis--SL7.1**

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D.E. Smith, R. Kolenkiewicz Goddard Space Flight Center Greenbelt, Maryland

P.J. Dunn, S.M. Klosko, J.W. Robbins, M.H. Torrence, R.G. Williamson ST Systems Corporation Lanham, Maryland

E.C. Pavlis, N.B. Douglas University of Maryland College Park, Maryland

S.K. Fricke
RMS Technologies, Inc.
Landover, Maryland

# NVSV

National Aeronautics and Space Administration

Goddard Space Flight Center Greenbelt, MD EAGL JRILITANISLES CLARIS

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## 1. Introduction

# 1.1 Overview and History of Satellite Laser Ranging (SLR) Solutions

This document describes the latest in a series of Satellite Laser solutions, SL7.1, performed at NASA's Goddard Space Flight Center. Through the analysis of globally acquired satellite laser observations, the time-averaged three-dimensional coordinates of the tracking sites are determined for prescribed time intervals. To meaningfully measure tectonic motions of the tracking sites, knowledge of the orbiting LAser GEOdynamic Satellite (LAGEOS) trajectory is required at a level of accuracy approaching that of the laser ranges themselves: one centimeter. The SL7.1 analysis, which represents our fourth global solution, utilized the complete (through 1988) laser tracking data set and incorporates the latest (as of 1987) improvements in force and measurement models.

Starting with the experimental SL4 solution which took place in the early 1980s, the investigation entailed the estimation of annual station coordinates computed from laser tracking data sets then available. Although undocumented, the SL4 results demonstrated that the analysis concept was sound and viable given the status of the then-available hardware and software. When the GEM-L2 gravity model [Lerch et al., 1985] became available (which, for its time, made major advances in the knowledge of the long-wavelength portion of the geopotential), the possibility of computing orbit trajectories of sufficient accuracy to resolve station motions due to plate tectonics was realized. The follow-on solution, SL5, made use of GEM-L2 and additionally, made use of laser normal points (discussed fully in Sect. 4.2) to provide data uniformity [Smith et al., 1985]. Based on laser tracking data taken between 1979 and 1983, estimates of tectonic motion between five of the Earth's major plates were made and reported in Christodoulidis et al. [1985]. The SL5 solution provided the first Satellite Laser Ranging (SLR)-based geodetic confirmation that global plate tectonic motions were detectable and occurring in real time. Additional data, as well as improved models of Earth nutations and solid-Earth and ocean tides were included in subsequent solutions resulting in the SL6 solution [Christodoulidis et al., 1986a]. The SL6 series of annual station coordinate solutions, based on tracking data spanning 1976-84, yielded estimates of horizontal velocities for a dozen sites. Many of these sites were centrally located on major tectonic plates and exhibited SLRdetermined motions strongly resembling those predicted by the global tectonic model developed by Minster and Jordan [1978] from geologic and geophysical data.

The SL7.1 solution realizes, to date, the most dynamically consistent reference frame based on our analyses of LAGEOS ranging data. Nearly 13 years of LAGEOS tracking data have been analyzed to provide *quarterly* solutions spanning the time period from May 1976 (LAGEOS' launch date) to December 1988. This solution uses the GEM-T1 gravity model [Marsh et al., 1988] within which the invariant and tidal parts of the geopotential were estimated simultaneously. The present work is intended to act as a companion volume to *Smith et al.* [1990b] which dealt more with the tectonic implications of the SL7.1 solution. This volume contains details regarding the data reduction, modeling, data and product evaluation steps taken, as well as the ancillary experiments and design decisions made during the analysis leading to the SL7.1 solution presented herein.

### 1.2 NASA's Role in the Development of Satellite Geodesy

Historically, the development of physical models to describe satellite tracking observations has provided a wealth of geophysical information. From the earliest measurements, using instruments which, at times, were no more sophisticated than binoculars and stopwatches (such as that used in the Smithsonian Astrophysical Observatory's project "Moonwatch" [Mueller, 1964, p. 236]), it soon became clear that satellite observations would both improve and change our understanding of the elements shaping our planet and its upper atmosphere. The earliest observed changes in orbits on the order of a few parts in a thousand quickly confirmed and refined the asymmetrical variations of the Earth's gravity field [Merson and King-Hele, 1958, and O'Keefe et al., 1959]. These original determinations of global characteristics of the Earth through the application of space technologies initiated the growth of the subdiscipline of satellite geodesy. These early discoveries inspired developments in satellite tracking technology which have continued since the launch of Sputnik in 1957.

During the 1960s, NASA established the National Geodetic Satellite Program (NGSP) to advance and build a space geodesy program. The purpose of the early program was to establish a fiducial geocentric tracking station network which would unify the world's diverse regional geodetic datums into a single system [Henriksen, 1977]. To support the early requirements of precise orbit determination, constants were estimated and established to describe the central term (GM) and inhomogeneous portions of the Earth's gravitational field. The NGSP began as an effort to provide time-invariant positions of the participating tracking sites utilizing a variety of tracking technologies, such as optical, radio and electro-optical methods. As

observational quality and physical models improved, the notion that estimates of crustal deformation and plate motions on global scales could be obtained via further technological refinement became more popular throughout the geodetic community. This led to the Williamstown Conference [Kaula, 1970] where plans were outlined to give direction towards achieving these goals.

Experiments utilizing satellite laser ranging began in the mid-1960s. From early experiences, improvements in the laser technologies led to the development of a second generation of tracking systems which offered 2-3 decimeter ranging accuracies, further encouraging the geodetic community to work towards the realization of more precise ranging systems. In 1972, an experiment began which was designed to test the capabilities of SLR to detect the effects of plate motion and deformation across California. This experiment, the San Andreas Fault Experiment (SAFE), sought to provide repeated measurements along a north-south, 896-km line straddling this complicated fault system [Smith and Vonbun, 1974]. The early success of SAFE, coupled with advances in the radio astronomic technology of Very Long Baseline Interferometry (VLBI), led NASA to increase the scope of its support for precise station positioning. The Earth and Ocean Dynamics Application Program (EODAP), formulated in 1972, specifically called for the development of centimeter-level VLBI and SLR systems to support geodynamic and oceanographic flight missions [Geodynamics Program Office, 1983, p. 7]. Details on the SLR system development and deployment can be found in Degnan [1985] and Shawe and Adelman [1985].

As an outgrowth of both the EODAP and the Earthquake Hazard Reduction Act of 1977, the NASA Crustal Dynamics Project (CDP) was founded in 1979 under the auspices of NASA's Geodynamics Program. The CDP was responsible for: (1) designing and developing space technology systems to acquire precise geodetic measurements for crustal dynamics investigations, (2) delineating measurement strategies enabling these investigations to proceed, (3) organizing and collecting the observations taken during the measurement program, and (4) supporting the analysis and interpretation of these results [Geodynamics Program Office, 1983, pp. 67-73]. CDP activities have sparked intense international interest in high-precision space-based point positioning. Through the participation and cooperation of over 30 countries, the capabilities of SLR and VLBI for geodetic monitoring of global tectonic processes continues to improve [Coates et al., 1985 and Flinn and Baltuck, 1989]. Outlines for future developments promise improvements in scientific capabilities by expanding network coverage and by strengthening data acquisition strategies [NASA Office of Space Science and Applications, 1991].

# 1.3 The Laser Geodynamics Satellite - LAGEOS

The LAGEOS satellite was designed as a passive target for precise laser ranging. The satellite is a 60-cm-diameter sphere having a mass of 407 kg (Figure 1.1). The outer portion of the satellite is made of aluminum with 426 corner cube reflectors embedded within its surface. Of these, 422 reflectors are composed of fused silica with the remainder being composed of germanium. The satellite has a 175-kg cylindrical inner core made of brass. A complete description of the structural details of LAGEOS can be found in *Cohen and Smith* [1985].

LAGEOS was launched from the Western Test Range in California on May 4, 1976. It was placed into a high-altitude, near-circular orbit having an inclination of 109.8°. At an altitude of nearly 6000 km, LAGEOS experiences a minimal amount of atmospheric drag and is less apt to be perturbed by short-wavelength components of the Earth's gravitational and tidal fields. By minimizing the effects of non-conservative forces and higher frequency geopotential effects, LAGEOS acts as a target which has a highly predictable behavior; a quality that is necessary for the estimation of the motions of the tracking stations.

Through the global acquisition of high-precision laser tracking of LAGEOS, the data can be analyzed to yield information regarding geophysical parameters other than station positions and their ongoing motions. For example, improvements of the long-wavelength portion of the Earth's gravitational field from the analysis of LAGEOS data has been reported by Lerch et al. [1985] and Marsh et al. [1988]. Polar motion has been estimated [Tapley et al., 1985] and high-frequency estimation of polar motion has been investigated and reported by Pavlis et al. [1988] and Caporali et al. [1990]. Tidal parameter estimation from LAGEOS data has been reported by Christodoulidis et al. [1986a]. Although not directly a geophysical parameter, a more physically appropriate model for general relativity and its effects on near-Earth satellites was studied and tested by Martin et al. [1985] and Ries et al. [1988]. Both studies concluded that within the noise limits of the laser measurement system, no significant effects were detectable. Ranging data to LAGEOS have provided a rich source of information from which advances in Earth science and physics have been and will continue to be made.

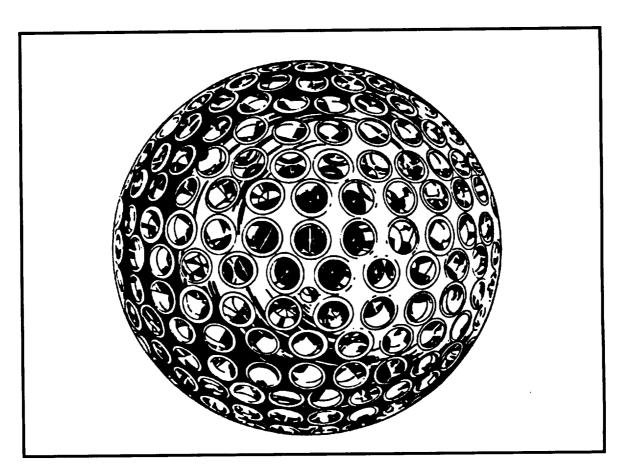


Figure 1.1 The LAGEOS laser reflecting geodynamic satellite launched by NASA.

## 2. Methodology, Definitions, and Rationale

### 2.1 Solution Strategies

#### 2.1.1 Introduction

Satellite geodesy has traditionally been divided into two techniques; one based on geometric methods, and the other on dynamic methods. The geometric method utilizes the satellite simply as a high-flying target. Knowledge of the satellite's orbit is only required to locate the satellite during tracking. The dynamic method treats the satellite as a sensor as it passes through the Earth's gravitational field. Both methods have their merits and difficulties, but, as is explained below, the SL7.1 solution is based on the dynamic method.

#### 2.1.2 Dynamic Satellite Geodesy

The theory behind the dynamic method has its roots in the works of various pioneers in the field of celestial mechanics. However, the specialized theory for close-Earth satellites did not emerge until the launch of Sputnik and the development of high-speed computing machines. Comprehensive texts of the theory have been made by *Mueller* [1964], *Kaula* [1966], and recently by *Schneider* [1988], although the latter is available only in German. Another book, by *Seeber* [1988] shares the same title as Schneider's book and is also in German, but its focus is not so much theoretical as technological.

The dynamic method relies on accurate modeling of the satellite's orbital behavior. The behavior of the class of satellite flown for geodetic purposes is largely dictated by the Earth's gravitational field. Additionally, for high-precision satellite tracking, known perturbing forces on the spacecraft, arising from non-gravitational sources, must be accurately modeled. Knowledge of the location of the satellite along its orbit and the orientation of the orbital plane with respect to the tracking station network, which rotates below on the Earth's surface, are required as a function of time. This provides the *dynamic* description of both the satellite's motion and orbital evolution and provides the connection to the Earth-based tracking system observing the satellite through time.

In the dynamic satellite approach, the solution parameters are estimated via least squares in an iterative manner until the parameters cease to improve (i.e., they have reached a prespecified level of convergence). The parameters which describe the physical situation for the tracking sites on the Earth (i.e. locations, polar motion, etc.), are estimated simultaneously with the parameters used to describe the orbit. In this scheme, the Earth orientation parameters are implicitly referenced to a system based on the LAGEOS orbit plane, and are directly relatable to the adopted model for the dynamical equator and equinox.

Other dynamic solution strategies have been used in various, primarily regional, investigations. For example, the work by Klosko et al., [1990] utilized simultaneous LAGEOS tracking data in a technique dubbed "BEST" (Best Estimate from Simultaneous Tracking) [Kolenkiewicz et al., 1985] to estimate baseline lengths in California and the Baja Peninsula averaged over 5 to 30 days. The technique is purely dynamic, but by using simultaneous data, the effects of orbit error are minimized. A similar technique called "translocation" was used by Stolz et al. [1989] to estimate the baseline rate between sites in California. The technique of "Pseudo Short-Arc" SLR analysis has been developed and used by Sellers and Cross [1990] to estimate baseline lengths in the northeastern Mediterranean. This technique is quite similar to the BEST technique but differs in that a consistent reference frame is maintained through the monthly arcs.

## 2.1.3 The Geometric Approach

The simplicity of the geometric approach, wherein the satellite dynamics are not required for the solution, must be tempered by the reality of whether sufficient tracking is likely to be available. The geometric method is based on triangulation or trilateration principles, or combinations thereof (see, for example, Escobal et al. [1973] and Henriksen [1977], Chapter 7, by H. Schmid) employing strictly simultaneous observations. Within the existing laser tracking data set, the choice of stations that qualify for mutual satellite inter-visibility is limited by deployment schedules and weather conditions which further restrict the overall size of the data set satisfying the condition of simultaneity, particularly for intercontinental station separations. Even when strong geometry is achieved, strictly geometric methods exhibit a strong sensitivity to data quality, both in (a): the ability to detect and separate unavoidable systematic errors and in (b): the difficult decisions for weighting of observations from instruments of differing precision. For these reasons the geometric approach could not be fruitfully applied in the global laser analyses for SL7.1.

## 2.2 Software Implementation

The software system utilized for the dynamic analysis of satellite laser ranging data is GEODYN II, which employs direct numerical integration of the satellite's equations of motion and variational equations in rectangular coordinates. Direct numerical models of a large number of satellite perturbing forces are evaluated at each integration step. Section 3 below describes the force modeling formulation, defines the adopted reference system, and details the measurement correction algorithms. The GEODYN System [Henriksen, 1977, Section 5.4.1, by B. Putney, Putney et al., 1990 and Eddy et al., 1990] is designed to apply a Bayesian weighted least squares algorithm but in practice, all a priori knowledge of the estimable parameters is relaxed so that a priori constraints are not generally applied to the estimated quantities, with rare exceptions.

In order to efficiently implement the required multi-arc capability for spanning many independent orbital arcs of data and for enabling a single simultaneous solution for orbit state vectors, station positions, Earth orientation parameters, tidal coefficients and other elements of the force model, the GEODYN system generates an intermediate data form (a matrix) consisting of a system of normal equations. These matrices are generated for each arc of data and are combined to yield a multi-arc solution in the SOLVE program [Majer, 1986] in which the full solution matrix is created by summing the selected rows and columns in the arc-normals and is inverted. The SL7 series are the first GSFC tectonic solutions to utilize the vector processing computer facility at Goddard: GEODYN II and SOLVE II were radically redesigned for operation on the CYBER 205 computer. The substantial improvement in resource utilization and details regarding program development can be found in Chapter 2 of Marsh et al. [1987].

## 2.3 The Role of Monthly, Quarterly, Annual and Global Solutions

The design of the software system allows considerable flexibility in choosing both the data time-span within which the analysis is to take place and the set of parameters to be adjusted in the solution. As was mentioned above, SOLVE can be directed to invert single-arc matrices as well as matrices formed by combining several subsequent arcs. In the course of the analysis, the arcs are combined in several different ways in order to provide a means to assess data quality and to estimate parameters which are dependent upon data continuous across time.

Initially, the raw range data to LAGEOS goes through a number of steps in order to prepare the data for full analysis (described in Chapter 4). The resulting data set is collected into data groups, called *arcs*, which accumulate all tracking data acquired over a specific time span. The time span chosen for the SL7.1 analysis is typically 30 or 35 days in duration. Error analysis studies indicated that this length of time was appropriate for the estimation of geodetic parameters. Arcs of this length have 180 continuous revolutions and several hundred passes of tracking making them quite stable. These *monthly arcs*, as processed in the form of matrices by GEODYN, provide the basic information for subsequent single- and multi-arc inversions by the SOLVE program. Each monthly arc is separately processed, evaluated, and qualified within GEODYN. If any data within an arc exhibits anomalous results, it undergoes further scrutiny via residual analyses to isolate the cause of the anomalous behavior.

Error analyses show that monthly arcs are capable of yielding precise station coordinates since perturbing forces acting on arcs of this length are well known. This capability is hampered by variations in local weather, system maintenance schedules, and other logistical and unforeseen operational problems. Since 1979, the tracking network has become well-distributed geographically and, for most months, yields accurate monthly positions for the stations having successful tracking campaigns. By combining several monthly arcs into a single solution, a more rigorous solution for all but the very weakest tracking sites can be made. We have chosen to make 3-month solutions, called *quarterly solutions*, to provide the principal means by which we estimate global tectonic motion for the tracking sites.

Just as monthly arcs are used to monitor individual station data quality, we also use annual solutions to assess global force model parameters such as the product of the gravitational constant with the Earth's mass (GM). The annual estimation of GM can yield important information about the variations in overall scale within the solution. However, the most accurate determination of global parameters such as GM, Earth orientation, and Earth and ocean tidal parameters is obtained by combining all monthly arcs into a single global solution. In this scheme, plate motion of the tracking stations is modeled in order to prevent a secular drift of the estimated pole which would occur due to the neglect of plate motion. This global solution yields a continuous Earth orientation series in a continuous reference system as well as a consistent monthly satellite ephemeris, simultaneously with the global geodetic parameters of interest.

In all these solutions, the parameters of chief importance include the tracking station locations in a center of mass system, the polar motion and UT1 variations of the Earth's rotation, and

mean station tidal displacement terms. The gravity field and the Earth and ocean tidal modes affect our solution, as well as arc-dependent orbit vectors, radiation pressure coefficients, and along-track acceleration parameters which are used to empirically model a drag-like effect on LAGEOS. These quantities are either held fixed to values consistent with the most recently accepted models, or are estimated in the least-squares adjustment, as discussed individually in the next chapter.

# 3. Reference Frames, Constants, and Models

## 3.1 Reference Systems and Frames

The analysis of experimental data requires that one maintain the ability to compare the obtained results with those based on other observations or analysis procedures. It is implicit that a framework be defined which is adhered to by all analyzing the data and in all techniques. This provides the common ground on which we can base our comparisons and derive conclusions. This framework is termed the *reference system*.

For any given reference system it is possible to adopt various sets of numerical constants, mathematical models, and formalisms that will realize it, each with a different level of accuracy. Naturally, we are interested in adopting the most up-to-date and most accurate ones available. This adopted set of constants, models, etc., that realizes our preferred framework is known as the *reference frame*.

Not all of the required entities are preset to adopted values. Depending on the kind of data we are dealing with, we may find that these data are quite sensitive to certain parameters that enter the definition of our reference frame. In that case, the data themselves may actually determine improved values which are then more consistent with the data. For example, the LAGEOS laser ranging data can determine very accurately the value of the Earth's gravitational constant, GM. Although a reference value for this parameter has been adopted (through international accords), we have chosen to estimate it. This permits us to study its temporal variation and test the plausibility of theories as to the meaning and consequences of its variation.

The SL7.1 solution focuses on the temporal variation of several physical quantities which are of interest to a wide number of scientific disciplines. The experiments that we analyze are events in the space-time continuum in the sense of the general theory of relativity. We should point out, however, that the formalism adopted for the current analysis follows the classical Newtonian description rather than that of Einstein's geometro-dynamics.

Unlike the reference system which is a congregate of concepts alone, the reference frame comprises several categories of entities discussed below. Models for physical processes contain parameters set to adopted values and/or parameters which are estimated as part of the data

analysis. The gravity field is an example of such a model. The central term of the field GM is estimated, but the remaining terms of the expansion are set to prescribed adopted values. The motion of the Earth's spin axis with respect to the crust is also amenable to different parameterizations. We have adopted the one that happens to be most commonly used, albeit not the only one possible.

Ancillary data sets are usually combinations of mathematical models and numerical values that complement our approximation of the natural environment where the observations take place. The Solar, Lunar and Planetary Ephemerides required in the integration of LAGEOS' orbit are a prime example for this category. We have chosen to use the ephemerides developed by the California Institute of Technology's Jet Propulsion Laboratory Development Ephemeris 200 and Lunar Ephemeris 200 (DE200/LE200) even though other ephemerides exist.

Finally, the way in which the data are analyzed is as important in defining the reference frame, as is the integrity of the data themselves. Dynamic satellite geodesy offers various options; the stability of the resulting reference frame in each case is different, and depending on the phenomena studied, one can have certain advantages over another. In the following subsections we describe the Reference System used in the present analysis of the LAGEOS data, and we discuss in summary the constants and numerical models that realize this system, i.e., the associated Reference Frame.

#### 3.1.1 Reference Systems

In general, it suffices to use a single reference system within which we describe our experiment. Traditionally, and mostly for reasons of convenience, we use two such systems: one that is motionless with respect to the "fixed stars," the *Inertial System*, and one that is motionless with respect to the Earth's crust, the *Terrestrial System*.

The realization of these two systems is only an approximation of the actual concept of either of them. To stress this explicitly, it is common practice to refer to these as the Conventional Inertial Reference System (CIRS) and the Conventional Terrestrial Reference System (CTRS), [Kovalevsky and Mueller, 1981]. The two systems are related to each other through three rotations which are functions of the fourth coordinate, time. We will not differentiate here between proper and coordinate time since, in the classical theory, they are assumed to be identical. The adopted free variable in the equations of motion is measured on the Atomic Time scale and the orientation of the Earth is specified in terms of the Universal Time scale. The

first is chosen because of its uniformity, while the second is periodically stepped to keep it closer to the scale defined by the Earth's actual rotation. With the time coordinate defined, we proceed to the definition of the spatial coordinate system.

The international organization responsible for the definition of astrodynamical reference systems is the International Astronomical Union, (IAU). Our definitions follow as closely as possible those of the IAU. We have strived to maintain this parity by adopting their most recent recommendations every time a new cycle of analysis commences.

Traditionally, astronomers defined reference systems for their use by means of catalogs of repeatedly observed stars. When dynamical theories advanced and the contemporary instrumentation allowed it, the ephemerides of the planets, the Sun, and the Moon were realizations of the first dynamical reference system. The large distances between the bodies warranted that little attention be given to the issue of elaborate force modeling for the equations of motion. The very close approximation of the true motions by such simple point mass models was the main reason these ephemerides were used as stable frames of reference for a very long period of time.

The advent of satellite geodesy offered other options in the choice of the bodies whose orbits define the reference system. Precise tracking of artificial satellites provides an accurate measure of the observer's location relative to the spacecraft. However, the closer the satellite to the Earth, the stronger is the influence of the irregularities of the Earth's gravitational field and atmosphere on its trajectory. This is a drawback for the definition of a reference frame. The geopotential is not perfectly known, and the modeling of non-conservative forces such as atmospheric drag, Earth radiation, Solar radiation, etc., are in most cases incomplete at best. Therefore, the forces which perturb the orbit need to be estimated and they are undoubtedly of significant scientific importance. While this may improve the results, errors will still be present, for the model remains incomplete and imperfect. Clearly not all satellites are of equal use for the definition of a dynamical system despite the fact they may all be useful for other purposes.

The LAGEOS orbit can be determined through highly accurate laser ranging observations, thereby establishing a dynamical reference system which is directly accessible. When the results of the SL7.1 analysis are presented it will be clear that the goals set forth in the LAGEOS mission have been met and most of them surpassed by an order of magnitude. Nevertheless, the long term stability of the system is still limited due to unmodeled very long

period perturbations, especially in the angular elements (node, inclination) which are yet to be fully modeled. As our modeling improves, we find that we more effectively use the satellite orbit as the means to define a dynamical reference system (even though imperfect), which we can access through direct observations from the Earth's crust.

This system is related to the astrodynamical reference systems defined through the planetary ephemerides by a weak link: the relatively small orbital perturbations that the rest of the solar system's bodies have on LAGEOS' trajectory. The astrodynamical system which is realized by these ephemerides is well studied [Newhall et al., 1983, and Lieske and Standish, 1981]. The resulting system will, to a certain extent, violate one of the defining principles of a dynamical system based on the theory of the motion of some bodies in the solar system constructed in such a way that there remains no rotational term in the equations of motion. To reiterate, there are imperfections in the force modeling of LAGEOS' motion which may introduce frame distortions; our system will slowly rotate with respect to the inertial space, and the rate will be a function of the mis-modeled force effects.

Since we cannot define a truly inertial system, but rather a quasi-inertial one, we must associate a date with our definition. We use the IAU-adopted fundamental epoch of Noon January 1, 2000 Julian Ephemeris Date, designated by J2000. The first axis of the CIRS is defined as the intersection of two fundamental planes: the ecliptic and the mean celestial equator. By convention, the positive direction is that which points in the direction of the ascending node of the ecliptic on the equator, that is, the Mean Vernal Equinox of date. The third coordinate axis is perpendicular to the plane of the mean equator of J2000. Lastly, the second axis completes the orthogonal triad on the equator.

As we have already mentioned, the CIRS and the CTRS are related through three independent rotations which are functions of time. In order to study various phenomena that have vastly different origins or magnitudes, and because part of the total rotation is well represented by theoretical models, the total rotation is decomposed into several successive rotations which are all time-dependent. The mean places of the fundamental epoch are related to the mean places at the observation epoch through the *precessional* rotation. The short periodic (relatively speaking) variations of the Earth's orientation in space are modeled through the *nutational* rotation at the observation epoch. Both of these motions are forced and directly attributable to the gravitational torque of the solar system's bodies exerted on the Earth due to its oblateness. At this point, there are no other motions with respect to the inertial space. The interim system we have reached is what astronomers call the "true of date system" and for the sake of

uniformity we shall call it the Celestial Ephemeris Reference System (CERS). It is described in Figure 3.1.

To relate this to the CTRS we must still define the rotations of the CERS with respect to the CTRS. These are: the orientation of the instantaneous equatorial plane, or equivalently, an axis perpendicular to it, the sidereal rotation, and the non-uniform rotation rate of the Earth on the Equator (see Figure 3.2). The sidereal diurnal rotation is modeled through a polynomial in time which describes at any instant the angular separation of the equinox and the conventionally adopted origin of longitudes on the Earth. The first two rotations account for the highly irregular polar motion while the last refers to the spin rate irregularities. Because these motions are "free" responses of Earth, polar motion and Earth rotation variations are, by and large, unpredictable to the required accuracy by any current theory. Therefore, they must be determined through observation. Their estimates orient the observer on the Earth's crust with respect to the CERS as materialized by the satellite's orbit. In fact, an accurate determination of these parameters is one of the goals of this analysis since their temporal variation can provide us with vital additional information about the inner structure and the elastic properties of the Earth.

The axis whose polar motion is "observed" by the various techniques must be uniquely defined and naturally "observable." The definition of this axis - the Celestial Ephemeris Pole (CEP) - has been a controversial issue since the 1970s, (cf. a historical review in [Moritz and Mueller, 1987]), and it is only recently (1984) that the issue has been settled. The IAU-adopted definition for the CEP is that it should have "no periodic diurnal motion relative to the crust (not the mantle) or the CIRS" [Mueller, 1981]. We should note that the CEP is the third axis of the CERS and it is the axis to which our nutation model refers. Since the nutation is derived from a model which is necessarily only an approximation of reality, it is important to choose a model that complies with it in order to conform with the above definition.

#### 3.1.2 Reference Frames

The first international campaign to utilize laser ranging data for the definition of a dynamical system was ISAGEX, the International Satellite Geodesy Experiment. The accuracy of early-1970s ranging systems that participated was between 1 and 2 meters. Since the errors from the gravity field were large at the time, the resulting reference frame had an estimated accuracy of only about 5 meters. Instrumentation, however, has improved tremendously, and our

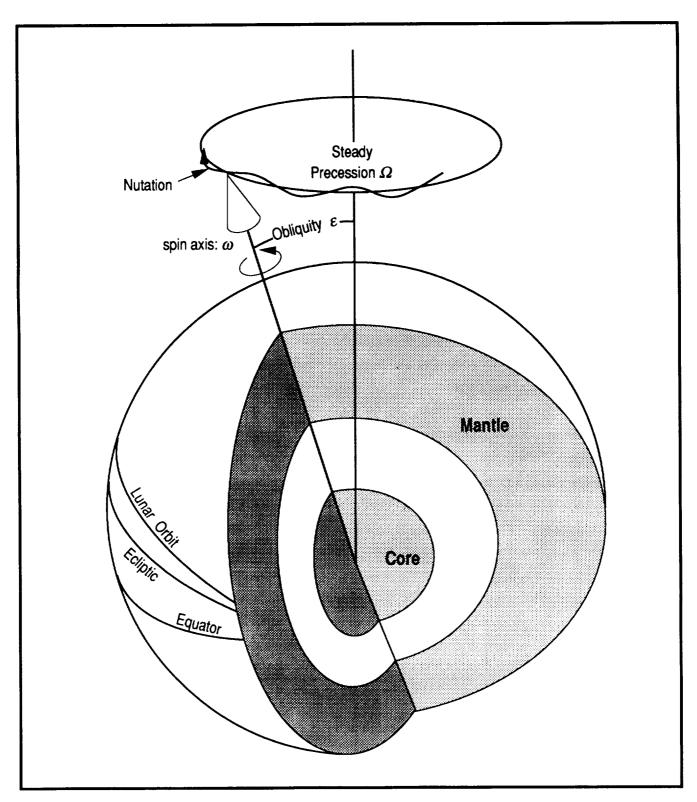


Figure 3.1 Earth rotation in inertial space: Precession and nutation.

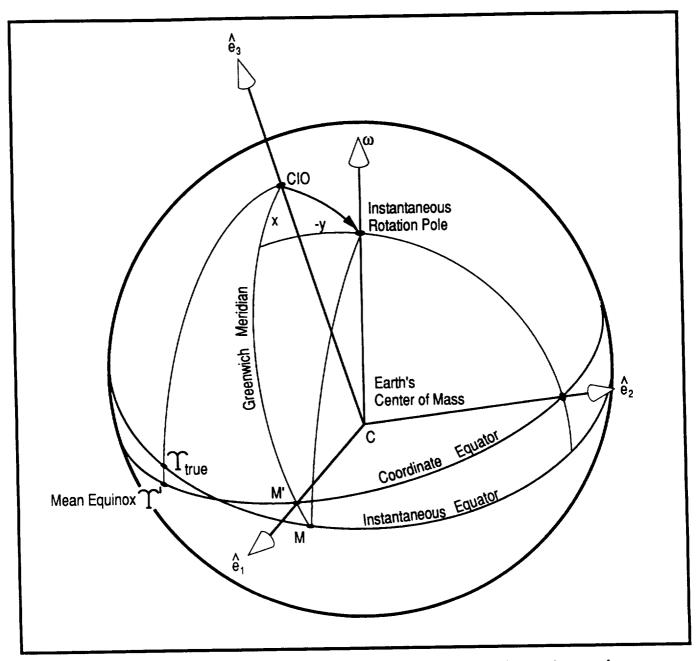


Figure 3.2 The terrestrial system: Polar motion and Earth rotation angles.

understanding and modeling of the gravity field and other forces acting on near-Earth satellites has advanced by orders of magnitude.

One of the most successful recent international campaigns organized for the purpose of studying Geodynamics was MERIT; it covered the period September 1983 through October 1984. MERIT was a program of international collaboration to Monitor Earth Rotation and to Intercompare the Techniques of observation and analysis, [Mueller, 1985]. Tracking of LAGEOS and the

analysis of the collected data were main contributors to its success. Due to the high quality and abundance of data, and the variety of estimated geodynamic quantities, the MERIT campaign has had a major influence on subsequent international efforts in geodynamics.

As part of the preparation for this campaign the "MERIT Standards" [Melbourne et al., 1983] were instituted and applied to a wide range of analyses. Therein one found a collection of constants, models, and formalisms that were used to define the reference frames associated with Project MERIT. Regardless of whether these Standards provided the most accurate or most popular values, their single most important contribution was bringing together in one document the entities one needed to adopt in the process of establishing a reference frame. In most cases, we only have to describe minor deviations from MERIT, rather than re-enumerate every single value required. To a great extent, this accurately describes the standards adopted for the SL7.

#### 3.1.2.1 The Inertial Frame

The adopted definition for the CIRS is that of J2000. This frame is connected to the CERS frame at any instant through the IAU 1976 model for precession [Lieske et al., 1977, and Lieske, 1979] and the nutations of the IAU 1980 model [Wahr, 1981]. The definition of the reference pole for Wahr's model happens to be such that it fulfills the CEP definition consistent with J2000. The obliquity of the ecliptic of date with respect to the reference ecliptic of J2000 is modeled through the IAU 1976 adopted formula [Kaplan, 1981], which is consistent with the adopted model for the precession. The adopted Solar, Lunar and Planetary ephemerides, JPL's DE200/LE200, are also consistent with J2000.

The connection of the CERS with the CTRS involves a model for the orientation of the first axis of one with respect to that of the other: the Greenwich Mean Sidereal Time, GMST. The formula that we have adopted is consistent with the IAU 1976 resolution [Kaplan, 1981, p. 8]. It complies with the definition of the Celestial Equator implied by the above-mentioned formula for the obliquity of the ecliptic as well as the definition of the CEP through Wahr's nutation model.

Application of the CIRS to the CERS transformation defines (as we already noted), an "instantaneously inertial" frame in which the orbit of the satellite is observed. This orbit is the "link" through which the aforementioned models effect the connection between the two frames. We know however, that there are no "bench marks" in space to define the CIRS and

that today's adopted models are mere mathematical abstractions. If we were to reverse the argument about the "orbit link," we could see how the definition of the CIRS is realized indirectly through the dynamics of the satellite orbit. It is therefore clear why such a reference frame is termed a dynamical one.

#### 3.1.2.2 The Terrestrial Frame

The connection of the CERS with the CTRS requires the knowledge of the Earth Orientation Parameters (EOP), namely the variation in the sidereal rotation and the polar motion coordinates. We have already mentioned that the systematic part of the first rotation is given by the GMST formula. To refer this angle to the true Equinox of date we must add to GMST the "Equation of the Equinox," which is the effect of the nutation on the mean Equinox. The resultant angle is the Greenwich Apparent Sidereal Time, GAST. The fact that the Earth rotates with a variable rate about an axis which has an irregular motion with respect to the crust, forces us to determine through observation the remaining portion of the three Eulerian angles.

The observatories which collect the tracking data are fixed on the Earth's crust. The polyhedron whose vertices are the observatories provides a crude approximation of the crust; the denser and more uniform the distribution of the observatories, the closer the approximation. Were the Earth's crust completely rigid, a few stations would suffice. Due to the motion associated with plate tectonics, this is not the case. Monitoring the magnitude and direction of these motions is currently an important task in geodynamics and is of chief interest in this study. Tectonic models exist to describe these motions, but are based mostly on geological data and make simplistic assumptions about the rigidity of the internal plate structure. These models can have large uncertainties associated with them and they reflect average behavior over several million years. Short-term variations can only be determined through direct observation and can provide us with vital information on precursory seismic events with obvious societal implications.

We are in a situation where we have no model demonstrably accurate enough to represent the global tectonic motions present in the tracking network, whose effects are large enough to affect the rest of the parameters that will define the CTRS station positions. The general rule in such cases is to estimate the effect from the data themselves. In fact, to help our solution converge faster, we have adopted as a first approximation the model AM0-2 of *Minster and Jordan* [1978]. The correction to the underlying model is made by allowing the observing station

locations to adjust to new time-averaged positions over a prescribed interval of time. Depending on the purpose of the solution, this interval can be as short as a month or as long as a year, as described in Section 2.3. This procedure, along with the AM0-2 model, accounts for crustal motions within our analysis. We have thus reached the point where a set of piece-wise continuous station positions and an adopted model of crustal motion define our approximation of the Earth's crust.

The satellite dynamics are sensitive to the location of the observatory to the extent that the observatory's position can be determined from its observations along with the satellite trajectory. In particular, the analysis of ranging data to estimate tracking site positions is a problem which theoretically has only one singularity: the definition of the origin of longitudes. It is not necessary then to adopt positions for the "mean" places of the stations, we can simply estimate them from the data themselves. We only need to constrain the longitude of one station to remove the singularity (Figure 3.3). This would suffice for the solution to the definition of our CTRS if it were not for the simultaneous estimation of the Earth orientation parameters. An examination of the range equation in terms of this enlarged set of estimated parameters reveals that a change in the station position can be accommodated by an opposite change of the CTRS with no change in the observation residual itself. To remove this singularity, we need to define the location of the third axis on the already defined zeroth meridian. This can be accomplished through the adoption of the latitude of the already constrained station. One further constraint is required which will remove the rotational degree of freedom of the zeroth meridian plane about its equatorial axis. This can be effected in one of two ways: fixing the latitude of a station which is approximately on the same parallel and 90 degrees away in longitude (Figure 3.4), or fixing the longitude of a station nearly on the same meridian and about 90 degrees away in latitude (Figure 3.5).

We have used both approaches in different test solutions, considering in each case which of the two stations had stronger tracking. The nominally constrained stations adopted were: Greenbelt, Maryland, selected to serve as the primary station (fixing both latitude and longitude), and for the second station we had a choice between either Maui, Hawaii (fixing its latitude) or Arequipa, Peru (fixing its longitude). The applied constraints force these coordinates to change in time with a predefined tectonic motion provided by the AM0-2 model. It can be easily verified that these particular constraints are selected in such a way that the estimated changes in distance due to the tectonic motion between the constrained stations remain nearly unaffected over time.

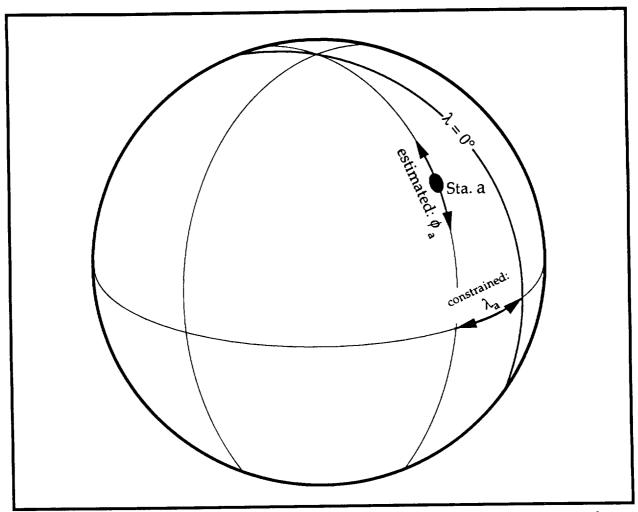


Figure 3.3 Minimal constraint required to establish a CTRS in a solution where Earth orientation parameters are not being estimated.

The initial approximate positions for the tracking stations were the result of the previous cycle of analysis, the SL6 solution. For stations that appeared after 1984, the values were obtained from preliminary solutions within the frame of the SL6 stations. The starting EOP set (the approximation for the estimates), was of mixed origin. For the 1976 through 1979 period we have used the values provided by BIH Circular D, and the same holds for the 1985-86 period. For the 1980-84 period, we have used the pole positions derived from the SL6 cycle of analysis. In all cases the BIH Circular D values were used for Earth rotation variations, described through the UT1-UTC.

The sequential application of the orthogonal rotations described in the last two subsections effects the connection of the CTRS to the CIRS, in other words, the observer's frame of reference to that of the inertial space as it is realized by the orbit of LAGEOS. The final solution which

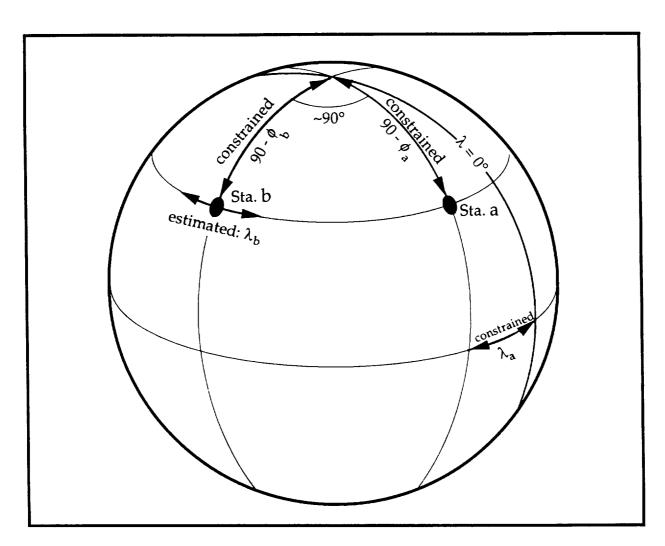


Figure 3.4 Minimal constraint required to establish a CTRS in a solution in which Earth orientation parameters are being estimated. Case 1: two stations on the same parallel.

is presented here, is the result of a second iteration to minimize non-linearity effects. As such, we must point out that these results have been based on using as *a priori*, information which has been derived from the previous iteration. This statement encompasses all of the adjusted parameters with the exception of the arc-dependent solar radiation pressure coefficients and the along-track acceleration series.

## 3.2 Adopted Constants

The following tables list the values adopted for constants that enter into the models used in the reduction of the observations. Only the more important ones have been included. We have

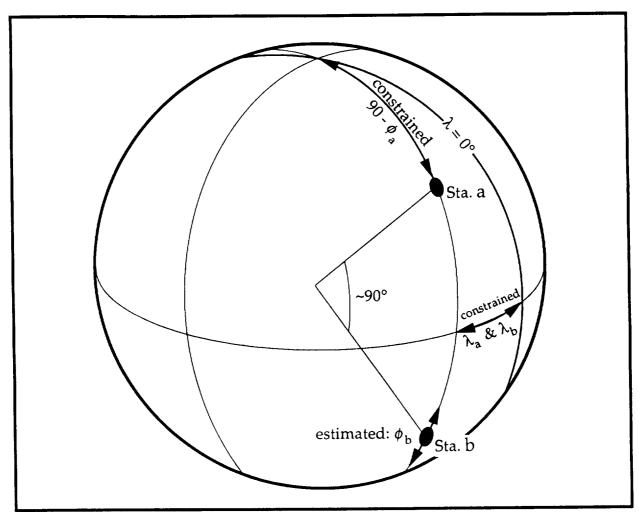


Figure 3.5 Minimal constraint required to establish a CTRS in a solution in which Earth orientation parameters are being estimated. Case 2: two stations on the same meridian.

also avoided repeating numbers which are implicitly embedded in standard models which we have adopted in the whole, e.g., the constants describing Wahr's nutation model, or Lieske's expressions for the precessional matrix.

#### 3.2.1 Astronomical Constants

Speed of light	299792458 m/s
Equatorial radius of the Earth	6378137 m
Flattening of the Earth	1 / 298.257
Mean spin rate of the Earth	0.00007292115 rad/s
Geocentric gravitational constant	$398600.440  \text{km}^3/\text{s}^2$

Ratio of Earth to Moon mass

0.012300034

Ratio of Solar to Earth mass

332946.038

Astronomical unit

149597870660 m

#### 3.2.2 Dynamical Models

Geopotential expansion

GEM - T1 (to degree and order 20)

Solid-Earth tides

Wahr model

Ocean tides

**GEM - T1** 

Radiation pressure at 1 AU

 $0.0000045783 \text{ kg/m/s}^2$ 

Mass of LAGEOS

406.965 kg

LAGEOS cross-sectional area

0.28274 m<sup>2</sup>

LAGEOS reflectance coefficient

1.13

#### 3.2.3 Measurement Model

Troposphere

Marini-Murray model

Satellite center of mass correction

0.24 m

Station tidal displacements

Wahr model

#### 3.2.4 Reference System

**CIRS** 

J2000.0

Planetary Ephemeris

DE200/LE200

Terrestrial time scale

UTC(USNO)

Precession

IAU 1976 (Lieske model)

Nutation

IAU 1980 (Wahr model)

CTRS

Global Solution 11.7 y

Tidal variations in UT1

Yoder model

Tectonic motion model

Minster & Jordan AM0-2

## 3.3 Force Modeling

This section describes the force models of GEODYN and their specific application in the SL7.1 solution. The complete mathematical descriptions are found in *Eddy et al.* [1990].

The numerous forces which accelerate a satellite are naturally classified as conservative potential effects and non-conservative effects. The potential effects modeled include the geopotential due to the static mass distribution of the Earth and the temporally varying geopotential due to the deformation of the Earth by the gravitational forces of the Sun and Moon. The third body effects augment the conventional point mass potential to include the effect of Earth's dominant non-spherical component, C<sub>20</sub>, that is, the "indirect oblateness" effect is modeled.

# 3.3.1 Potential Effects

The static geopotential is typically represented as a series of spherical harmonics by [Heiskanen and Moritz, 1967]:

$$U^{s} = \frac{GM}{r} \left[ 1 + \sum_{n=2}^{n \max} \sum_{m=0}^{n} \left( \frac{a_{e}}{r} \right)^{n} \overline{P}_{nm} (\sin \phi) (\overline{C}_{nm} \cos m\lambda + \overline{S}_{nm} \sin m\lambda) \right]$$
(3.1)

where GM is the gravitational constant of the Earth; r,  $\phi$  and  $\lambda$  are the geocentric distance, latitude, and east longitude, respectively, at the point of evaluation;  $\overline{P}_{nm}(\sin\varphi)$  are the associated Legendre functions of the first kind; and  $\overline{C}_{nm}$  and  $\overline{S}_{nm}$  are the geopotential coefficients, sometimes referred to as the Stokes' coefficients, which represent the inhomogeneous mass distribution of the Earth. The use of the normalized harmonics is indicated by the overbars. To completely represent the geopotential, nmax should be very large. However, for the purposes of modeling satellite behavior, the series can be truncated with minimal loss of accuracy due to the gravitational attenuation with altitude. The evolution of LAGEOS' orbit and the forces acting upon LAGEOS at any one moment are predominantly influenced by the geopotential. The static geopotential model is further augmented with a model describing the dynamically varying indirect tidal potential, which may simply be regarded as the above model with the prescribed astronomic forcing.

The tidal potential adopted is split into two components; the solid body tide potential and the ocean tide potential. The body tide potential is modeled based on the frequency-dependent elastic response of the Earth [Wahr, 1981]. The ocean tide model is based upon the spherical harmonic expansion of a simple surface density layer model. Both of these potentials may be expressed in the standard spherical harmonic form given in equation 3.1, where the coefficients vary with time. However, tidal potentials are more conventionally expressed in terms of

amplitude and phase, where the amplitudes are related to either surface tidal heights (ocean tides) or to their contribution to the elasticity parameter  $k_2$  (for the solid-Earth tides).

The formulation for the tidal potentials in GEODYN is fully documented in *Christodoulidis et al.*, [1988]. The body tide potential is expressed as (for either the Sun or the Moon):

$$U^{b} = \sum_{f} k_{2,f} \overline{A}_{f} G_{D} \frac{3 - m}{3} \left[ \frac{a_{e}}{r} \right]^{3} P_{2m} (\sin \phi) \cos \alpha_{f}^{SE}$$
 (3.2)

and the ocean tide potential is similarly expressed as

$$U^{o} = \sum_{f} \sum_{l,q,\pm} 4\pi G_{D} a_{e} \rho_{o} \left( \frac{1 + k_{l}'}{2l + 1} \right) C_{lq,f}^{\pm} \left[ \frac{a_{e}}{r} \right]^{l+1} P_{lq} (\sin \phi) \cos \alpha_{lq,f}^{\pm}$$
 (3.3)

where

indicates summation over all tidal constituents f in the expression of the tide-generating potential.

 $k_{2,f}$ ,  $\delta_{2,f}$  are the second-degree Love number amplitude and phase respectively, which describe the body response of the Earth.

 $\overline{A}_f$  is equivalent to the Doodson coefficient (given by equation A7 in Christodoulidis et al. [1988]).

 $G_D$  equivalent of the Doodson Constant given by  $G_D = 3\mu_m R^2 / (4a_m^3)$  where  $\mu_m$  is the product of the gravitational constant with the mass of the Moon and  $a_m$  is the semi-major axis of the lunar orbit (likewise for the solar case), R is the mean radius of the Earth.

is the order associated with f which is 0 for the long-period tides,1 for the diurnal tides, and 2 for the semi-diurnal tides.

 $\rho_0$  average density of ocean water.

 $k'_{i}$  load deformation coefficients.

 $C_{lq}^{\pm}$ ,  $\mathcal{E}_{lq,f}^{\pm}$  are the amplitude and phase of the  $(l,q,\pm)$  subharmonic of the ocean tide generated by constituent f.

and where the angular arguments are:

$$\alpha_f^{SE} = (\mp) [(2-2h)\omega * + (2-2h+j)M * + k\Omega *] + m\Theta_g + m\lambda + \pi - m\frac{\pi}{2} + \delta_{2,f}$$
 (3.3a)

$$\alpha_{lq,f}^{\pm} = (\mp)[(2-2h)\omega^* + (2-2h+j)M^* + k\Omega^*] + m\Theta_g + q\lambda + \pi - m\frac{\pi}{2} + \varepsilon_{lq,f}^{\pm} \quad (3.3b)$$

and finally where

 $\omega^*$ ,  $M^*$ ,  $\Omega^*$  are the traditional Keplerian elements for the disturbing body referred to the ecliptic, and the are combinations of factors which map the six Doodson angular

arguments into subscripts suitable for application with the

Keplerian elements of the Moon and apparent Sun.

 $\Theta_{g}$  is the Greenwich sidereal hour angle.

The eccentricity and inclination of the osculating elements of the perturbing body are incorporated in the Doodson coefficient.

Each constituent f is associated with an unique frequency. It should be noted that if

$$k_{2,f} \equiv k_2$$
 
$$\delta_{2,f} \equiv \delta_2$$
 (3.4)

for all f (i.e., the solid-Earth Love number is frequency invariant) (including f=0, see comment below), then the total body tide potential may be simply computed in the time domain using the simple second-degree potential

$$U^{b} = \sum_{d} k_{2} \frac{\mu_{d} a_{e}^{2}}{r_{d}^{2}} \left[ \frac{a_{e}}{r} \right]^{3} \left\{ \frac{3}{2} \left[ \frac{\overline{r}_{d} \cdot \overline{r}}{r_{d} r} \right]^{2} - \frac{1}{2} \right\}$$
(3.5)

based on the point mass attraction of the third bodies and the Earth's deformation given by a constant Love number. Hence,  $\bar{r}_d$  is the geocentric vector to the Sun or Moon,  $\mu_d$  is the gravitational constant of the Sun or Moon and  $\bar{r}$  is the position vector to the point of computation. For a more realistic frequency-dependent model for the Love numbers, most of the variations are concentrated in a single band (the diurnal). It is computationally efficient to use a simple frequency-invariant background model as a complete description of the solid Earth tides (as in equation 3.5) and correct select terms for which the Love numbers differ significantly from the background reference values. This procedure was adopted in our analysis.

Because terms with f = 0 were included in the tidal acceleration of the spacecraft, the resulting gravity field, its geoid etc., have all the permanent-body tidal deformation completely removed. In this way, they happen to be in agreement with earlier IAG resolutions on modeling the permanent tide and conflict with those which are most recent.

The tidal constituent f is uniquely identified by the Doodson argument number. Table 3.1 identifies the principal tidal frequencies and gives the (approximate) matching Darwinian symbol for each corresponding Doodson number. The frequencies are based upon the ecliptic constant element rates. Note that these same frequencies are also present in the ocean tide effects.

The direct potential effects of the other disturbing bodies are modeled as point mass effects:

$$U^{d} = \mu_{d} \left( \frac{1}{\rho} - \frac{\bar{r}_{d} \cdot \bar{r}}{r_{d}^{3}} \right) \tag{3.6}$$

where  $\rho = |\vec{r}_d - \vec{r}|$  is the distance from the satellite to the disturbing third body. The second term refers the accelerations of the satellite to the center of the Earth.

In the case of the Earth-Moon system, the effect of the Earth's oblateness must be included in the precise computation of third-body accelerations. The effect of the Earth's gravity on the Moon is given by Equation. 3.1. As the force exerted on the Moon by the gravity of the Earth is matched by an equal and opposite force by the Moon on the Earth, the additional acceleration to be applied to the satellite radially and in latitude is:

$$\ddot{r} = \frac{-1.5\mu_m}{r_m^4} a_e^2 C_{20} (3\sin\phi_m - 1)$$
 (3.7a)

$$\ddot{\phi} = 3 \frac{\mu_m}{r_-^3} a_e^2 C_{20} \sin \phi \cos \phi_m \tag{3.7b}$$

where  $\mu_m$  and  $r_m$  correspond to  $\mu_d$  and  $r_d$  for the Moon and  $\phi_m$  is the latitude of the Moon. The inclusion of this effect more precisely refers the accelerations of the satellite to the center of the Earth.

## 3.3.1.1 The A Priori Static Geopotential Model: GEM-T1

The *a priori* gravitational model adopted was the Goddard Earth Model - T1 (GEM-T1) using terms through degree and order 20. GEM-T1 resulted from a major new computation of the terrestrial gravitational field by the Geodynamics Branch of Goddard Space Flight Center.

Table 3.1. Principal Tidal Components

Darwinian Symbol	Doodson's Argument Number	Period (hr)	Description
M2	255.555	12.42	Principal lunar semidiurnal
S2	273.555	12.00	Principal solar semidiurnal
N2	245.655	12.66	Larger lunar elliptic semidiurna
K2	275.555	11.97	Lunar/Solar semidiurnal
L2	265.455	12.19	Smaller lunar elliptic
K1	165.555	23.93	Lunar/Solar diurnal
O1	145.555	25.82	Principal lunar diurnal
P1	163.555	24.07	Principal solar diurnal
Mf	075.555	13.66d	Lunar fortnightly
Mm	065.455	27.55d	Lunar monthly
Ssa	057.555	188.62d	Solar semi-annual

A simultaneous solution was made for spherical harmonic parameters of both tidal and invariant parts of the gravitational field (Marsh et al., 1988, Christodoulidis et al., 1988).

The GEM-T1 model adopted the latest IAG reference constants and was solved in the J2000 Reference System. This gravitational model was based on modern ellipsoidal parameters (a<sub>e</sub>=6378137m and 1/f=298.257) and the adopted speed of light (c=2999792.458 km sec<sup>-1</sup>). It provided a simultaneous solution for a gravity model in spherical harmonics complete to degree and order 36; and a subset of 66 ocean tidal coefficients for the long wave-length components of 12 major tides. This adjustment was made in the presence of 550 other ocean tidal coefficients representing 32 major and minor tides and the Wahr frequency-dependent solid-Earth tidal model.

GEM-T1 was derived exclusively from satellite tracking data acquired on 17 different satellites whose inclinations ranged from 15 degrees to polar. In all, almost 800,000 observations were used, half of which were from third-generation laser systems. LAGEOS contributed nearly 5 years of observations to this solution. The calibration of the model accuracies performed for GEM-T1 show it to be a great improvement over all earlier GSFC "satellite-only" models for both orbital and geoidal modeling applications. For the longest wavelength portion of the

geoid (to 8 x 8), GEM-T1 appears to be an improvement over all earlier GEM models, even those containing altimetry and surface gravimetry, including GEM-L2 [Lerch et al., 1985] which was adopted by the MERIT Campaign for LAGEOS data analyses. Figure 3.6 compares the calibrated accuracy of the GEM-L2 and GEM-T1 potential models revealing the basis for its adoption for the SL7.1 analysis.

### 3.3.1.2 The A Priori Body Tide Model: Wahr

Table 3.2 gives the Love numbers computed by Wahr [1981], based upon the Earth Model 1066A of Gilbert & Dziewonski [1975]. Note that  $\delta_{2,f}$  is zero for this elastic model, i.e., the model is free of dissipation. These Love numbers characterize the response of the 1066A Earth to the non-loading tide generating potential.

### 3.3.1.3 A Priori Ocean Tides Models: GEM-T1 Solution

The response of the oceans caused by the tide generating potential is a set of constituent tide heights

$$\xi_f(P) = A_f(P)\cos(\omega_f - \psi_f(P))$$
(3.8)

where  $\omega_f$  is the angular argument associated with constituent f and  $A_f(P)$  and  $\psi_f(P)$  are the tidal amplitude and phase, respectively, at point P. The amplitudes and phases are computed from numerical solutions of the Laplace Tide Equations. Such solutions involve a high computational burden and presently such models are available for only a limited number of tidal constituents.

The tidal heights are expanded into spherical harmonics by:

$$\xi_f(P) = \sum_{l,q,\pm} C_{lq,f}^{\pm} P_{lq}(\sin\phi) \cos\left(\sigma_{lq,f}^{\pm} \pm \varepsilon_{lq,f}^{\pm}\right)$$
(3.9)

Given the global tidal heights, the coefficients  $C_{lq,f}^{\pm}$  and phases  $\varepsilon_{lq,f}^{\pm}$  necessary for the evaluation of the potential can be computed.

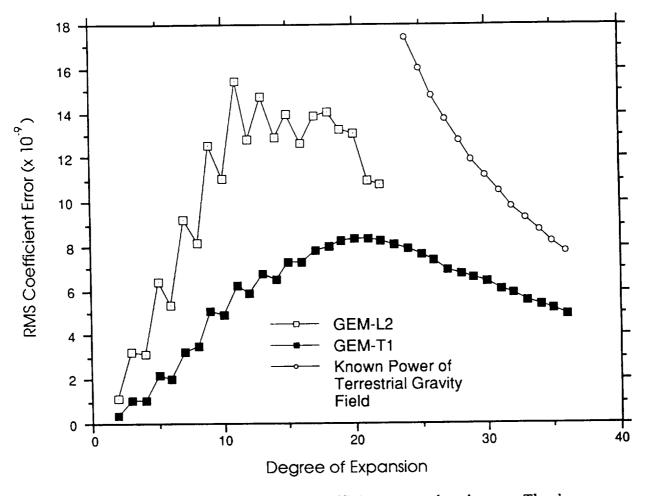


Figure 3.6 Gravity model RMS coefficient error by degree. The known power of the terrestrial fields is given by Kaula's rule which shows the approximate power of the field and gives a basis for estimating the percent accuracy of the harmonics of the field. Figure taken from *Marsh et al.* [1987].

Observed tide models for 11 major tide constituents in the semidiurnal, diurnal, and long-period bands have been computed on a 1° x 1° global grid by E.W. Schwiderski using an integration scheme which incorporates the available deep-sea tide gauge data. These tidal constituents typically account for over 90% of the total ocean tide amplitude at any point. However, numerous minor ocean tidal constituents, although small in amplitude, can have significant perturbing effects on satellite orbits. Models for these were developed using linear admittances from the oceanographic tide models [Christodoulidis et al., 1986b].

With the advent of centimeter-level satellite geodesy and geodynamics, it is necessary to accurately model the tidal deformation of the Earth and its oceans, i.e., the dominant temporal variations of the geopotential. This is in part because the data distribution in time and space cannot be selected so that the effects of these temporal variations average out. All these tides

Table 3.2. Wahr Love Numbers for 1077A

 Band	Tidal Line	k <sub>2,f</sub>	
Long Period	All	.299	
Diurnal	145555 (O1)	.298	
	163555 (P1)	.287	
	165545	.259	
	165555 (K1)	.256	
	165565	.253	
	166554 (PSI)	.466	
Semi Diurnal	A11	.302	

have significant perturbations on all near-Earth satellites of geodetic interest. In fact, geodetic satellites form a sensitive measurement system for monitoring tidal effects. Table 3.3 shows the periods of the principal long-period tidal perturbations on the orbits of most of the laser satellites. The diurnal and semidiurnal perturbations are quite different in frequency than the corresponding periodicities of the tides on the Earth's surface, because it is the satellite's nodal precession with respect to the third bodies and not the Earth's rotation which defines these periodicities. The amplitude of the major tides on the orbital inclination and ascending node of Starlette, (a satellite similar in design to LAGEOS, but orbiting in a slightly eccentric orbit at 800-1200 km altitude), and LAGEOS are shown in Figures 3.7 and 3.8.

Dynamic values for select terms in the ocean tides which are most orbit sensitive were derived as part of the GEM-T1 gravity solution. The body tides were held fixed according to the Wahr values during this development as given in Section 3.3.1.2 and the adopted precession and nutation are the IAU 1980 models. Because the body tides are not separable from the ocean tides using orbital dynamics, only the ocean tides were adjusted in GEM-T1. The ocean tides which were recovered simultaneously in this model actually represent a determination of the total temporal variations of the geopotential exterior to the Earth's atmosphere in the presence of a fixed solid-Earth tidal model [Marsh et al., 1987; Christodoulidis et al., 1988] and thereby are an aggregate mass transport model.

Table 3.4 summarizes the ocean tidal terms which were modeled in the development of SL7.1 and indicates which were adjusted in the GEM-T1 solution. Due to attenuation by the distance

Table 3.3. Periods (Days) of Principal Long-Period Satellite Perturbations

	Due to Solid Earth and Ocean Tides For 12 Major Tide Constituents											
	0	0	0	0	1	1	1	2	2	2	2	2
	5	5	6	7	4	6	6	4	5	7	7	7
	6	7	5	5	5	3	5	5	5	2	3	5
	•	<u>:</u>		<u>:</u>	<u>:</u>	<u>:</u>					5	
	5	5	4	5	5	5	5 5	6 5	5	5 5	5	5 5
	5	5	5	5 5	5 5	5 5	5 5	5 5	5 5	6	5	5
	4 5	5 5	5 5	5 5	5	5	5	5	5	5	5	5
SATELLITE	Sa	Ssa	Mm	Mf	01	P1	K1	N2	M2	T2	S2	K2
LAGEOS	365	183	27.6	13.7	13.8	221	1050	9.20	14.0	159	280	524
STARLETTE	365	183	27.6	13.7	11.9	60.8	91.0	7.61	10.5	33.1	36.4	45.5
GEOS-1	365	183	27.6	13.7	12.6	85.4	160	8.20	11.7	48.3	55.7	80.2
GEOS-2	365	183	27.6	13.7	14.4	629	257	9.83	15.3	2250	436	129
GEOS-3	365	183	27.6	13.7	15.2	482	132	10.6	17.2	145	104	66.2
BE-B	365	183	27.6	13.7	13.1	118	332	8.66	12.6	70.2	87.0	166
BE-C	365	183	27.6	13.7	11.8	57.9	84.8	7.51	10.3	31.5	34.4	42.4
SEASAT	365	183	27.6	13.7	14.8	7130	178	10.2	16.1	331	174	89.0
TELSTAR-1	365	183	27.6	13.7	12.8	93.9	193	8.34	12.0	53.9	63.2	96.7
ANNA	365	183	27.6	13.7	12.0	64.4	99.4	7.71	10.7	35.3	39.1	49.7
OSCAR	365	183	27.6	13.7	13.6	180	11700	9.12	13.6	119	177	5830

of the satellite from the oceans, the tidal model is only required to degree 6 in the SL7.1 solution development. Partial derivatives for the tides most significant on the evolution of the LAGEOS orbit were computed to add flexibility to the SL7.1 analysis.

# 3.3.2 Non-Conservative Forces: Atmospheric Drag and Solar Radiation Pressure

The non-conservative forces which are of concern in modeling the evolution of the LAGEOS orbit are the forces of an apparent "drag-like" effect and solar radiation pressure. We are presently not modeling Earth albedo: we believe we have minimized any unmodeled albedo effects by adjusting empirical coefficients.

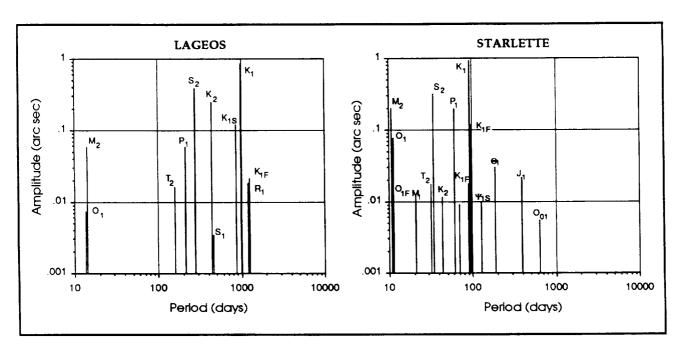


Figure 3.7 Effects of tidal perturbations on the inclinations of LAGEOS (left) and Starlette (right). Figure taken from *Marsh et al.* [1987].

### 3.3.2.1 Mathematical Formulation of the Models

The acceleration of an Earth orbiting satellite due to atmospheric drag is commonly expressed as

$$\overline{A}_{D} = -\frac{1}{2}C_{D}\left[\frac{A}{M}\right]\rho_{D}v_{r}\overline{v}_{r} \tag{3.10}$$

where  $C_D$  is the satellite drag coefficient, A is the effective cross-sectional area of the satellite, M is the mass of the satellite,  $\rho_D$  is the density of the atmosphere,  $\overline{v}_r$  is the velocity vector of the satellite relative to the atmosphere and  $v_r$  is its modulus. The standard atmosphere model of *Jacchia* [1971] is used by GEODYN to provide atmospheric density values at satellite altitude. Jacchia's model is designed to give density values between 90 and 2500 km altitudes. Due to these limits, density values at LAGEOS altitude are unavailable. However, a "drag-like" decay of the LAGEOS orbit of ~1.3 mm/day in its semi-major axis is observed and a means to precisely model the decay is required. This is accomplished in the SL7.1 solution through the adjustment of along-track acceleration parameters within each monthly arc.

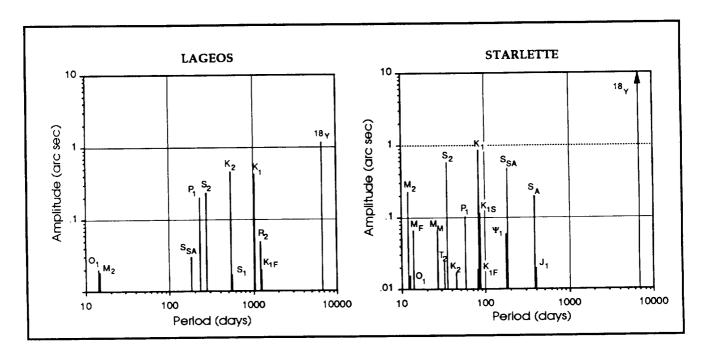


Figure 3.8 Effects of tidal perturbations on the right ascension of the ascending node of LAGEOS (left) and Starlette (right). Figure taken from *Marsh et al.* [1987].

General satellite accelerations can be modeled in GEODYN and have the form

$$\ddot{\overline{X}} = \alpha \hat{u} \tag{3.11a}$$

where  $\hat{u}$  is a unit vector defining the direction of the acceleration (specifiable within GEODYN) and  $\alpha$  is the solved-for parameter. The direction of along-track acceleration is defined as

$$\hat{u} = \frac{\overline{v}}{|\overline{v}|} \tag{3.11b}$$

and is in the direction of the satellite's time of date velocity vector. After extensive experimentation, it was concluded that a single  $\alpha$ -value for each 15-day period within a monthly orbit properly resolved this observed "drag-like" effect. Many authors have sought to provide the physical explanations for this observed effect. The results and discussion of our estimation of  $\alpha$  within the context of the recent developments are given in Section 5.2.

The acceleration due to solar radiation pressure is given by

Table 3.4 Ocean Tide Modeling Within the GEM-T1 Solution Adopted for SL7.1 Taken from *Marsh et al.* [1987]

	Taken from Mars Long Perio		
Doodson	Darwin	Modeled	Adjusted
Number	Name	in SL7.1	in GEM-T1 Solution
056.554	Sa	deg. 2→6	deg. 2
057.555	$S_{sa}$	prograde	deg. 2
058.554	ou.	only	none
065.455	$M_{\mathbf{m}}$	•	deg. 2
075.555	$M_f$		deg. 2
075.565			none
	Diurr	ıal	
135.655	$Q_1$	deg. 2→6	none
145.545		prograde	none
145.555	$O_1$	and	deg. 2,3,4
155.455		retrograde	none
155.655	$M_1$		none
162.556	$Pl_1$		none
163.555	$P_1$		deg. 2,3,4
164.556	$S_1$		none
165.545			none
165.555	$K_1$		deg. 2,3,4
165.555			none
166.554			none
167.555	_		none
175.455	S <sub>1</sub>		none
185.555	$OO_1$		none
	Semi Di	urnal	
245.655	$N_2$	deg. 2→6	deg. 2,3,4,5
255.545		prograde	none
255.555	$M_2$	and	deg. 2,3,4,5
265.455	$L_2$	retrograde	none
271.557			none
272.556	T <sub>2</sub>		deg. 2,3,4,5
273.555	$S_2$		deg. 2,3,4,5
274.554	$R_2$		none
275.555	K <sub>2</sub>		deg. 2,3,4,5
285.455			none
295.555			none

$$\overline{A}_{R} = -vC_{R} \left[ \frac{A}{M} \right] P_{s} \hat{r}_{s} \tag{3.12}$$

where v is the eclipse factor accounting for shadowing of the satellite by the Earth or Moon,  $C_R$  is the satellite radiation pressure coefficient, A and M are as used in equation 3.10,  $P_s$  is the

solar radiation pressure at the satellite, and  $\hat{r}_s$  is the geocentric vector pointing toward the Sun. The quantity  $P_s$  is nominally specified by its mean value at 1 astronomical unit and corrected for the distance to the Sun through a term  $\left(r_s / r_{law}\right)^2$ . The parameter  $C_R = 1 + \rho_s$ , where  $\rho_s$ , is the (specular) reflectivity of the satellite surface.

An assumption of this simple model is that the satellite is spherical; an assumption that is quite adequate for LAGEOS. Moreover, the adjustment of the along-track acceleration and/or radiation pressure coefficients accommodate much of the model error associated with errors arising in the non-conservative force modeling. This premise was tested in the simulation described below.

## 3.3.2.2 The Neglect of an Earth Albedo Model

Generally stated, an accurate model for both the diffuse and specularly reflecting Earth is still under development. In modeling the time history of the specular properties of the Earth Rubincam and Weiss [1986] have listed several complications which make modeling Earth albedo difficult. These include, among others, geographical variations in albedo, albedo variations in time due to meteorological changes, and reflection and scattering due to the atmosphere itself. Further investigations have been made to assess the magnitude of these effects of Earth albedo on LAGEOS' orbit (cf. Section 5.2).

One assessment of possible albedo effects was made in an experiment (performed courtesy of Richard Eanes at the University of Texas Center for Space Research) where a 15-day orbit of LAGEOS was integrated which included perturbations arising from an along-track drag effect, direct solar radiation pressure, and albedo re-radiative effects using a rather complete model developed by Philip Knocke (private communication). This trajectory was then converted into satellite positions in time which could be used as data for simulation purposes. These values were fit in a least-squares estimation process where the albedo model was no longer used, but one in which the along-track acceleration and solar radiation pressure coefficients were adjusted. The resulting orbit agreed with the original to within 1-cm RMS. This experiment, coupled with a worst-case scenario study by *Rubincam et al.* [1987], support the contention that neglecting an Earth albedo model does not significantly corrupt the SL7.1 solution within the scope of the non-conservative and empirical force models adopted here for our monthly arc lengths.

# 3.4 Station Motion Model Within the Terrestrial System

There are two distinct sources for temporal variations in the locations of tracking stations relative to the CTRS: the effects of the astronomic tides on the geosphere and the effects of plate motion. This section will describe the models used in SL7.1 and discuss planned improvements.

# 3.4.1 Station Tidal Variations

The tidal forces acting upon the Earth's surface cause the tracking stations to undergo periodic motions. This effect is conveniently modeled as the sum of the response of a spherical elastic Earth to the disturbing potentials of the Sun and Moon plus correction terms due to the frequency-dependent elastic response of a more realistic Earth. A convenient formulation for these motions was derived by *Diamante and Williamson* [1972] and has been implemented in GEODYN as well as having been adopted in the MERIT standards [Melbourne et al., 1983] and subsequent IERS standards [McCarthy et al., 1989].

For the simple elastic model, the vector displacement of the station to a precision of 1 cm is given by *Diamante and Williamson* [1972]:

$$\Delta \bar{r} = \sum_{d} \frac{\mu_{d}}{\mu} \frac{r_{sta}^{4}}{r_{d}^{3}} \left\{ (3l_{2}\cos S) \frac{\bar{r}_{d}}{r_{d}} + \left[ 3\left(\frac{h_{2}}{2} - l_{2}\right)\cos^{2} S - \frac{h_{2}}{2} \right] \frac{\bar{r}_{sta}}{r_{sta}} \right\}$$
(3.13)

where d indicates either the Sun or Moon as the disturbing body,  $\bar{r}_d$  is the position vector of the disturbing body,  $\bar{r}_{sta}$  is the station position vector,  $\mu_d$  is the gravitational constant of the disturbing body,  $\mu$  is the gravitational constant of the Earth,  $h_2$   $l_2$  are the Love and Shida numbers, respectively, which characterize the Earth's elastic response, and

$$\cos S = \frac{\overline{r}_{sta} \cdot \overline{r}_d}{r_{sta} r_d} \tag{3.14}$$

Nominal values for the Love and Shida numbers are

$$h_2 = .6090$$
  $l_2 = .0852$ 

When a more realistic model of the Earth is used, the fluid interior of the Earth causes the deformation response to be frequency dependent. Wahr [1980] has shown that this effect in station position can be modeled to better than 5 mm by simply correcting the response of the simple elastic model for the differential response at the  $K_1$  frequency. At this frequency, the Love number h from Wahr's theory is 0.5203. Only the radial displacement needs to be corrected at the 5-mm accuracy level. The additional radial correction, which is also specified by the MERIT and IERS Standards, is (in meters):

$$\overline{\Delta r_2} = -.0253 \sin \phi \cos \phi \sin \left(\theta_g + \lambda\right) \frac{\overline{r}_{\text{stat}}}{r_{\text{stat}}}$$
(3.15)

where  $\phi$  is the station geocentric latitude,  $\lambda$  is the corresponding east longitude, and  $\theta_g$  is the right ascension of Greenwich. At 45 degrees latitude, this effect reaches a maximum of 13 mm. The total correction vector is given by

$$\Delta \bar{r}_{sta} = \overline{\Delta r_1} + \overline{\Delta r_2} \tag{3.16}$$

For future solutions, an expanded frequency-dependent model including all terms to the millimeter level is anticipated. In addition, ocean and atmospheric loading should also be incorporated. It has been shown that ocean loading can have an effect as large as 17 mm in vertical displacement for locations in the middle of the North American Continent [Pagiatakis, 1990]. Ocean loading can be quite sizable (> 50 mm) at coastal sites. Atmospheric loading can cause vertical surface displacements as large as 20 mm and the oceanic response to atmospheric loading can additionally effect the vertical displacements for sites in coastal regions [Van Dam and Wahr, 1987].

### 3.4.2 A Priori Station Plate Tectonic Motions

As discussed in Section 3.1.2.2, it is difficult to adopt a completely satisfactory Earth-fixed reference frame due to the motion of the tectonic plates. While the relative location of points on the earth's surface are strictly deterministic, the absolute direction of the station motions are not easily defined in a system useful for geophysical and geological time frames. When confronting this problem, *Minster and Jordan* [1978] considered modeling tectonic motions within four distinct "absolute" systems. These were each developed under differing kinematical constraints: best fitting to hotspot data (mean mesospheric frame, AM1-2), African plate fixed

(AM2-2), Caribbean plate fixed (AM3-2), and a solution whereby the net rotation of the lithosphere is constrained to be zero (AM0-2).

The hot spot system, based on the traces of long-term (~10 million years) centers of mantle plume activity, was thought by Minster and Jordan [1978] to best represent an absolute frame. However, as they were aware, the resulting absolute motion model depended on the validity of the Wilson-Morgan fixed hot spot hypothesis which has recently received some challenge. Molnar and Stock [1987], and in summary by Olson [1987], have determined that the hot spots themselves are moving relative to one another with rates of at least 10 mm/yr and as much as 20 mm/yr. They therefore conclude that the hot spot traces do not define a fixed reference frame. The use of the hot spot frame is additionally complicated by an element of subjectivism with regard to the selection of the hot spots used to define the frame. Although Minster and Jordan [1978] were careful in their selection, an omission or addition of one or several hot spots traces could dramatically change the "absolute" motions of the plates.

Other alternatives to defining an "absolute" system include simply fixing one particular plate or applying a constraint which forces the net rotation of the plates to be zero. Minster and Jordan [1978] made two plate motion solutions where the African and Caribbean plates were each fixed, respectively, in accordance to certain hypotheses regarding these two plates. Unfortunately, the global data set used by Minster and Jordan was unable to completely support the frames defined by fixing these plates. The application of a no net rotation constraint to the solution yields a uniquely defined reference frame that is free from subjective choices. However, as pointed about by Jurdy [1990], this mean lithosphere reference frame is based solely on the plate geometry and velocities and any variation in the velocities will alter the definition of the frame.

As a practical matter, any of these systems would be satisfactory for implementation in SL7.1 for each yields an identical set of temporal changes for inter-station distance determinations. Since the relative tectonic motions of points on the Earth's surface are the principal observational products of the SL7.1 solution, adoption of a frame largely serves to define the directions by which the station network is deforming. Although a more recent and further refined tectonic model is now available, NUVEL-1 [DeMets et al., 1990], we have, throughout the SL7.1 analysis, followed the MERIT standards (cf. Section 3.1.1) and use the AM0-2 model to provide the framework within which to make the solution.

Besides giving absolute reference to the observed tectonic motions of the SLR sites, an a priori tectonic motion model has additional application for the subset of quarterly solutions within SL7.1. For quarterly station coordinate determinations, sites located on fast moving plates may have perceptible motions within this averaging interval. Since the tracking data distribution is not consistent across time, the averaging taking place within such a solution may not be adequate for obtaining the location of the sites at their quarterly mid-point. Since earlier SLR results indicated that the relative motions predicted by AM0-2 were largely verified (e.g. Christodoulidis et al. [1985]), a more satisfactory result is achieved when the AM0-2 model is used to describe the a priori continuous motion of all sites. The quarterly solutions then correct the values for the station positions for the midpoint within each quarter, while simultaneously the change in location of the sites between the start and end of the quarter is modeled by AM0-2.

The mathematical implementation of an "absolute" plate motion model is found in *Melbourne* et al. [1983] as provided by Minster and Jordan. Briefly, let  $X_o$ ,  $Y_o$ ,  $Z_o$  at time,  $t_o$ , be the Cartesian location of a site on a known plate. The calculation of X, Y, Z at a new time, t, is obtained by:

$$X = X_o + (\dot{Y} \cdot Z_o - \dot{Z} \cdot Y_o)(t - t_o)$$

$$Y = Y_o + (\dot{Z} \cdot X_o - \dot{X} \cdot Z_o)(t - t_o)$$

$$Z = Z_o + (\dot{X} \cdot Y_o - \dot{Y} \cdot X_o)(t - t_o)$$
(3.17)

where the Cartesian velocities  $\dot{X}$ ,  $\dot{Y}$ ,  $\dot{Z}$  per plate for the AM0-2 model are given in Table 3.5. This is the formulation used in GEODYN II.

Table 3.5. AM0-2 Cartesian Plate Velocities (degrees/MY)\*

Plate	Ż	Ϋ́	Ż
Pacific	-0.12276	0.31163	-0.65537
Cocos	-0.63726	-1.33142	0.72556
Nazca	-0.09086	-0.53281	0.63061
Caribbean	-0.02787	-0.05661	0.10780
South American	-0.05604	-0.10672	0.08642
Antarctic	-0.05286	-0.09492	0.21570
Austro-Indian	0.48372	0.25011	0.43132
African	0.05660	-0.19249	0.24016
Arabian	0.27885	-0.16744	0.37359
Eurasian	-0.03071	-0.15865	0.19605
North American	0.03299	-0.22828	-0.01427

<sup>\*</sup> The values shown in above must be scaled by 1.7453292 x 10<sup>-8</sup> to produce values in radians/yr before being used in equation (3.17).

# 4. Data Acquisition, Preparation and Processing

# 4.1 Laser System Description, Performance and Data Quality Control

Each laser tracking station consists of a variety of subsystems and instruments as illustrated in block form in Figure 4.1. The tracking system's laser and associated telescopes are aimed at a satellite using a target acquisition system which utilizes accurate orbit predictions. Laser pulses are emitted from the station, reflected by the target, and return to the receiving system where the pulses are detected and the elapsed travel time is measured. The detection system typically utilizes a predicted time-of-flight window (technically, a gated discriminator) to eliminate background noise in the returns, and uses filters tuned to the laser wavelength to further improve system sensitivity by rejecting undesired wavelengths. In many of the larger fixed systems, the transmitter optics are separate from the receiving optics, whereas the compact mounts of the transportable systems incorporate common transmit/receive paths. A separate timing system with good long-term stability is used to establish epoch time and is synchronized to a universal time standard using LORAN-C, the Global Positioning System (GPS) or a transportable atomic clock.

Much time and effort has been spent in developing laser tracking systems that minimize the effects from error sources and maximize output efficiency and ease of operation. Throughout the developmental process, all associated subsystems have been thoroughly scrutinized to guarantee successful operation and to insure that the goals set out by the CDP would be achieved. A detailed account of laser system development and the considerations and decisions made regarding the design or selection of each component is found in *Degnan* [1985]. A more recent account of the current (1991) status of the laser tracking system and its capabilities is found in *Murdoch and Decker* [1989]. Specific details on the designs and operations of many of the laser stations can be found in a variety of international laser ranging workshop proceedings. (Of recent note are proceedings from meetings held in 1986 at Antibes Juan-Les-Pins, France, [Gaignebet and Baumont, 1986] and in 1989 at Matera, Italy, [Veillet, 1990]).

# 4.1.1 Laser Ranges, Corrections, and Calibration

Knowledge regarding the entire ranging system, its relationship to fixed ground points, and certain satellite characteristics are required in order to link the measurements to ongoing

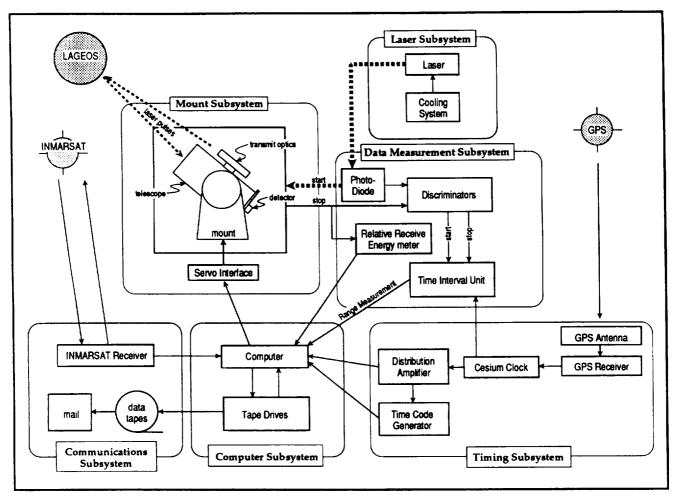


Figure 4.1 Laser tracking system block diagram (modified from Murdoch and Decker [1989]).

geophysical and tectonic processes. This knowledge constitutes the range measurement model and through calibration procedures we are able to confidently analyze and interpret the results. In this section we will summarize the elements which form and influence the laser range observations to LAGEOS.

The laser generates pulses of monochromatic, coherent light at repetition rates ranging from a few pulses per minute to 10 pulses per second (pps), and at power levels between 5 mJ and 1.5 J. The *range* between the station and the satellite is taken to be one-half of the product of the round-trip transit time of the laser pulse with the speed of light. The time tag of the measurement must be corrected to satellite reception time, taking into account the transit time of the pulse to reach the satellite (~20 msec for LAGEOS). Each range observation is corrected for

the effects of atmospheric refraction with the Marini/Murray algorithm [Marini and Murray, 1973], which is based on locally measured meteorological readings taken coincidentally with the laser data at the tracking site. A correction for the offset of the satellite retroreflector from the center of mass of the spacecraft is also made which amounts to 24 cm for LAGEOS [Fitzmaurice et al., 1977]. The fixed laser systems rest firmly on concrete pillars where, in many cases, the measurement reference point is defined by the optical center of the system and, except for instances of equipment upgrades, are considered to be invariant reference points. The mobile systems normally are parked and leveled on concrete pads and surveys are performed during each occupation to locate the optical center of the instrument to a nearby brass marker embedded in concrete. These offsets are known as site eccentricities and are crucial in the monitoring of the site's motion across time. These eccentricity offsets are listed by station and time in Appendix 1. At the mobile sites, the SL7.1 solution for station positions refers to the location of these brass markers which are directly constrained through the eccentricity values to the location of the optical centers of the laser for each site occupation.

The stations are calibrated regularly during field operations by tracking targets placed either external to or within the optical system at a known distance. A battery of system-level accuracy checks is routinely performed to ensure that the instruments are working within their specifications, specific details of which can be found in *Degnan* [1985]. Range observations are therefore transmitted from each site with a minimum of error. Further quality control checks are performed at the analysis centers to identify blunders, systematic biases, and registration errors that may be embedded in the data. These aspects are described in Section 4.1.4.

# 4.1.2 Collocation Testing

Each laser tracking system fielded by NASA undergoes a calibration against a fixed standard before it is deployed. The calibration compares, in a side-by-side or collocated fashion, the range measurements and the meteorological observations taken by the independent laser systems. These tests provide the opportunity to identify laser system range biases and to isolate system-dependent systematic error sources. Occasionally, collocation tests are conducted in the field, utilizing a mobile system which has, in turn, been collocated with the fixed standard (typically MOBLAS-7 at Greenbelt, MD). A list of collocation tests is given in Table 4.1, showing the names of systems compared. By regularly conducting these calibration experiments anomalous system behavior can be identified and accuracy at the specified level can be assured.

Table 4.1. Collocation Tests

Syste #1	ems #2	Location	Date
STALAS	ML01	GORF*	Nov 77
STALAS	ML03	GORF	Oct-Nov 77
TALAS	ML08	GORF	Feb-Mar 79
TALAS	ML05	GORF	Mar-Apr 79
STALAS	ML06	GORF	Feb-Apr 79
TALAS	ML07	GORF	Apr-May 79
TALAS	ML04	GORF	Mar-May 80
TALAS	TL01	GORF	Mar-May 80
STALAS	TL01	GORF	Sep-Oct 80
STALAS	ML07	GORF	Jul-Aug 81
/L07	ML04	GORF	Aug-Oct 81
HOLLAS	ML01	Hawaii	Sep 81-Jan 82
1L07	ML04	GORF	Jan-Apr 82
L01	MLRS	Fort Davis, TX	Jul-Aug 82
/IL07	ML06	GORF	Jul-Oct 82
1L07	TL02	GORF	Sep-Nov 82
1L07	ML04	GORF	May-Jun 83
/IL08	TL01	Quincy, CA	Jul-Aug 83
/IL04	TL01	Mon. Peak, CA	Oct 83
MT01	KOOLAS	Kootwijk, Neth.	Apr-May 84
ML08	TL01	Quincy, CA	Sep-Dec 84
AL04	TL01	Mon. Peak, CA	Jan-Jul 85
ML02	ML07	GORF	May-Jun 85
ML07	MT01	GORF	May-Jul 85
ит01	MATERA	Matera, Italy	Jan-Mar 86
AT02	MATERA	Matera, Italy	Jan-Mar 86
мт01	MT02	Matera, Italy	Jan-Mar 86
ML07	TL02	GORF	Nov 86 - May 87
ML07	TL01	GORF	Dec 86 - Jan 87
ML07	TL03	GORF	Oct 87 - Jan 88

<sup>\*</sup> GORF: Goddard Optical Research Facility, Greenbelt, MD.

Typically, a collocation test involves a series of procedures and system check-outs. Strict control of the hardware and software set-up, or configuration, throughout the collocation experiment is required to ensure that the results will accurately describe unforeseen system discrepancies. Both systems in the collocation test go through a series of ground tests and satellite ranging tests. The ground tests check system stability parameters by measuring system delays and determining the delays due to any azimuthal and elevation dependence. For the TLRS-1 and MOBLAS-7 systems, these delays should meet a 20-mm performance goal. Both systems were shown to have easily achieved these goals in 1987 with the actual performance being measured at the 4 - 5 mm level [Husson et al. 1987]. In the satellite tests, the systems are run in two modes; calibration mode having a performance goal of 20 mm and satellite ranging mode having a performance goal of 30 mm. Again, TLRS-1 and MOBLAS-7 easily achieved these goals by a factor of 2 [Husson et al., 1987]. Meteorological closure is assessed by differencing the meteorological data (e.g. temperature, humidity and barometric pressure) taken by each system during the course of the collocation. Typically these differences are quite small (e.g. < 1 mbar and < 1° C).

The chief assessment of system performance comes from an analysis of simultaneous laser tracking of geodetic satellites in a variety of categories; e.g. by quadrant, by ascending or descending passes, and in daylight passes. The analysis provides information from which detailed bias assessments can be made. These entail examining the data to determine the nature and extent of range biases, and their dependence on azimuth, range and elevation. For example, Kolenkiewicz et al. [1987] showed that between TLRS-1 and MOBLAS-7 a mean range bias of  $2.7 \pm 4.9$  mm was measured based on 22 passes of simultaneous LAGEOS tracking.

# 4.1.3 System Improvement Milestones

The systems which were originally built and operated by the Smithsonian Astrophysical Observatory (SAO) underwent their upgrade programs simultaneously (M. Pearlman, private communication). At the time that LAGEOS was launched in May 1976, these stations, situated at Mount Hopkins, Arizona; Arequipa, Peru; Orroral, Australia; and Natal, Brazil were equipped with time digitizers which yielded range observations at a noise level of approximately one meter. Pulse choppers installed in 1978 narrowed the effective pulse length from 25 nanoseconds to 6 nanoseconds, producing a noise level improvement to about 30 cm. Improved shutters were installed in 1980 which further reduced the noise level to 15 cm for a transmitted signal of 3 nanoseconds, and analog detectors were introduced to handle an increased repetition rate from 15 per minute to 30 per minute.

Goddard Space Flight Center fielded a series of five similar laser systems in late 1979 to supplement the three different systems in operation at that time. After temporary deployment, these mobile laser systems settled at Monument Peak, California (MOBLAS-4); Yaragadee, Australia (5); Mazatlan, Mexico (6); Greenbelt, Maryland (7); and Quincy, California (8). The short-pulsed Quantel laser which was implemented in the systems at these locations was modified between 1982 and 1983 to increase the repetition rate from one pulse per second to 5 pps. In 1985 and 1986 the noise level of the systems was reduced from 2 or 3 cm through the installation of a high resolution photomultiplier (micro-channel plate), together with a low noise discriminator. The current noise level for LAGEOS observations taken by each system is for MOBLAS-4: 11 mm, MOBLAS-5: 9 mm, MOBLAS-6: 8 mm, MOBLAS-7: 8 mm and MOBLAS-8: 8 mm.

# 4.1.4 Data Quality Control and Estimation of System Biases

The control of the laser measurement quality is first exercised during the compression of the observations to normal points (details of which are described in Section 4.2). In the orbital fit to the full-rate data, only observations which fall within a 3-m residual window are considered for further analysis. The normal point generation step subsequently eliminates outliers that exceed three times the rms residual about a polynomial fitted to each pass. The normal points themselves are used in the final stage of data quality control. They are fitted to an orbit and their residuals are inspected for unusually high noise and for any systematic bias. Observations failing this quality control step are excluded from the final reduction of the data in which normal equations are generated.

A further quality control step can be taken during the geodetic analysis procedure. A subset global solution is made in which month-by-month range bias values for each station are estimated simultaneously with a single station position for the full mission lifetime. Stations providing concentrated observations over a long period of time can thus allow us to separate persistent systematic range errors from station position. Table 4.2 gives a list of stations exhibiting unusually high range bias estimates, which sometimes occur for only part of the station occupation. The full history of range bias values for the stronger stations is presented in Figures 4.2(a - o).

# 4.1.5 Data Catalogs

The results of the data quality control process are given in Appendix 2 which provides a summary of station characteristics for every monthly arc in which its observations were included. The number of observations, range RMS statistics, bias estimate and the number of passes available for each month are listed for each station. The nature of any corrections to the data used in the SL7.1 solution are listed in Table 4.3, and are the result of confirmed and correctable station anomalies, most of which were trapped by the data quality control procedure at an early stage.

Table 4.2. Stations Showing Significant Range Bias

Station	Number	Data Span (Partial Occupation)	Bias (cm)	
McDonald	7086	(8506-8712)	-4±3	
Haystack	<b>7</b> 091	7802-8011	$30\pm 5$	
Mon. Peak	7110	(8307-8712)	4 ± 2	
Platteville	7112	(8103-8308)	-10 ± 5	
Goldstone	7115	7909-8104	-13 ± 5	
Mazatlan	7122	8305-8712	3±3	
Maui	<b>72</b> 10	8109-8712	5±2	
Zimmerwald	<b>7</b> 810	8405-8705	10 ± 5	
Kootwijk	7833	(7904-8005)	20 ± 5	
Wettzell	7834	7807-8712	-3±2	
Simosato	7838	8204-8706	5±4	
Graz	7839	8309-8705	-3±2	
Orroral	7843	8505-8611	15 ± 10	
Arequipa	7907	(8001-8604)	-7±3	
		(8605-8712)	-3±3	
Mt. Hopkins	<i>7</i> 921	(7807-8203)	-35 ± 10	
Natal	7929	(7807-8110)	-20 ± 10	
Matera	7939	8309-8712	-3±2	
Orroral	7943	7904-8202	-35 ± 10	

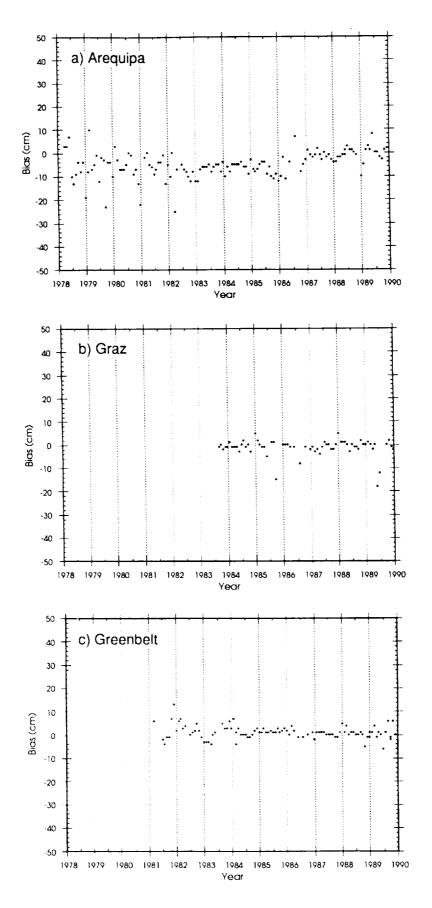


Figure 4.2 (a-c) SL7.1 estimates of monthly range bias values.

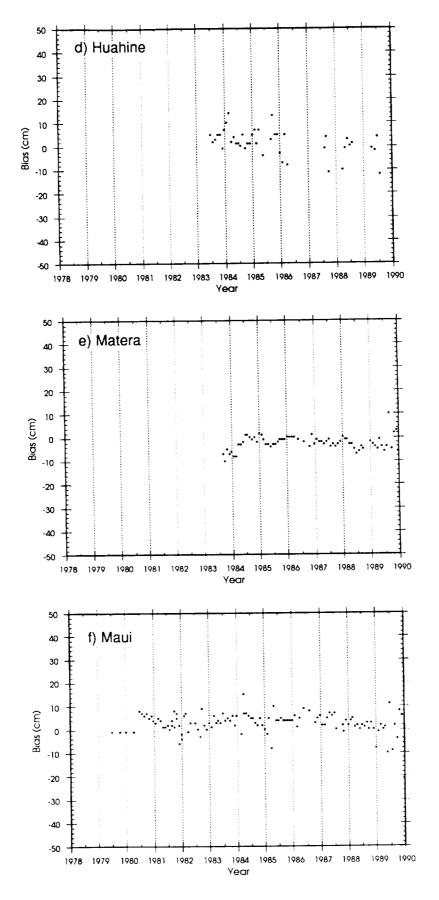


Figure 4.2 (d-f) SL7.1 estimates of monthly range bias values.

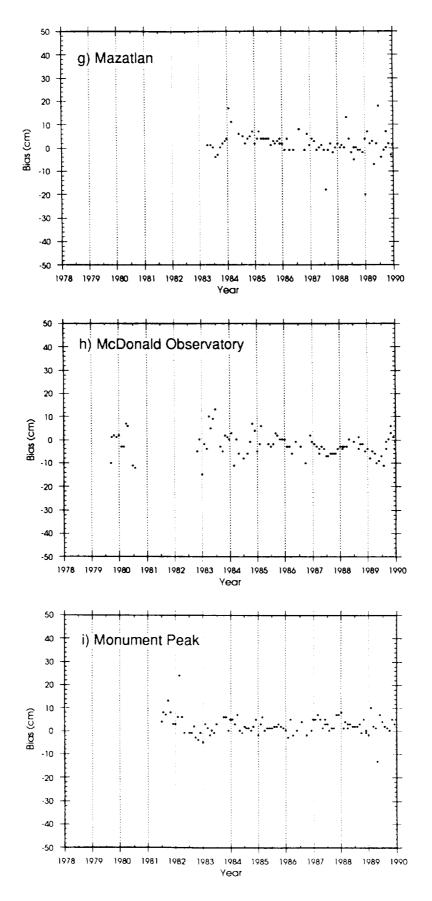


Figure 4.2 (g-i) SL7.1 estimates of monthly range bias values.

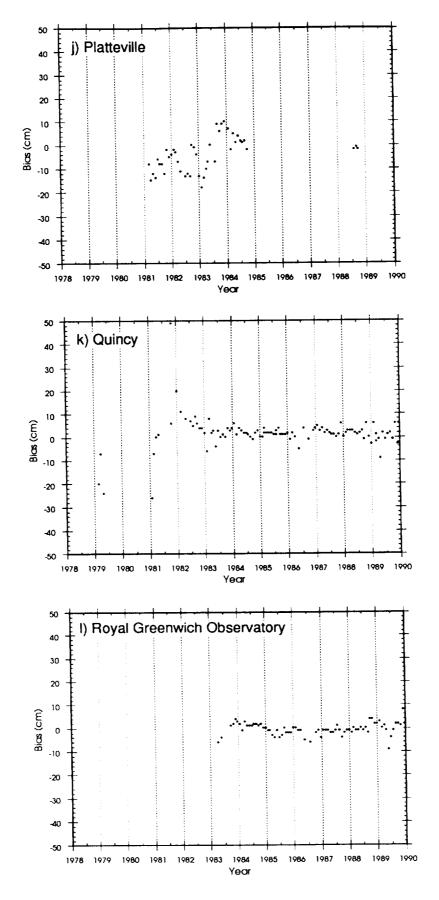


Figure 4.2 (j-l) SL7.1 estimates of monthly range bias values.

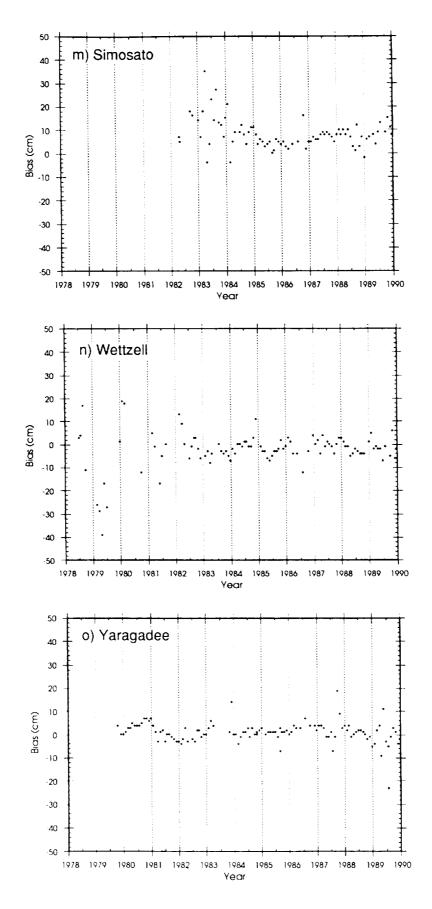


Figure 4.2 (m-o) SL7.1 estimates of monthly range bias values.

Table 4.3. Observation Correction Table

Station	Number	Date Start-End	Data Correction*
Orroral	7943	7609-8203	$\Delta R = -0.041 \text{ m}$
			(Target Survey Error)
Orroral	7943	7806-7809	$\Delta R = -4.62500345 \text{ (MJD-} 2443690) \times 10^{-6} \text{ (m)}$
			(Counter Error)
Bear Lake	7082	7609-7611	$\Delta R =325 \text{ m}$
			(Target Survey Error)
Wettzell	7834	7807-8308	$\Delta R = 7*10^{-9} R (m)$
			(Oscillator Error)
Huahine	7121	8307-8308	$\Delta T = -194126  \mu sec$
			(Clock Error)
RGO	7840	8305	$\Delta R = 14.937 \text{ m., WT} = -62  \mu \text{sec}$
		8307	$\Delta R = 16.290 \text{ m., WT} = -367 \mu\text{sec}$
			(Calibration Error)
RGO	7840	8310-8312	$\Delta T = -(21-(MJD-45608)*0.209)(sec)$
			(Clock Error)
Simosato	7838	8204-8406	$\Delta T = +8 \mu sec$
		8410-8501	(Clock Error)
Easter I.	7061	8305-8307	$\Delta T = -1$ msec.
		8404-8105	$\Delta T = 1$ msec.
		8406-8411	$\Delta T = 2 \text{ msec}$
			(GPS Timing Error)

<sup>\*</sup> $\Delta$ T: correction to a timing error.

 $\Delta R$ : correction to a range error.

# 4.2 Normal Point Processing

In order to efficiently utilize available computer resources, satellite laser ranging (SLR) data to the LAGEOS satellite have been compressed into *normal points*. Recently the SLR data has become so numerous, with current data rates of 1 to 10 points per second and almost thirty systems tracking worldwide, that an aggregation method has become desirable to avoid excessive costs in the analysis of the data. For a satellite such as LAGEOS, which is orbiting at nearly an earth's radius in altitude, the temporal density of information provided by the full rate data is approximately two orders of magnitude greater than that which is needed to fully monitor the perturbed motion of this satellite. While large data sets of independent observations reduce the influence of data noise on the calculated orbit, experience has shown that data noise is not a dominant error source for dynamic orbit modeling applications of these data. Statistical methods can be used applying the full data density to estimate and then filter out the noise contribution to the observations. The SLR data is then compressed using temporal sampling based upon the presence of some minimum number of data points in the sampling interval. This entire process is known as forming laser normal points.

Other groups, such as *Hauck and Lelgemann* [1982] and *Masters et al.* [1983], have adopted methods to thin the data while at the same time reducing noise in the data set. *Masters et al.* [1983] used successive differences in the second time derivative of the range to edit the data and Chebyshev polynomial fits to short spans (150 sec) of the edited data to produce laser normal points. These procedures were designed to accomplish three major objectives: (1) outlying differences were used to edit anomalistic points, (2) the noise over these short spans was reduced by being averaged over the empirical function, and (3) filtered data, absent this noise, were produced. We have adopted similar procedures to accomplish these same objectives [*Torrence et al.*, 1984]. Our approach was adopted to address not only the formation of normal points but also to assist with the assessment of the systematic stability of the laser systems, and to assess their relative performance with respect to the other laser systems.

### 4.2.1 Normal Point Formulation

Measurements inherently contain random errors or noise. Ideally, the normal points associated with a given set of laser range observations are representative of the same observations free from noise, i.e., the observations which would have been made if the measurement process were noise free. The normal point procedure is not designed to eliminate systematic errors in the

data; such analysis normally requires an aggregate fit to the data from many tracking systems in an orbital reduction.

The observed laser range at time t may be expressed as

$$R_o(t) = R(t) + \varepsilon(t) \tag{4.1}$$

where R(t) is the true range and  $\varepsilon(t)$  is the observational noise. Optimally, the noise is minimized by averaging sufficient observations at time t so that the expected contribution of the random error to the average is insignificant. (for example, 0.1 mm). However, there is only one measurement at each time t, so the method must rely on having observations taken at a rapid rate over a short period of time,  $\Delta t$ . There must be sufficient observations during  $\Delta t$  so that the expected noise contribution is insignificant. It is also critical for the unmodeled signal in the observation during this  $\Delta t$  to have an insignificant contribution before forming a normal point.

Because the noise removal must be performed over a non-zero time span, the method requires the concept of an observation model and a noise model. The computed range to the satellite at any time  $R_c(t)$ , is the result of known modelable physical processes, as is done in GEODYN II. These models are capable of representing a range at all times within a pass, not just at the times of the observations, to the same general level of accuracy: it is deterministic, yielding a misclosure of observed vs. computed range on LAGEOS at the sub-decimeter level. While there are errors in our modeling of the "true" range, the model of the evolution of the range in time is correct for the first seven or so significant figures. This error in  $R_c(t)$  is given by:

$$\delta R(t) = R(t) + \varepsilon(t) - R_c(t) \tag{4.2}$$

Note that R(t) is the true noiseless range or the "normal" point range which is to be obtained.

Given a process for estimating R(t), normal points can be produced for each observation time. This is a very dense set, with observations occurring far more often than is required to sense the physical phenomena influencing the satellite's orbit. Therefore, along with normal point creation (noise removal), the data are thinned. This desirable decimation is made by just selecting the observation closest in time to the  $\Delta t/2$  point, which is the bin midpoint, and forming a normal point with this observation. This, in practice, also yields a uniform distribution of points across each pass.

Several considerations are involved in constructing normal points. First, the expected range as a function of time must be characterized. Through knowledge of the characteristics of the forces acting on a satellite, a "sampling" interval (bin) is determined which permits the reconstruction of all known "true" physical signals in the observed ranges from the thinned normal points. It is necessary to consider the behavior of  $\delta R$  within each bin. The spectra of  $\delta R$  must be known at short period (i.e., the bin width), to leave uncorrupted all meaningful longer periods from unmodeled orbit errors and modeled orbit effects. Harmonic analyses of the force-model error perturbations on LAGEOS show no perturbation greater than a centimeter for periods of less than 5 minutes. A numerical analysis of the order of the orbit integrator and the integration step size available in GEODYN II reveals that a good combination is a twelfth-order integrator coupled with a 150-second step size. Through the consideration of the spectra of the orbit perturbations and the numerical accuracy of GEODYN II, the choice was made to use 2-minute bins for forming normal points.

The orbit errors are found to be modeled adequately by a low-degree polynomial over a pass of residuals and, except for the rarest cases, vary linearly within a properly selected bin width. This is a result of using an accurate  $R_c$ . Therefore, the normal point  $R_N(t)$  is

$$R_N(t) \equiv R(t) = f(\delta R(t)) + R_c(t) \tag{4.3}$$

where  $f(\delta R(t))$  is some empirical function over the pass and bin used to correct the calculated range for the error in our physical models. The coefficients for this function are obtained from the signal left in the range residuals over the pass coupled with piecewise linear fits to the remaining residuals in the bin. The adopted procedure does both in succession.

Therefore, the procedural steps utilized for forming normal points are:

1. GEODYN II, based on our best knowledge of the forces, etc. produces a set of residuals from 15 days worth of global range data. This orbit fit produces a set of range residuals,  $\delta R(t)$ , representing the misclosure between the observations and the mathematical model of the satellite ephemeris.

$$\delta R(t) = R_o(t) - R_c(t)$$

2. A polynomial, g(t), is fit to the residuals of a pass of data

$$\delta R(t) = g(t) + \xi(t)$$

Each residual is thus characterized in terms of signal and noise. Note that  $\delta R(t)$  is distinct from the noise  $\xi(t)$  according to the sufficiency of g(t) to absorb the unmodeled signal in the original fitting process – A low-degree polynomial fit to  $\delta R(t)$  effectually removes any residual signal. The remaining residual,  $\delta r(t)$  is then

$$\delta r(t) = \delta R(t) - g(t)$$

The mean residual in the bin is then calculated

$$\delta \overline{r}_h = \langle \delta r(t) + \xi(t) \rangle$$

3. The expression for the "noiseless range" is given as:

$$R_{p}(T) = g(T) + R_{c}(T)$$

where *T* is mid-point time in the pass measured in uniform 2-minute intervals.

4. The normal point at time *T* is then:

$$R_{\scriptscriptstyle B}(T) = g(T) + R_{\scriptscriptstyle c}(T) + \delta \overline{r}_{\scriptscriptstyle b}$$

where T is defined as in 3 above, and  $\delta \bar{r}_b$  is the "bin" correction. However, to avoid any error in the interpolation of range to an arbitrary time, we select the true observation closest to the bin mid-point to produce a normal point:

$$R_N(t') = R_c(t') + g(t') + \delta \overline{r}_b$$

or alternatively as:

$$R_N(t') = R_o(t') - (\delta r(t) - \delta \overline{r}_b)$$

where t' is the time of an observation closest to the mean observation time within the bin.

In summary, the normal point noise at a specific point is estimated from the residual mean "signal" over the bin width. The noise error at this point is estimated and removed from the original range. Note also that the normal point is at the time of a real observation. An estimate of the noise from this observation to form a "normal point" at the most centrally located observation time within each bin is removed. This is repeated providing one normal point for each 2-minute tracking span.

# 4.2.2 Verification of the GSFC Normal Point Computations

The normal point computation procedure has been verified using a segment of LAGEOS full-rate data. These data were used to verify that the normal points preserve the information content of the full rate data for calculating the orbit and for the recovery of station coordinates.

Two tests were performed to assess the performance of the normal points. In the first test, a common orbit is used as a reference for the determination of tracking station coordinates. The results based on the full-rate observation set are compared to those obtained using the normal points. In the second test, the orbit computed from the normal points is compared to that using the full-rate data with all other models and geodetic parameters held to be constant in the two cases. The differences which are obtained are compared to the formal errors of the parameter recoveries.

When the normal points were utilized, they were given individual observation weights:

$$w = \frac{1}{\sqrt{n}} \text{ meters} \tag{4.4}$$

where n is the number of full-rate points in the 2-minute bin used to compute the normal point. In contrast, each of the full-rate ranges was given a weight of 1 m. This preserved the data distribution variation as it is seen in the full-rate data.

Table 4.4 shows the difference obtained in a sampling of the adjusting orbit parameters. Shown is the difference in the inertial X position and velocity component, the along-track acceleration and the coefficient of solar radiation pressure for the normal point vs. full-rate orbit determination results. In each of the orbit parameters, the difference was insignificant

Table 4.4. Test of Orbit Adjustment: Four Stations, 3-Day Arc Values shown are the difference between normal point and full-rate orbital solutions

ΔX	Δ(X/t)	Δ Accel	ΔC <sub>r</sub>
(m)	(m/s)	10 <sup>-11</sup> m/s <sup>2</sup>	
0.004	-0.004	0.001	0.0000

when compared to the noise-only uncertainty obtained in the adjustment assuming 10-cm data noise.

Table 4.5 shows a comparison of the station adjustments obtained (taken with respect to the *a priori* coordinates used in the orbital arc) for the full rate vs. normal point determination. Again, the difference in the two adjustments is a small fraction of the noise-only uncertainty of the results. These tests confirm that the normal point process does not alter the fundamental geodetic signals contained within the full-rate ranging data.

Table 4.5. Test of Station Position Adjustment: Four Stations, 3-Day Arc Values shown are from a priori for normal point and full-rate station coordinate solutions

	Δ <i>X</i> (m)	ΔΥ (m)	Δ Z (m)
Full rate data	-1.327	0.705	0.636
Normal point data	-1.358	0.727	0.652

# 5. Analysis of Estimated Parameters

# 5.1 Assessment of SL7.1 Solution Quality

Before presentation of the geodetic results from the SL7.1 solution, an appreciation of the quality of the solution across time is essential in order to assess the solution's strengths and its limitations. The amount of data entering into the solution as given by the number of LAGEOS normal points (1 normal point = 1 "observation" in the SL7.1 solution) is illustrated in Figure 5.1. It can be easily seen that a marked improvement in observational effort has been achieved during the history of LAGEOS tracking with an apparent seasonal variation in the number of normal points. Large troughs in the graph are probably associated with coincidental poor weather conditions across tracking stations as well as network-wide system upgrade programs (both fixed and mobile lasers) in which many sites experienced a considerable amount of downtime simultaneously (or lack of occupations for mobile sites – this was the case in 1986).

The monthly RMS orbital fit also provides a measure of solution quality for each of the monthly solutions and is shown in Figure 5.2. A dramatic improvement in solution quality is shown over the period of May 1976 to July 1989 whereby RMS orbital fits have dropped from ~30 cm to less than 5 cm. This improvement may not be entirely ascribable to system improvements since there appears to be some level of correlation between the number of normal points and the RMS fits as shown in Figure 5.3. It is well known in least-squares theory that as the number of observations increases, the solution uncertainties will decrease. However, in this case, system improvements most likely account for both the increased number of normal points (a measure of system reliability and more progressive measurement schedules) as well as lower RMS orbital fits as can be seen by distinguishing between pre-1980 data and post-1979 data. Since an obvious temporal grouping can be seen, we conclude that system improvements are more likely the cause for improved RMS orbital fits. This is especially the case for months of relatively few normal point observations (<2000) where even though they lack observations, the overall RMS orbital fit remains in the 5- to 15-cm level.

The SL7.1 solution, as assessed by these general measures, is of significantly lesser quality before 1980. Therefore, some of the analyses of the estimated parameters will disregard these results obtained from these early years of tracking. Between early 1980 and mid 1986, improvement in solution quality was slow but consistent, improving at a rate of ~2 cm/yr, in

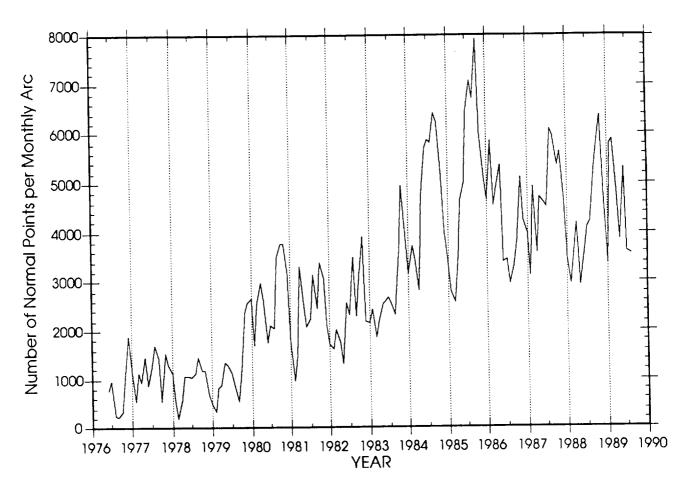


Figure 5.1 Number of monthly normal points utilized in the SL7.1 analysis.

terms of the RMS orbital fit. After 1986, the solution quality has remained rather constant at a level below 5 cm.

# 5.2 Non-Conservative Force Parameters: Estimation and Analysis

# 5.2.1 Introduction

In addition to the main products of the SL7.1 solution (i.e., station positions and Earth orientation parameters), other parameters related to the orbital environment of LAGEOS are also routinely estimated. These parameters (given in Appendix 3) provide useful information to characterize the evolutionary behavior of LAGEOS' orbit. Analyses of these parameters have proven to be useful in isolating remaining systematic behavior as well as providing information for theorists in their determination of physical models to further explain anomalous satellite behavior. In this section, the results and implications of these parameters are discussed and

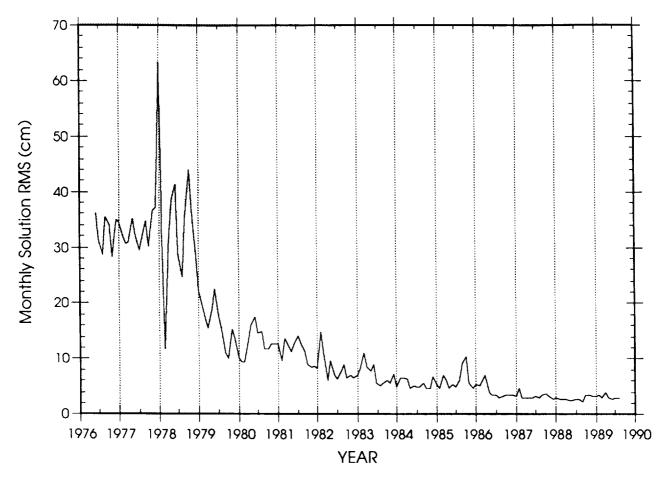


Figure 5.2 Monthly solution RMS orbital fits to LAGEOS. Only data taken after 1980 are used in subsequent spectral analyses of non-conservative force parameters due to the poorer orbital fits in earlier months (shown in the shaded region).

current theories and models are reviewed which, as of this writing, provide consistent explanations to describe a large portion of the systematic aspects that remain in LAGEOS' orbit.

The solar radiation pressure and along-track acceleration parameters are direct effects on LAGEOS which are estimated during the orbit estimation procedure. Fluctuations and trends in these parameters are due to unmodeled effects in the satellite environment which may be modelable or unmodelable, depending on the nature of the effect.

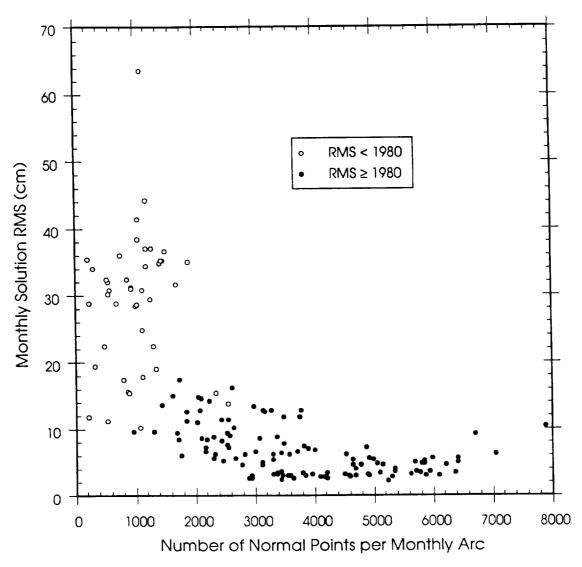


Figure 5.3 SL7.1 monthly solution RMS orbital fits correlated with the number of normal points. Open circles indicate arcs created with data acquired before 1980; blackened circles for arcs created with data acquired hence.

# 5.2.2 Solar Radiation Pressure

Bimonthly values for the solar radiation coefficient as shown by equation (3.12) have been recovered in each of the monthly solutions. The  $C_R$  parameter is estimated in these solutions because it has been shown that it helps reduce the overall solution RMS orbital fits by absorbing as yet unmodeled force parameters. By studying the variations in  $C_R$ , it may be possible to isolate remaining unmodeled phenomena.

Figure 5.4 presents the time evolution of the bimonthly recovered  $C_R$  parameters. LAGEOS' specular reflectivity coefficient  $\rho_s$  is quite small due to the brushed aluminum surface of the areas between corner cubes, therefore,  $C_R$  is not expected to be much larger than 1. In the figure, rather short-period variations occur primarily in the form of large dips of magnitude roughly 0.1 which appear to occur every 37 months. Interestingly enough, these correspond to the period of the node for LAGEOS.

The portion of the time series after 1979 has been spectrally analyzed producing the spectrum shown in Figure 5.5. The spectral decomposition is performed using a weighted least-squares spectral analysis algorithm of *Wells & Vanicek* [1978] where an average linear bias and slope have been removed. Significant peaks can be seen for periods of 1270 days and 550 days. Due to the broad character of the 1270-day peak, it is possible that this peak is associated with the nodal rate of 37 months (approximately 1120 days). The period at 550 days (nearly half of the nodal rate) also contains a considerable amount of power.

The implication of these results is that there remains some unmodeled force (or forces) which is in some way related to the nodal period. This variation in  $C_R$  is a variation in the non-conservative force directed outward from the Sun, and what we see is the least-squares accommodation of the unmodeled effect.

## 5.2.3 Along-Track Acceleration

The orbit of LAGEOS is perhaps the most accurately modeled of any artificial Earth-orbiting geodetic satellite. However, after modeling all of the known forces acting upon LAGEOS, there still remains a residual along-track acceleration that exhibits fluctuations and periodic behavior. Several investigators have reported on this residual acceleration with the general purpose of determining the phenomena that adequately explain the residual behavior, a review of which follows in the next section. By using the formulation explained in Section 3.3.2.1, bimonthly estimates of the along-track acceleration have been recovered in each of the monthly solutions.

The time series for the residual along-track acceleration is shown in Figure 5.6. It is immediately evident that the series is periodic in which a 37-month period is primary. The spectrum of the accelerations is illustrated in Figure 5.7 and exhibits similar character to that determined independently by *Barlier et al.* [1986]. As was the case for the solar radiation

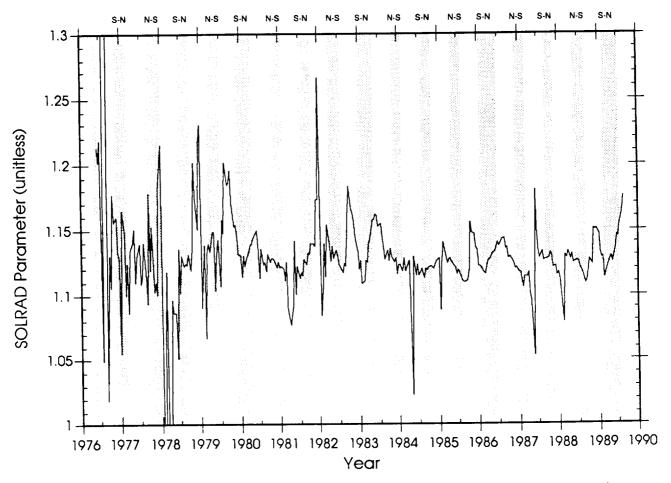


Figure 5.4 Time series of solar radiation pressure parameter (SOLRAD). The "N-S" and "S-N" refer to the orientation of the shadow entry and exit, respectively. Values estimated from 1980 onward were used in the subsequent spectral analysis.

pressure coefficient, two peaks dominate the spectrum. Again, the peak at 1060 days has a fairly broad character which is likely associated with the nodal period of 1120 days. The fact that the peak is skewed in the direction of the nodal period strengthens this conclusion. Again, the peak at 560 days (at half the nodal period) contains a considerable amount of power. The remaining spikes are most probably due to higher order harmonics (e.g., 280- and 140-day periods which correspond to multiples of the nodal frequency) and are probably influenced by the intrinsic noise of the data [Barlier et al., 1986]. A comparison with the radiation pressure coefficient series reveals that the phase of the periodic signature of the along-track acceleration is orthogonal. The correlation diagram in Figure 5.8 shows this quite clearly. The cruciform shape seen in the diagram is a direct outcome of the orthogonal phase relationship. This relationship can be stated as follows: When the along-track acceleration undergoes an excursion away from its mean, the solar pressure coefficient remains at its mean and vice versa.

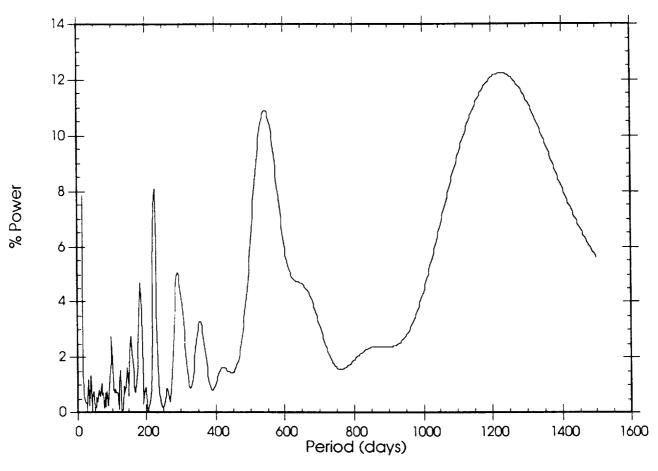


Figure 5.5 Spectral decomposition of the solar radiation pressure.

## 5.2.4 Discussion

From what has been shown, the parameters of the along-track accelerations and solar radiation pressure coefficients behave in a manner that is evidently correlated. Possible sources to explain the average and fluctuating portions of the along-track acceleration behavior were explored in the 1970s by many researchers; these were summarized in an early paper by *Rubincam* [1982]. Further refinements of these proposed models and better measurements to LAGEOS have brought a more complete description of the rather obscure non-conservative forces acting on LAGEOS. These improvements are summarized below.

## 5.2.4.1 Average Along-Track Acceleration

The average along-track acceleration of approximately -3.5 pms<sup>-2</sup> was originally thought to be predominantly due to a combination of charged and neutral particle drag (e.g., *Afonso et al.* [1985] and earlier papers referenced therein). Neutral particle drag was shown to account for

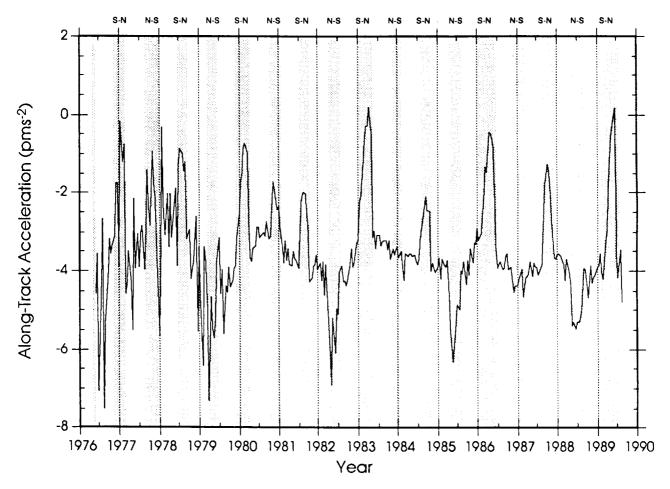


Figure 5.6 Time series of along-track acceleration as experienced by LAGEOS. The "N-S" and "S-N" refer to the orientation of the shadow entry and exit, respectively. Values estimated from 1980 onward were used in the subsequent spectral analysis.

only ~10% of the average along-track acceleration (*Rubincam* [1980] and *Afonso et al.* [1985]). A more recent analysis by *Rubincam* [1990a] indicates that neutral and charged-particle drag on LAGEOS are of similar magnitudes; -0.46 and -0.52 pms<sup>-2</sup> for neutral and charged-particle drag respectively, accounting, in combination, for about 30% of the total along-track acceleration. In most models developed to date, it is typically assumed that these quantities are invariant, but, as pointed out by *Scharroo et al.* [1991], this is not completely true since it is well known that in the case of charged-particle drag, the drag from protons will vary slightly as the Sun/orbit geometry changes.

Rubincam [1987] proposed that the Yarkovsky thermal drag, or the asymmetric thermal response of LAGEOS upon Earth-emitted infrared radiation accounts for -3.33 pms<sup>-2</sup> of the

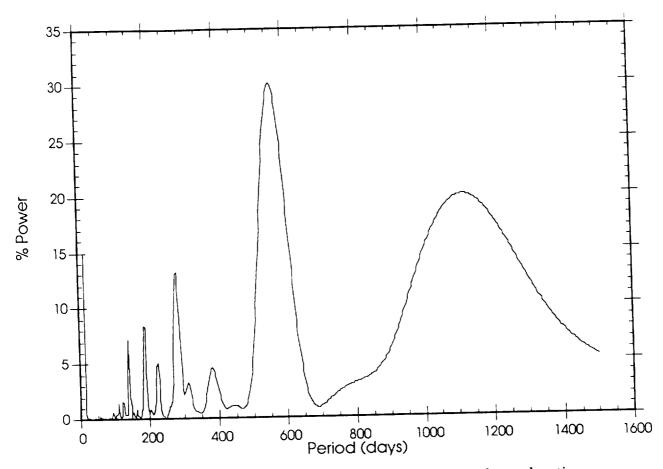


Figure 5.7 Spectral decomposition of the along-track acceleration.

average along-track acceleration observed to be occurring on LAGEOS. This value has since undergone some modification, largely due to refined considerations of the thermal behavior of the corner cubes on-board LAGEOS, to a generally accepted value of -3.08 pms<sup>-2</sup> (*Rubincam* [1988] and *Scharroo et al.* [1991]). The Yarkovsky thermal drag is modeled through (*Rubincam* [1988])

$$S_{ytd} = \langle S_{\text{max}} \rangle [1 - s_z^2 + \frac{1}{2} (3s_z^2 - 1) \sin^2 I + s_z \sin 2I (s_y \cos \Omega - s_z \sin \Omega) + \frac{1}{2} (s_x^2 - s_y^2) \sin^2 I \cos 2\Omega + s_z s_y \sin^2 I \sin 2\Omega]$$
 (5.1)

where  $\langle S_{\rm max} \rangle$  = -3.08 pms<sup>-2</sup>, l is the inclination of the orbit,  $\Omega$  is the right ascension of the ascending node (a function of time, given by  $\Omega = \Omega_o + \dot{\Omega} (t-t_o)$ ) where  $\dot{\Omega}$  is the rate of change of the ascending node and  $\Omega_o$  is the epoch position of the ascending node at time  $t_o$ ). The

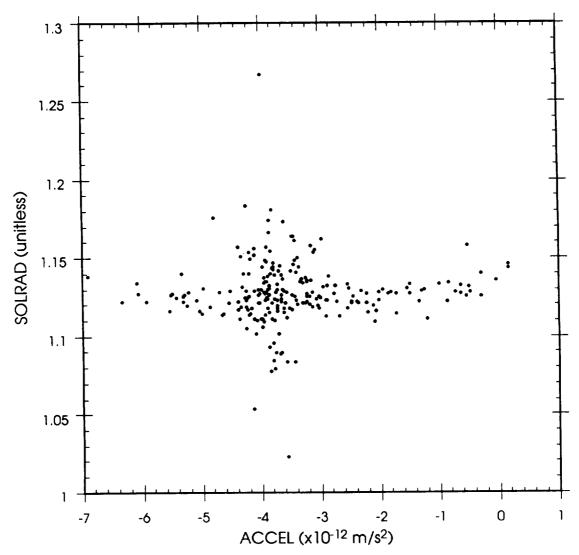


Figure 5.8 Correlation plot of SOLRAD vs. ACCEL.

 $s_x$ ,  $s_y$ ,  $s_z$  are the unit vector components of the spin axis of LAGEOS in an Earth-centered, celestial coordinate system, given by

$$s_{x} = \sin \theta \cos \lambda$$

$$s_{y} = \sin \theta \sin \lambda$$

$$s_{z} = \cos \theta$$
(5.2)

where  $\theta$  and  $\lambda$  are the co-latitude and right ascension of the direction of LAGEOS' spin axis. Originally, the angle  $\theta$  was thought to be constant at ~22° with respect to the Earth's spin axis, but recently, assessments of magnetic and gravitational torques have shown that LAGEOS' spin

axis has been changing as a function of time [Rubincam, 1990a]. In the work by Scharroo et al. [1991], they have made the assumption that the spin axis of LAGEOS is slowly aligning itself to the Earth's spin axis due to the magnetic torque experienced by LAGEOS' passage through the Earth's magnetic field. This has the effect of reducing the amplitude of the variation of the modeled effect. More recently, Bertotti and Iess [1991] have proposed that as the spin axis of LAGEOS comes into close alignment with the Earth's spin axis, gravitational torques will predominate over the forcing of the satellite's spin axis, sending LAGEOS into a chaotic tumbling state of spin. Their prediction is that LAGEOS will reach this chaotic state sometime in late-1991 or in 1992.

For the purposes of discussion here, the exponential progression of the alignment of LAGEOS' spin axis towards the Earth's spin axis has been adopted in a manner similar to that described by *Scharroo et al.* [1991] whereby the spin axis co-latitude decreases by 50% every 6 years; a value which has also been determined empirically by *Ries* [1991]. The combined effects of the Yarkovsky thermal drag and neutral and charged-particle drag are shown superimposed on the observed along-track acceleration in Figure 5.9a with the residual along-track acceleration after removing these effects being shown in Figure 5.9b. With the removal of the average along-track acceleration, the residual acceleration is now centered about zero but still contains excursions (or spikes) from the mean for which explanations have been proposed—discussed in the next paragraphs.

#### 5.2.4.2 Along-Track Acceleration Spikes

Much effort has been spent by several researchers to understand the excursions that had been seen in the along-track acceleration parameter recovered from LAGEOS orbital analyses. Recently, *Scharroo et al.* [1991] have offered two models which reproduce the data remarkably well, at least for the time span from which their analysis was made as the prediction capability of their proposed algorithm appears to degrade after 1989.

The first model was put forth in detail by *Rubincam et al.* [1987] in which it was suggested that an asymmetry of the reflectivity of the satellite might cause the observed excursions in the along-track acceleration parameters. It has further been shown that even small differences in hemispheric reflectivity of LAGEOS could cause a portion of the observed spikes. The model is somewhat controversial because little pre-flight evidence exists that would indicate a variation in albedo on LAGEOS. The surface of the satellite was presumably manufactured in a uniform way and ground tests made on LAGEOS II indicate less than 2% hemispheric

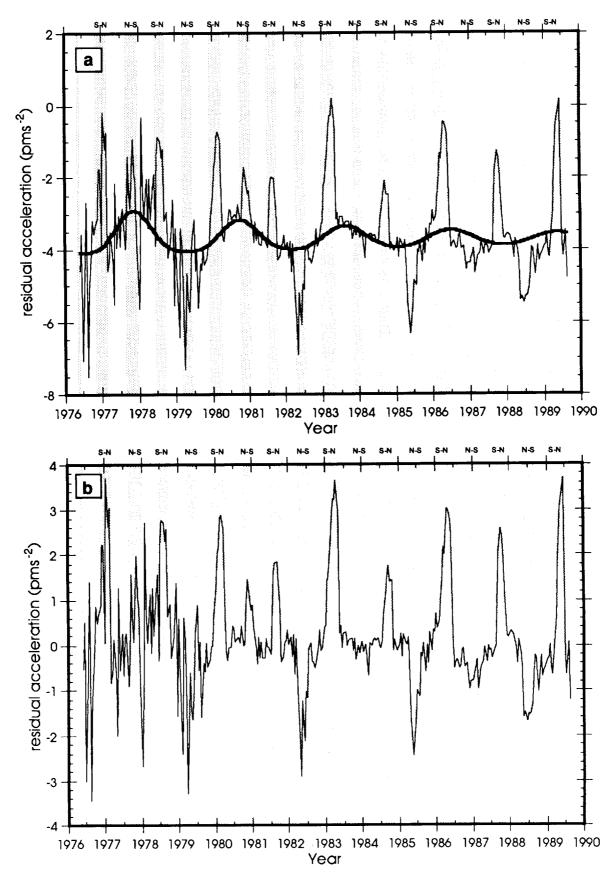


Figure 5.9 (a) Theoretical Yarkovsky thermal drag on LAGEOS shown (heavy line) superimposed on the total along-track acceleration determined by the SL7.1 analysis. (b) Residual along-track acceleration after removal of the Yarkovsky Thermal drag.

variation in reflectivity (*Rubincam*, [1990b]). Nonetheless, *Scharroo et al.* [1991] maintain that a hemispheric reflectivity variation of only 5% adequately explains the observed behavior, the source of which remains an intriguing mystery.

Anisotropic reflection of sunlight, assuming anisotropy exists on the satellite, will cause a recoil in the direction of the region or zone having the lower albedo, since fewer solar photons will rebound in this region. For a satellite having hemispheric variation in albedo and in the course of an orbit, this effect will largely cancel out if the satellite's orientation remains reasonably fixed in inertial space and if the orbit remains in full sunlight. When a portion of the orbit passes through the Earth's shadow, the recoil ceases, thereby causing an apparent force to act on the satellite and giving a net result which has all the appearances as that of an acceleration. Whether the effect takes form as a positive or negative acceleration is strictly a function of which satellite hemisphere enters the shadow zone first. The model takes a relatively simple form as outlined in *Rubincam et al.* [1987] and *Scharroo et al.* [1991]. (The formulation below is from the latter.)

$$S_{ani} = \frac{1}{2\pi} \ddot{s}_{\text{max}} (A_1 - A_2) \sin^2 \theta_r$$
 (5.3)

where  $\ddot{s}_{\text{max}}$  = -12.1 pms<sup>-2</sup>,  $\theta_r$  is the angle between the spin axis of LAGEOS and the Sun,  $A_1$  and  $A_2$  are LAGEOS' unit spin vector mapped onto the direction of the satellite radius vector from the Earth's center at moment (1) when the satellite enters the Earth's shadow and at moment (2) when the satellite exits the Earth's shadow. Once again, the spin axis of LAGEOS is assumed in this work, to be slowly re-aligning itself with the Earth's spin axis.

The second effect proposed by *Rubincam* [1982] and developed later in detail by several investigators is known as the Yarkovsky-Schach effect. This effect shares similar concepts with both the Yarkovsky Thermal Drag model and the anisotropic reflectivity models already mentioned. The Yarkovsky-Schach effect is again a consequence of photon thrust, but in this case we are concerned with solar-produced photons. The effect is similar to the anisotropic reflectivity model in the sense that both are due to the thrust (or recoil) ceasing during the time LAGEOS spends in the Earth's shadow. Again, borrowing from the derivation given in *Scharroo et al.* [1991], the Yarkovsky-Schach model is formulated as

$$S_{yse} = \ddot{S}_{max} \frac{(A_1 - A_2) + u_o(B_1 - B_2)}{2\pi (1 + u_o^2)} \cos \theta_r$$
 (5.4)

where all values are defined as before with the exception that  $\ddot{s}_{\text{max}} = -89.4 \text{ pms}^{-2}$ ,  $u_0 = 1.45 \text{ rad}$ , a constant expressing the thermal response time of a retroreflector, and  $B_1$  and  $B_2$  are like  $A_1$  and  $A_2$  except now the unit spin vector is mapped onto the along-track direction of the satellite at entry and exit points as the orbit passes through the Earth's shadow.

The sum of the anisotropic reflectivity and the Yarkovsky-Schach effects is shown in Figure 5.10a. The residual acceleration is fairly well modeled by these two effects, but some residual spikes can be seen in Figure 5.10b which seem to exhibit some amount of systematic behavior.

# 5.2.4.3 Along-Track Acceleration Modeling: Discussion

A substantial amount of the signal in the along-track acceleration can be accounted for by the combination of the four models; charged and neutral particle drag; Yarkovsky Thermal drag; anisotropic reflectivity of LAGEOS; and the Yarkovsky-Schach effect. With the exception of the charged and neutral particle drag, all models are dependent upon the direction of the spin axis of LAGEOS. Throughout the present discussion, it has been assumed that the spin axis is slowly realigning itself with the Earth's spin axis as suggested by *Scharroo et al.* [1991]. However, there is evidence that this simple behavior of the spin axis may not be entirely correct.

First, in carefully examining the behavior of the final residual acceleration (shown in Figure 5.10b), the amount of scatter seems to increase after early 1988. In follow-on GSFC solutions to SL7.1 and in the solution of *Ries* [1991], it has been noted that in early 1990, the along-track acceleration exhibits an unexpected positive excursion having an amplitude of ~2 pms<sup>-2</sup>. The models, as presented here, fail to predict this spike which further raises questions regarding the orientation of LAGEOS' spin axis. If the prediction of *Bertotti and less* [1991] is valid, then it may be that the onset of a new spin axis dynamic, namely of a chaotic state, is the root cause of the 1990 spike. It is anticipated that if the spin axis begins to tumble in an uncontrolled fashion, the effects of the Yarkovsky thermal drag, the anisotropic reflectivity and Yarkovsky-Schach effect will be reduced, leaving approximately -1 pms<sup>-2</sup> of along-track acceleration due to charged and neutral particle drag. In essence, the spiky nature of LAGEOS' along-track acceleration should be dramatically reduced as well as ~70% of the average along-track acceleration. The state of chaotic behavior is predicted to begin in late 1991 or 1992.

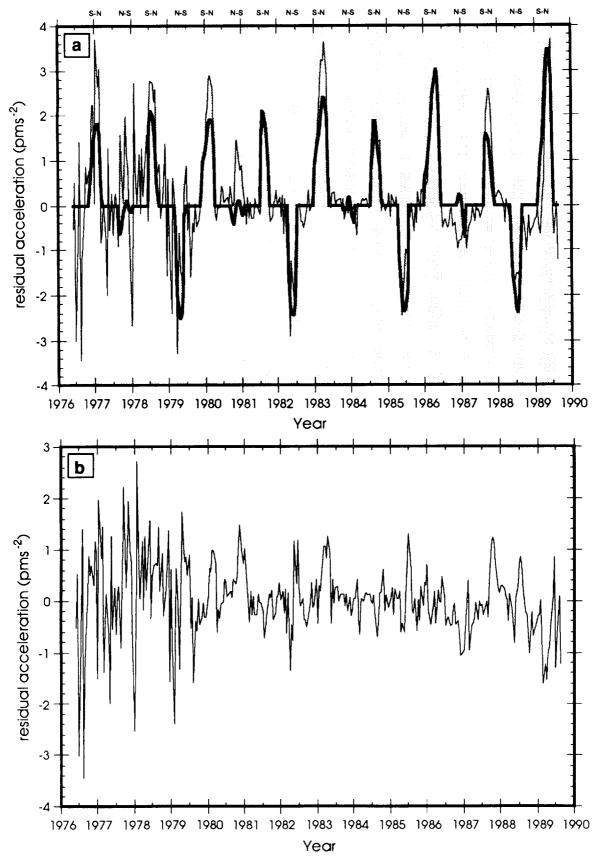


Figure 5.10 (a) Sum of theoretical anisotropic thermal response from Earth infrared radiation and Yarkovsky-Schach photon thrust (heavy line) superimposed on the residual acceleration shown in Figure 5.9b. (b) Residual acceleration after further removal of the anisotropic and Yarkovsky-Schach effects. In this chart, all proposed sources of acceleration variations have been removed.

Continued LAGEOS observations and analyses over this time period will clearly show whether or not the gravitational torque will become dominant, as expected by *Bertotti and less* [1991].

Finally, in Figure 5.11, the spectrum of the residual along-track acceleration (after 1979) is shown. Peaks at 885 and 140 days dominate the spectrum. The sources of the peaks remain unexplained. The lack of peaks at the nodal and half-nodal periods indicates that the models described here are effectively removing the signal at these periods.

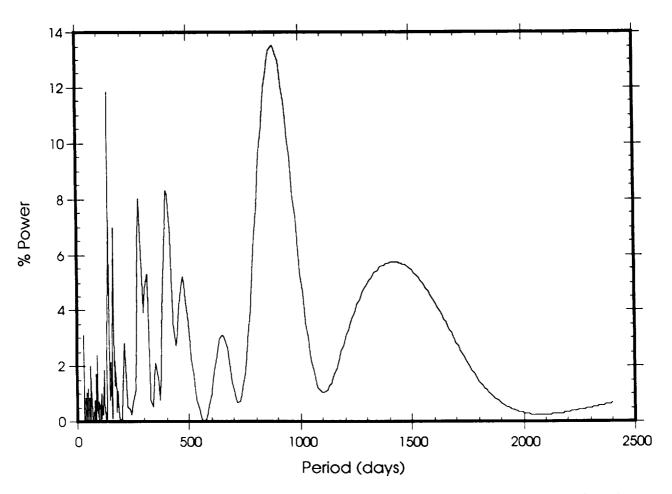


Figure 5.11 Spectral decomposition of the residual along-track acceleration after the effects of the four models have been removed. The five largest peaks are centered at 885, 140, 405, 283 and 163 days, respectively.

# 5.3 Orbit Evolution Studies

Analysis of LAGEOS' orbital evolution provides one means of assessing errors in the adopted models (gravitational, tidal, etc.) and errors entering into the solution from unmodeled sources. Several techniques have been devised to examine the long-term behavior of LAGEOS' orbital elements. In all of these techniques, it is desirable for the effects of the short-period variations to be minimized in order to understand the longer term fluctuations.

In our analysis, we have chosen to consider the Keplerian elements evaluated when the satellite arrives at a given position, rather than at a given time. Differences in the Kepler elements chosen in this manner from two differently computed osculating orbits reveal the long-period variations due to the different modeling. This enables the estimation of the Kepler element variations due to the errors in the adopted models. These variations must then be interpreted.

## 5.3.1 Methodology

The largest short-period perturbations are due to the Earth's oblateness ( $J_2$ ). The effects of the Earth's oblateness on the Keplerian elements of a near-Earth satellite are given by *Merson* [1961]. Expressions for the departures  $\delta a$ ,  $\delta e$ ,  $\delta i$ , and  $\delta \Omega$  from nodal conditions are presented in equations (35 - 38) from *Merson* [1961]:

$$\delta a = J_2 R^2 a^2 p^{-3} \left[ (1 - e \cos \nu)^3 \left( 1 - 3fS^2 \right) - \left( 1 + e \cos \omega \right)^3 \right] + O(J_2^2)$$
 (5.5)

$$\delta e = 3J_2 \left(\frac{R}{p}\right)^2 \left[ \left(-\frac{1}{2} + \frac{f}{3}\right) \cos \omega - \frac{1}{4}e(1 + \cos 2\omega) + \left(-\frac{1}{8} - \frac{f}{3}\right)e^2 \cos \omega \right.$$

$$\left. - \frac{1}{24}e^2 \cos 3\omega - \frac{1}{2}feS^2 - \frac{3}{2}feS^2 \cos^2 v + \frac{1}{2}e\cos^2 v \right.$$

$$\left. + -\frac{1}{3}f(1 - e^2)C\cos \omega + \frac{1}{2}\cos v - \left(\frac{7}{6} + \frac{1}{3}e^2\right)fS^2 \cos v \right.$$

$$\left. - \frac{1}{2}fe^2S^2 \cos^3 v + \frac{1}{6}e^2\cos^3 v \right] + O(J_2^2)$$
(5.6)

$$\delta i = -3J_2 \left(\frac{R}{p}\right)^2 \sin i \cos i \left[\frac{1}{2}S^2 + \frac{1}{3}e\cos\omega + \frac{1}{3}S^2e\cos\nu - \frac{1}{3}Ce\cos\omega\right] + O(J_2^2)$$
 (5.7)

$$\delta\Omega = -3J_2 \left(\frac{R}{p}\right)^2 \cos i \left[\frac{u}{2} + \frac{2}{3}e\sin\omega - \frac{1}{2}SC + \frac{1}{3}S^2e\sin\nu - \frac{2}{3}Ce\sin\omega\right] + O(J_2^2) \quad (5.8)$$

in which  $a, e, i, \Omega, \omega$  are the traditional Keplerian elements of the orbit and where:

$$J_2$$
  $\approx 1.1 \times 10^3$   $u = \omega + v$ 
 $R$  is the Earth's equatorial radius  $S = \sin u$ 
 $P = a(1-e^2)$ ; the orbit's latus rectum  $C = \cos u$ 

and  $f = \sin^2 i$ 

By grouping terms that are scaled by e and its higher orders, equations (5.5) through (5.8) can be expressed as

$$\delta a = J_2 R^2 a^2 p^{-3} \left[ -3fS^2 + e\Delta a \right] + O(J_2^2)$$
 (5.9)

$$\delta e = 3J_2 \left(\frac{R}{p}\right)^2 \left[ \left( -\frac{1}{2} + \frac{f}{3} - \frac{1}{2} fC \right) \cos \omega + \left( \frac{1}{2} - \frac{7}{6} f^2 \right) \cos v + e \Delta e + O(e^2) \right] + O(J_2^2) (5.10)$$

$$\delta i = -3J_2 \left(\frac{R}{p}\right)^2 \sin i \cos i \left[\frac{1}{2}S^2 + e\Delta i\right] + O(J_2^2)$$
 (5.11)

$$\delta\Omega = -3J_2 \left(\frac{R}{p}\right)^2 \cos i \left[\frac{u}{2} + \frac{1}{2}SC + e\Delta\Omega\right] + O(J_2^2)$$
 (5.12)

in which  $\Delta a$ ,  $\Delta e$ ,  $\Delta i$ , and  $\Delta \Omega$  are functions of the arguments of the satellite's motion ( $\omega + \nu$ , which are rapidly changing during an orbit). Since e is small for LAGEOS, the major terms in each of the equations (5.9), (5.11) and (5.12) are only functions of the motion of the satellite projected on the Earth's surface and consequently contribute no variation in the differences of the elements when two differently computed osculating orbits are evaluated at the same argument of latitude (u). The eccentricity variation of equation (5.10) does not share this property, but, as it turns out, this element is affected by  $J_2$  significantly less than are the other orbital elements.

As can be seen in the more general formulation of *Kaula* [1967] (equation 3.76), all of the short-period gravitational variations should similarly cancel. Using the same approach, it can also be shown that this is also approximately the case for third-body and non-conservative perturbations, especially if the satellite positions in the trajectories to be compared reach the same latitude at nearly the same time (i.e., the along-track difference between trajectories is not excessively large). The limitation of this approach is that the deviations in the mean orbits must not exceed the amounts describable by the first-order theory we have applied.

The elements of an orbit determined from a continuous data span (in this case, of 30 days duration) are evaluated at a given argument of latitude: we chose u = 0, the equator crossing (thereby causing S = 0 and C = 1 in the above equations), although previous analyses [Smith and Dunn, 1980 and Dunn et al., 1973], have considered  $u = \pi/2$  which is the point of maximum latitude. These "short arc" elements follow the real satellite orbit in the chosen "Equator crossing" space, but are averaged over the 30-day data interval. In our procedure, they are compared with Keplerian elements evaluated at the Equator crossing points from an orbit calculated over a time span of several years based on the May 1976 initial orbital state. The differences between the "short-arc" and "long-arc" elements shown in Figures 5.12 through 5.16 are measures of the effects of error in the force model used in the orbit determination process and errors introduced from unmodeled sources on Keplerian elements, but are significantly unaffected by short-period terms due to  $J_2$ . The differences are similar to those computed using mean elements but offer the advantage of direct evaluation during the data reduction process using GEODYN's versatile numerical integration scheme.

## 5.3.2 Results and Discussion

The slight downward trend observed in the semi-major axis residuals (Figure 5.12) suggests that the along-track acceleration value (-3.1 pms<sup>-2</sup>) adopted in calculation of the long arc is slightly higher than the true average. This is indeed the case. The along-track acceleration was shown in the previous section (Figure 5.6), and its mean calculated from the bi-monthly estimates is -3.44 pms<sup>-2</sup>. The excursions about a secular trend correspond to the data excursions in the along-track acceleration described in Section 5.2. The  $\pm$  0.2 ppm variations in the difference of the eccentricity (Figure 5.13) may be a result of error in the odd zonal terms of the geopotential and any seasonal variation in them, as well as by any Earth albedo effects and satellite thermal effects, which will additionally influence the length of the semi-major axis.

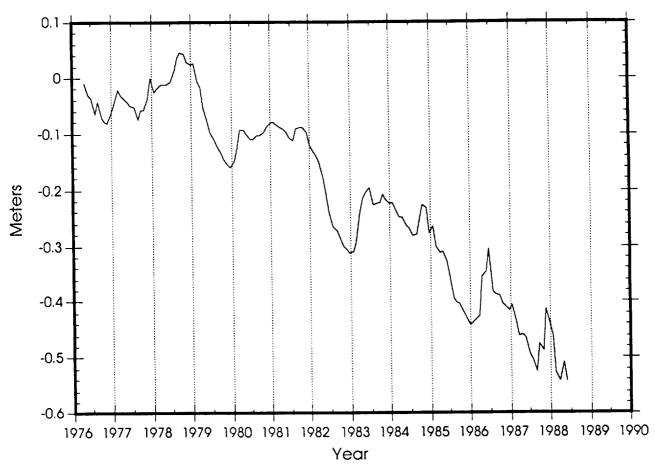


Figure 5.12 Monthly semi-major axis differences taken with respect to a single multi-year orbit calculated using identical force models beginning with the same initial conditions. An assumed average along-track acceleration of -3.1 pms<sup>-2</sup> has been applied in this chart and in the next 4 figures. The remaining linear trend is due to the fact that the actual along-track acceleration is closer to -3.4 pms<sup>-2</sup>.

A small upward trend in the inclination residuals (Figure 5.14) can also be attributed to the thermal drag effect described by Rubincam [1988] and  $Farinella\ et\ al.$  [1990], but the periodic effects are mainly caused by residual error in the tidal model and possibly by the Yarkovsky-Schach effect [Farinella\ et\ al., 1990]. The Earth and ocean tidal errors will produce signatures in the node (Figure 5.15), among which would be included seasonal variations in the SA (annual) and SSA (semi-annual) tidal amplitude [Smith\ and\ Dunn, 1980]. The large secular effects in the node residuals are due to a combination of the effect of mis-modelling the 18.6-year zonal Earth tide by assuming that  $k_{2,f}$  = .30 for this tide with zero phase and neglected ocean tides at this period and that of the rate of change of the second zonal harmonic caused by post-glacial rebound [Rubincam, 1984]. A few more years of tracking are required for the full

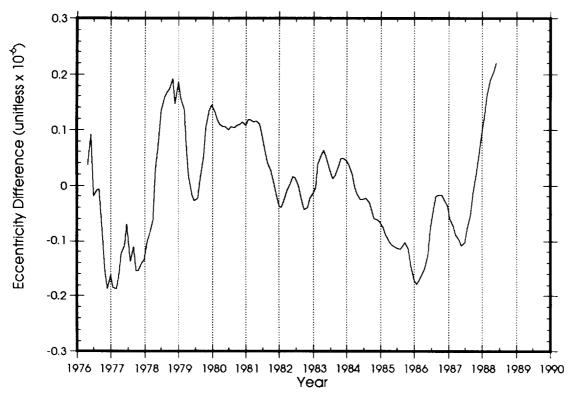


Figure 5.13 Monthly eccentricity differences taken with respect to a single multi-year orbit calculated using identical force models beginning with the same initial conditions.

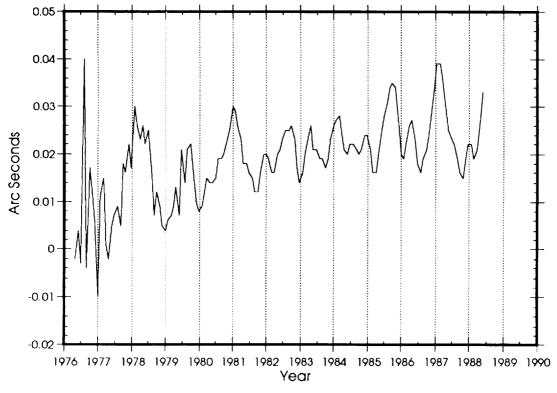


Figure 5.14 Monthly inclination differences taken with respect to a single multi-year orbit calculated using identical force models beginning with the same initial conditions.

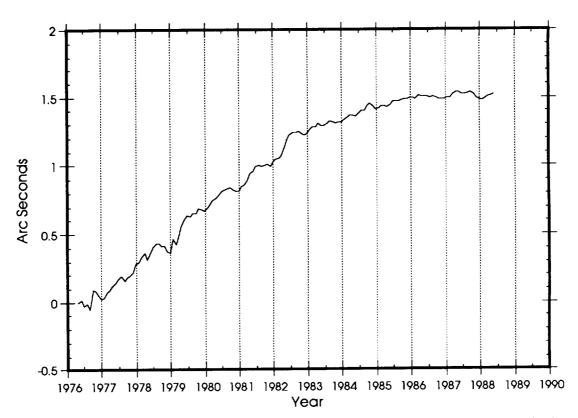


Figure 5.15 Monthly differences of the right ascension of the ascending node taken with respect to a single multi-year orbit calculated using identical force models beginning with the same initial conditions.

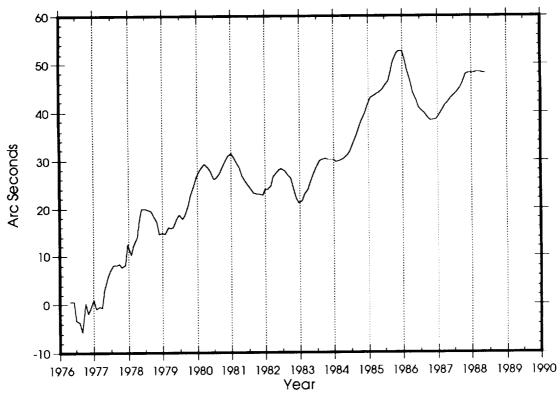


Figure 5.16 Monthly differences of the argument of perigee taken with respect to a single multi-year orbit calculated using identical force models beginning with the same initial conditions.

separation of these two effects. The argument of perigee variation (Figure 5.16) largely corresponds to excursions in the eccentricity.

#### 5.4 Earth Orientation

It has already been discussed in the section on Reference Frames (Section 3.1) that polar motion and variations in the Earth's rotation rate must be determined through observation. In the discussion below, the polar motion and Earth orientation results obtained from the analysis of the LAGEOS laser ranging data is presented. The averaging intervals for the recovered Earth orientation parameters have been chosen for convenience to correspond to those of the BIH Circular D publication .

#### 5.4.1 The SL7.1 EOP Series

The values of the SL7.1 recovered EOP series are given in Appendix 4. The series was obtained from a "global" solution (cf. Section 2.3) where all station motions were modeled with an adopted tectonic model; AM0-2 of *Minster and Jordan* [1978]. The horizontal position of Greenbelt, Maryland was unadjusted and constrained to move with AM0-2 motion as was the latitude of Maui, Hawaii. In addition to these, the first epoch estimate of A1-UT1R (the difference between atomic time (A1) and universal time regularized to account for tidal effects (UT1R)) was constrained in each arc, so that it could be decoupled from the node of LAGEOS.

Figures 5.17 through 5.20 graphically depict the estimated series of the coordinates of the pole in the usual conventional frame, the length-of-day, and its variations obtained by forward differencing of the estimated length-of-day (A1-UT1R) values. In Figures 5.21 through 5.23 are shown the standard deviations associated for each of the three components of the EOP series. It is remarkable how vividly the latter reflect the changes in the tracking network strength and the precision of the ranging instruments. Disregarding short transition periods in between major eras, one can clearly identify the existence of three such eras:

1976 - 80:	Weak network, low-precision instruments
1980 - 84:	Better network, higher precision instruments
1984 - 89:	Strong network, high-quality instruments

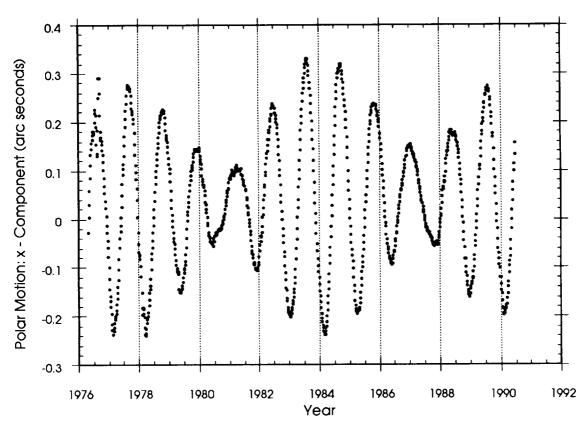


Figure 5.17 The x - component of the pole as recovered from the SL7.1 solution.

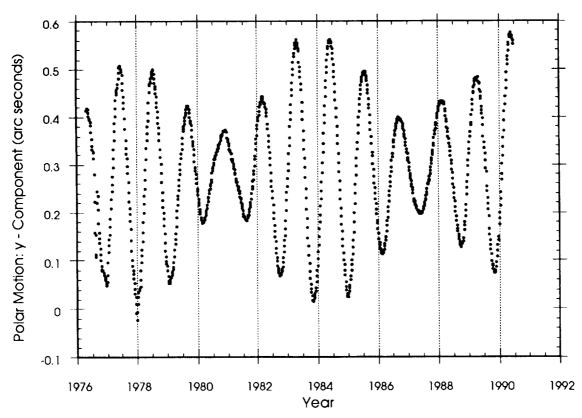


Figure 5.18 The y - component of the pole as recovered from the SL7.1 solution.

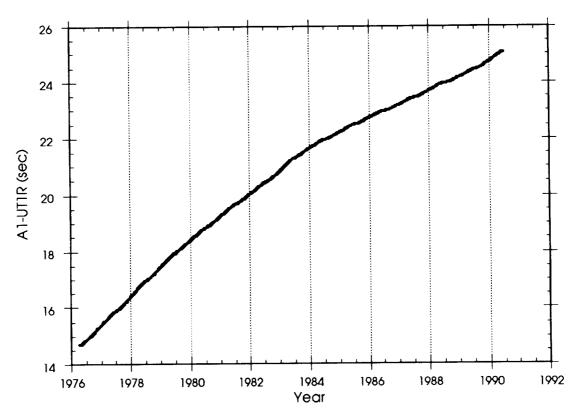


Figure 5.19 Length-of-day parameter (A1-UT1R) receovered by the SL7.1 solution.

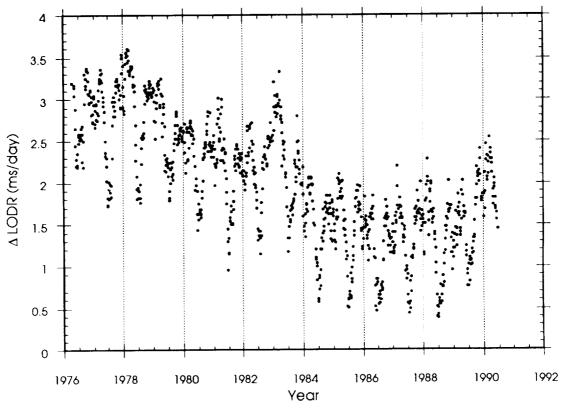


Figure 5.20 Change in the length of day as recovered by the SL7.1 solution.

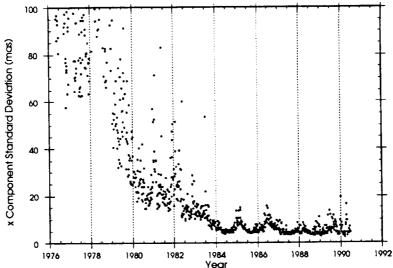


Figure 5.21 Standard deviations in the recovery of the x - component of polar motion.

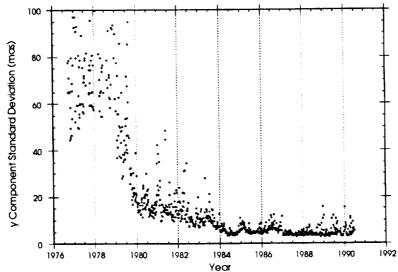


Figure 5.22 Standard deviations in the recovery of the y - component of polar motion.

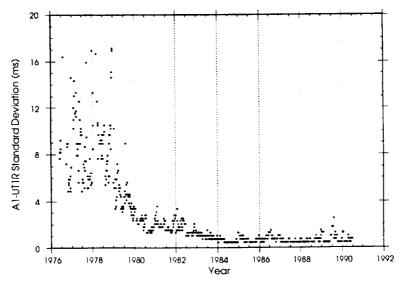


Figure 5.23 Standard deviations in the recovery of the length-of-day.

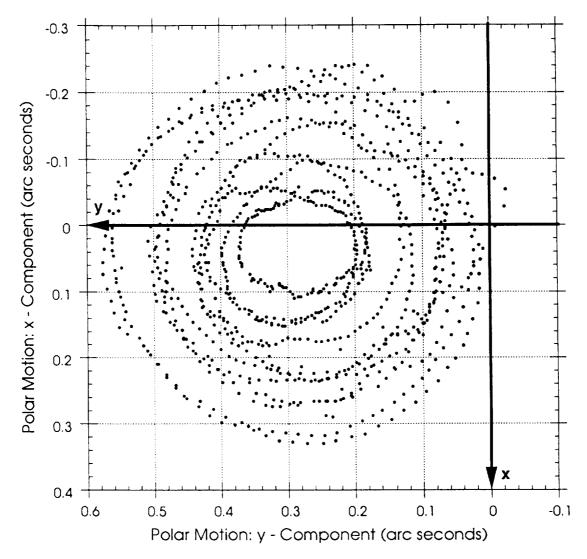


Figure 5.24 The polhode, or path of the pole, for the period May 1976 to July 1990 as recovered from the SL7.1 solution.

In Figure 5.24, there is shown a plot of the polhode, the actual trajectory of the Celestial Ephemeris Pole as determined in SL7.1, projected on a plane tangent to the Earth's surface at the Conventional International Origin (CIO).

# 5.4.2 Uniformization of the EOP Solution

The analysis of the SLR data produces a continuous series for polar motion (both components), and a discontinuous series of Earth rotation variations. The inability to separate the absolute magnitude of the Earth's angle of orientation in space from the satellite node requires us to

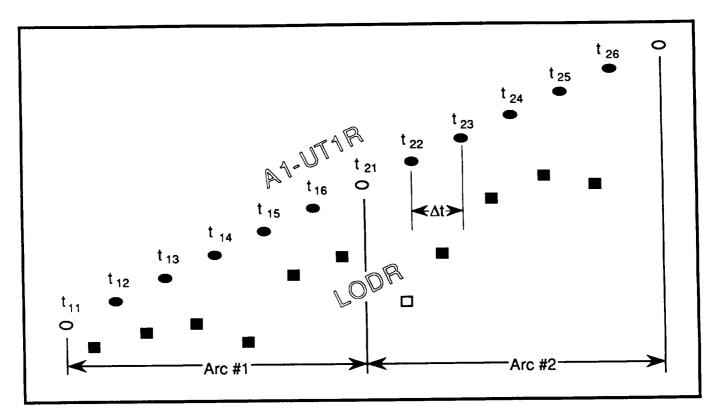


Figure 5.25 Method for uniformization of the estimated Earth orientation parameters. Two arcs are shown. The A1-UT1R series is depicted as ovals and the LODR series is depicted as rectangles. The open ovals indicate that A1-UT1R is constrained to BIH values. In the case of  $t_{11}$ , the BIH value is adopted to reference the uniform series. The solid ovals indicate values of A1-UT1R estimated in the solution. The solid rectangles indicate values of LODR determined from forward differencing of adjacent A1-UT1R values. The open rectangle indicates that LODR has been interpolated by cubic splines.

constrain the initial value of A1-UT1R in each of our independent arcs to its *a priori* value. If the constrained values are not consistent with the ensemble of values estimated, then the series will exhibit severe discontinuities at these nodal points.

Similar discontinuities exist in the derivative of the A1-UT1R parameter, the variation of the length of day,  $\Delta$ LODR. Despite the fact that absolute orientation angles are not estimable from the data, their relative variations are. What we have done therefore, is to determine the  $\Delta$ LODR series from the estimated A1-UT1R series and then determine, through spline interpolation, the missing values of  $\Delta$ LODR at the nodes between arcs. Figure 5.25 illustrates these concepts. Once the  $\Delta$ LODR series is rectified and complete, one only needs a starting value of A1-UT1R to reverse the forward difference procedure and integrate the  $\Delta$ LODR series into a continuous A1-UT1R series

$$(A1 - UT1R)_{unified}(t) = (A1 - UT1R)_{unified}(t - \Delta t) + (\Delta t)\Delta LODR\left(t - \frac{\Delta t}{2}\right) \quad (5.13)$$

In applying this procedure we also smooth the final series using the Vondrák filter [Vondrák, 1977] with a weak smoothing parameter  $\varepsilon = 10^{-4}$  which effectively suppresses the periods below 20-30 days. It is the rectified and smoothed series that was shown in the figures discussed above. This series is then in a form which can be used in comparison and time domain studies [cf. Pavlis, 1991].

The secular nature of the smoothed pole series was reported by *Pavlis* [1990] in which the secular trend of the pole was calculated from an 8-year span of polar motion data to be 3.3 mas/yr in x and 2.6 mas/yr in y giving a direction of approximately 38° E longitude with respect to the CIO.

#### 5.5 Elastic Earth Parameters

In addition to the Earth orientation parameters, the global elastic parameters  $h_2$  and  $l_2$  (Love numbers) associated with the station tidal variations were estimated. The adjusted  $h_2$  is 0.627  $\pm$  0.004 as compared with the Wahr *a priori* of 0.609 and the adjusted  $l_2$  is 0.0986  $\pm$  0.002 as compared with the Wahr *a priori* of 0.0852. The standard deviations given are three times the formal standard deviation of the global solution. The differences from the *a priori* are formally significant: however, they represent variations in station positioning at the 1- to 5-mm level which could well be due to neglecting a model for the site dependent ocean loading. The discrepancies are at the 4% level for  $h_2$  and the 16% level for  $l_2$ .

Previous recoveries of these parameters provide similar values for  $h_2$  and  $l_2$ : Christodoulidis et al. [1985] presented  $0.608 \pm 0.003$  for  $h_2$  and  $0.0934 \pm 0.002$  for  $l_2$  from analyses of the 1980-1983 LAGEOS tracking data. Carter et al. [1985], using VLBI data taken 1980-1984 determined values of  $0.6135 \pm 0.0054$  and  $0.0768 \pm 0.0191$  for  $h_2$  and  $l_2$ , respectively. Gendt and Dietrich [1988] estimated  $h_2$  and  $l_2$  to have values of  $0.610 \pm 0.003$  and  $0.099 \pm 0.002$ , respectively, based on their analysis of September 1983 to May 1985 LAGEOS tracking data. While none of these results are clearly inconsistent with the others, the values disagree by more than would be expected from their uncertainties; this behavior is more typical of model errors than geophysics.



Gendt and Dietrich [1988] have shed some light on this: they also evaluated  $h_2$  and  $l_2$  from their data on a station- by-station basis, recovering  $0.598 \pm 0.012$  for  $h_2$  and  $0.092 \pm 0.009$  for  $l_2$  as the respective means of their independent local determinations. The range of well-determined values was between 0.4 and 0.7 for  $h_2$  and between 0.02 and 0.24 for  $l_2$ . The individual station recoveries provide estimates of  $h_2$  and  $l_2$  which are formally distinct from the global mean estimate by significant multiples of the formal error of determination. They are observing the same type of behavior we see in comparing the solutions of different investigators, and the implication is that the data do not fully conform to the model. We suspect that unmodeled ocean loading effects are strong candidates for being the major source of the model error here. This will be considered in future analyses.

# 6. The Estimation of Station Coordinates and Reference Frame Realization

In Section 3.1, reference systems were described and reference frames, as applied to the analysis of laser range data, were considered. One of the ultimate goals of the SL7.1 solution is to simultaneously realize the CTRS and determine the individual motions of the tracking stations. Ideally, the solution should be completely robust and all estimable quantities of interest (including those that vary with time) should be solved for in a singular, massive inversion. Due to software restrictions, the estimation of the station motions could only be achieved through a series of individual station position determinations spanning the tracking history of the network. In other words, the GEODYN/SOLVE analysis system was limited in its capability to directly estimate epoch positions while simultaneously estimating tracking site velocities.

Given the limitations of the software system, the procedure which was used can be outlined as follows. Within each solution period, the motion of each station was modeled according to the adopted tectonic model (AM0-2). It is important to try to keep the time span of each solution as short as possible so that the resulting station positions are not contaminated by errors in the underlying tectonic model. Additionally, if the solution period was made too long, the detection of episodic events and station hardware problems may become overly averaged and possibly go undetected. Once the series of station positions are available, their time histories of latitude, longitude, and height can be determined by weighted least-squares line fits to these quantities or, better, they can be estimated via a combined adjustment of the ensemble of interstation distance variations. A graphical outline of the data reduction process which was followed to estimate tracking site velocities is shown in Figure 6.1. The remaining sections of the chapter will describe the details of this process.

# 6.1 Requirements for High Temporal Resolution Analysis

The analysis of variations in the length of the distance between tracking sites provides the basis for the inference of station motions in SL7.1. Given the aforementioned software limitations, we chose to determine the motion of the stations based on the interstation distance rates. This approach was taken for primarily two reasons. The first is that interstation

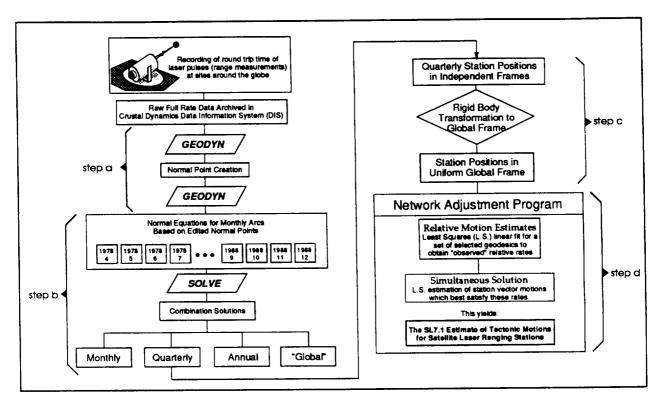


Figure 6.1 SL7.1 solution design. Step "a" on normal points was discussed in Section 4.2. The software system was described in Section 2.2. The various solution types were described in Section 2.3. The remainder of the present chapter will focus on steps "c" and "d."

distances are by and large uncorrelated, which then allows for the removal of off-diagonal terms within the covariance matrix without appreciable loss of accuracy. The second reason is due to the fact that the estimated station positions are directly dependent on the underlying reference frame. Since the reference frame from one estimation period (quarter) to the next is linked only through an *a priori* constraint, the stability of the reference frame is data dependent and therefore does not yield completely consistent station motion estimates based exclusively from the time histories of the geodetic coordinates themselves (this is discussed further in the next section).

Since the horizontal motion of the stations is of primary interest in assessing global tectonic behavior, it is required that all station positions be reduced to a common surface upon which distance computations are performed. A natural choice for the reference surface is an ellipsoid of revolution, such as is typically used for continental geodetic networks. The network computations are made with respect to the internationally accepted GRS-80 ellipsoid having a semi-major axis of 6378137m and a flattening of 1/298.257 [Moritz, 1988]. The last decision to be

made is the "type" of interstation distance to be analyzed. Given the fact that the reference surface is an ellipsoid, there are two choices for a unique definition of interstation distance. These include the *spatial chord* connecting the projections of the two station positions on the ellipsoid, and the *geodesic line*, the curve on the ellipsoid's surface with the shortest length between the two projected positions.

The geodesic line, or shorter, the geodesic (sometimes called the geodetic line in some texts), was chosen since it can directly determine the horizontal components of the vector of motion which most closely approximates the natural one. This obviates the need to project the resulting motion vector components to the surface, since they are already determined directly with respect to it. Additionally, analysis of surface curves versus baselines or chord lengths overcomes the ill-conditioned case regarding motion between pairs of stations which are nearly antipodal (i.e., opposite sides of the world). Since the Earth's shape departs very little from that of an ellipsoid, the interstation chord or baseline between antipodal stations will contain only minimal information about the horizontal motion of the stations since it is essentially orthogonal to the local horizontal at each station. In these antipodal cases, baseline or chord rates, having typically a low signal-to-noise ratio, reduce the likelihood that one can derive any meaningful results regarding horizontal motion.

The disadvantage of using geodesic lines lies in the fact that unlike the spatial chords, geodesics are not independent of the reference frame realized by the estimated station positions. This stems from the fact that the reference surface, the ellipsoid, is attached to the coordinate axes of the reference frame centered at its origin. Any misalignment of the axes between solutions or any translations of the origin will directly affect the computed geodesic lengths and thereby their rate of variation. This in turn will propagate into the station position motion and result in biased estimates for them.

Without loss of generality, one can examine the special case of two stations lying on the same meridian. The situation is illustrated in Figure 6.2 for the case of an origin shift along the Z axis, and for that of a rotation  $\Delta \psi$  about either the X or Y axis. As can be seen from these figures, the geodesic is less sensitive to rotations about X and Y (no changes for rotations about Z) but very sensitive to Z-axis translations. One can show that the sensitivity contrast between translations and rotations reaches a maximum when the ellipsoid degenerates to a sphere. At that point the geodesics degenerate into great circles and their length is, of course, independent of the orientation of the coordinate axes. For the spherical case, a change in a spherical

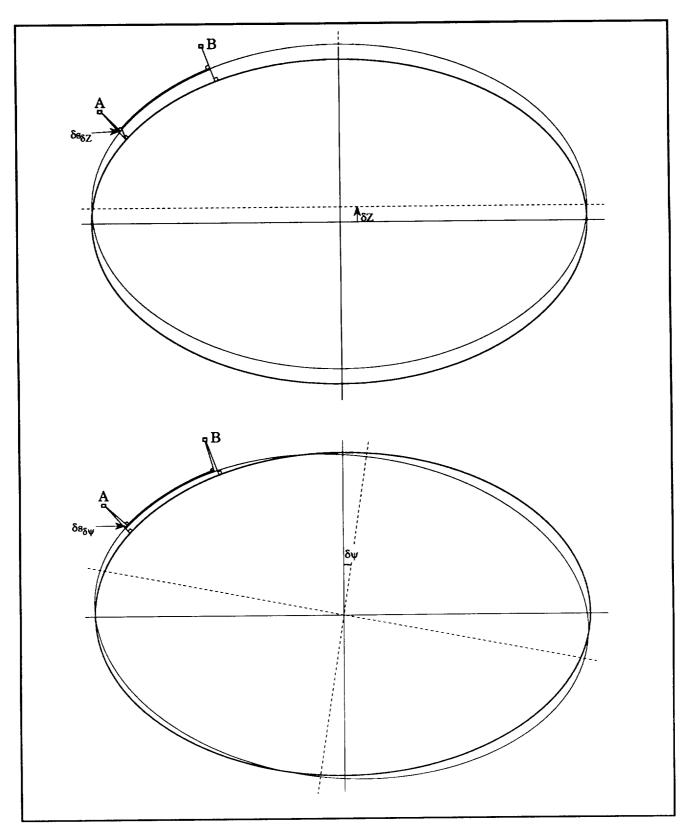


Figure 6.2 Changes in geodesic distances due to differential shift along the Z axis (top) and due to rotation about an axis lying in the equatorial plane (bottom). Points A and B represent tracking station locations which are projected to the ellipsoid for the purposes of computing geodesic distances. In both figures, the flattening of the ellipsoid is highly exaggerated compared to that of the real Earth.

distance ( $\delta s$ ) between points projected onto the sphere at A and B due to a differential shift along the Z axis ( $\delta z$ ) is given by

$$\delta s = -r_e \left( \frac{1}{\sqrt{1 - u^2}} \right) \frac{du}{dz} \, \delta z \tag{6.1}$$

where

$$u = \sin \varphi_a \sin \varphi_b + \cos \varphi_a \cos \varphi_b \cos \Delta \lambda$$

$$\frac{du}{dz} = \sin \varphi_b \cos \varphi_a \frac{d\varphi_a}{dz} + \sin \varphi_a \cos \varphi_b \frac{d\varphi_b}{dz} - \cos \Delta \lambda \left\{ \cos \varphi_b \sin \varphi_a \frac{d\varphi_a}{dz} + \cos \varphi_a \sin \varphi_b \frac{d\varphi_b}{dz} \right\}$$

$$\frac{d\varphi_i}{dz} = \frac{\sqrt{x_i^2 + y_i^2}}{r_i^2}$$

For the meridonal case as illustrated in Figure 6.2, the spherical approximation, formulated above, yields a family of curves describing the behavior of equation (6.1) which are illustrated in Figure 6.3. Shifts along the Z axis can cause variations of the spherical distance to have a ratio with respect to the Z shift as large as 2:1. The ellipsoidal case is not much different since the flattening of the ellipsoid departs from a sphere only by a small amount ( $\sim 0.3\%$ ).

# 6.2 Controlling the Stability of the Reference Frame

The results of the above analysis indicate that specific geodesics can attain magnification factors from Z axis translations as high as two. This means that to obtain geodesic rates free of any such biases and still claim accuracies of some millimeters per year, the reference frame must demonstrate comparable stability. This stability is a function of four major factors:

- the geometric strength of the network of observing stations,
- the variability of the station configuration between solutions,
- the time interval over which the stations define the reference frame, and,
- the orbital dynamics of the satellite(s) being tracked.

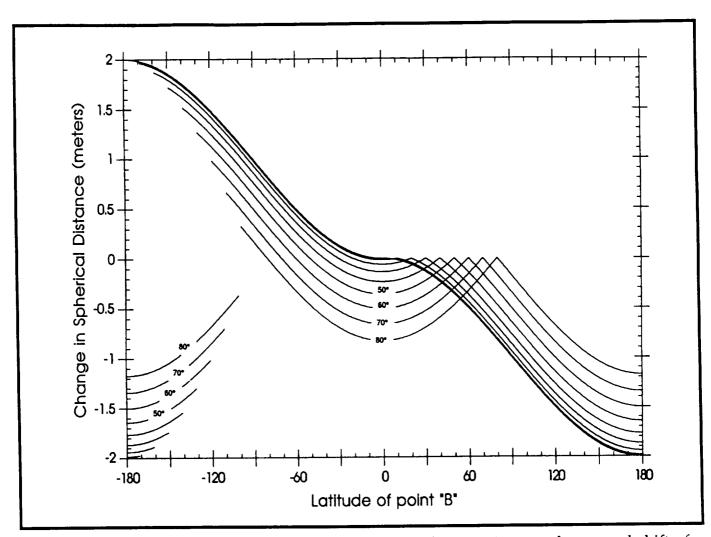


Figure 6.3 Behavior of meridonal spherical distances due to a 1-meter downward shift of the origin along the Z axis. Each curve represents the behavior of the spherical distance from point "A" to point "B". The latitude of point "A" is listed on each curve in  $10^{\circ}$  increments. The latitude of "B" goes beyond  $\pm 90^{\circ}$  when "B" is in the opposite hemisphere. The curves are discontinuous at the antipodal point at which a singularity exists. Along meridonal sections, the largest spherical distance change occurs when points "A" and "B" lie near the Equator and can approach as much as twice the amount of the Z shift.

There is not much that can be done with respect to the first point, since in the case of SL7.1 the network is given de facto. As for the last point, the orbital evolution studies (Section 5.3) have not indicated any significant stability problems. LAGEOS constrains the origin of the coordinate system to an effective center of the Earth's attracting mass with great stability. Due to the extremely accurate force modeling possible for LAGEOS, the origin should be, to a very high degree of approximation, equivalent to the center of mass of the Earth.

The stability of the network configuration turns out to be very important because the tracking problems of particular stations and the effect of residual unmodeled forces on the orbit propagate through the highly accurate ranging data into the recovered station positions, Earth orientation, etc., in considerably different ways from one solution to the next. The solution time interval is very closely related to the network stability. The longer the interval which the solution spans, the more stable the frame it realizes. This is not only because of the increase in the collected observations, but also because of the natural averaging in the tracking configurations encountered. As the interval is lengthened, the impact of station drop-outs or new stations joining the network is minimized. It is extremely difficult to control this last factor since in most cases, drop-outs are to be blamed on unpredictable station malfunctions or prevailing climate conditions that are beyond our control. Nevertheless, one needs to develop a measure that reflects these changes in the network so that one can appropriately correct for them.

#### 6.2.1 Network Geometric Stability

One way to quantify the two factors mentioned above is to monitor the changes in the geometric center of the tracking stations ensemble. We have done this for the case of the shortest span over which a set of data has been reduced (one month nominally) and for the station distribution over the triplets of the monthly subsets which define our basic solutions, the quarterlies, as presented herein.

We define the geometric center of the network as the point whose Cartesian coordinates are the average of those of the stations in the network:

$$\overline{X} = \frac{1}{N} \sum_{i=1}^{N} X_i \qquad \overline{Y} = \frac{1}{N} \sum_{i=1}^{N} Y_i \qquad \overline{Z} = \frac{1}{N} \sum_{i=1}^{N} Z_i \qquad (6.2)$$

where N is the number of stations in the network. If the station configuration were to remain the same over the entire period of time, then the evaluation of the above would show no variations. On the other hand, the actual values would indicate how symmetrical the current station distribution is or, for that matter, how biased it is with respect to any one particular region. The results in Cartesian and spherical coordinates are shown in Figures 6.4 and 6.5.

The initial observation is that the geometric center of the network is located in the Northern Hemisphere as depicted in the graphs of the variation in Z (bottom of Figure 6.4) or in latitude

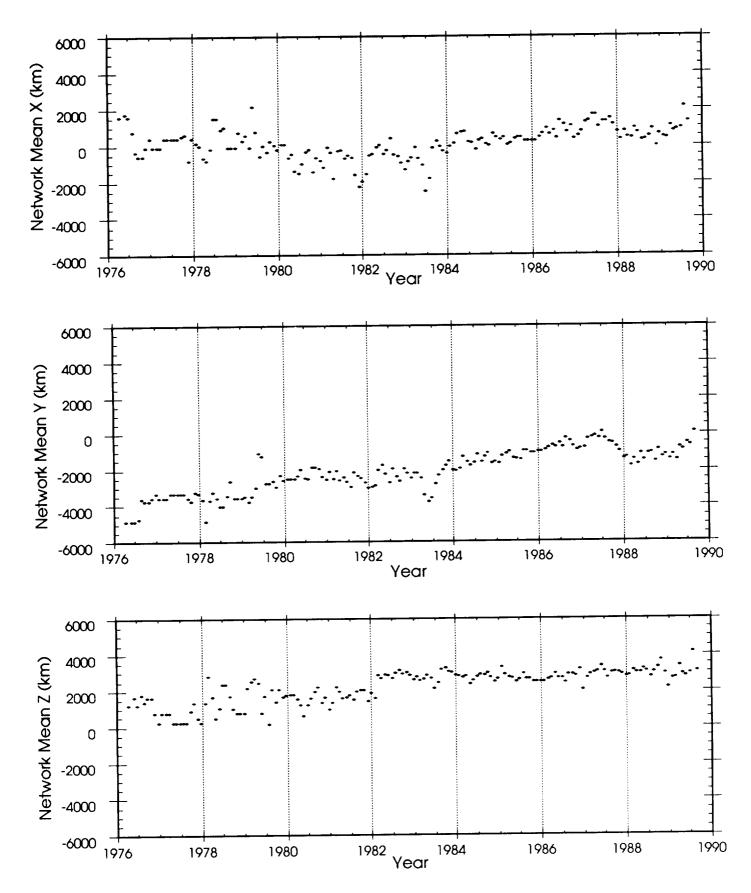


Figure 6.4 Monthly variations of the mean geometric center for the SLR network in terms of Cartesian coordinates.

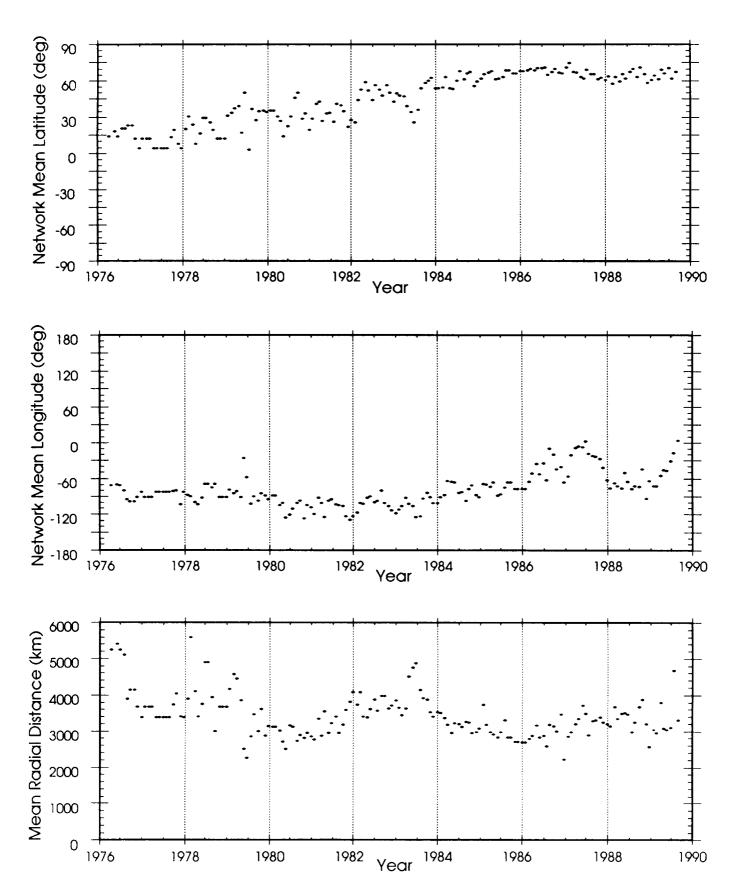


Figure 6.5 Monthly variations of the mean geometric center for the SLR network in terms of spherical coordinates.

(top of Figure 6.5). Secondly, the longitude of the mean geometric center is consistently close to 270 degrees indicating the strong influence of the stations located in the continental U.S. (middle graph of Figure 6.5). In terms of variations, one should note that the network center undergoes significant changes from one month to the next and, due to averaging, one can anticipate the variation across quarterly solutions to be smaller than that of the monthly ones.

The results of this analysis indicate that even with the extended solution period of 3 months, the network will continue to exhibit instabilities which may hinder the solution in achieving the accuracies required for answering geodynamically relevant questions. What therefore needs to be done is to devise a technique that would allow an increase in the resolution of the results without forcing a trade-off in their accuracy.

### 6.2.2 The Global Solution as a Reference Standard

If the length of the interval of analysis plays an important role in determining the stability of the reference frame, then the global solution should provide the most stable frame that can be established. As previously described, one of the main concerns in this "global" definition is the fact that the station motions are modeled through the adopted tectonic model rather than being estimated from the data. This, however, should not matter too much since the majority of the stations follow very closely the modeled motion anyway. What has been done, is to refer the estimated station positions from each quarter we analyzed to the frame realized by the globally estimated positions. To accomplish this, similarity (or rigid-body) transformation parameters (scale excluded) between each quarterly solution and the corresponding global positions from the global solution are determined. In order to avoid biases in the recovered transformation parameters, a time correction is made to bring the global positions from their reference epoch (January 1983) to the mid-epoch of each quarter. The geometry of the transformation is shown in Figure 6.6. Mathematically, the transformation can be written as

$$\begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_{Global} = \begin{bmatrix} \Delta X \\ \Delta Y \\ \Delta Z \end{bmatrix} + \begin{bmatrix} 0 & \omega & -\psi \\ -\omega & 0 & \varepsilon \\ \psi & -\varepsilon & 0 \end{bmatrix} \begin{bmatrix} X \\ Y \\ Z \end{bmatrix}_{Quarterly}$$
(6.3)

where the translational and rotational quantities are as shown in Figure 6.6. These parameters are estimated via a weighted least-squares inversion scheme. The results of this procedure are

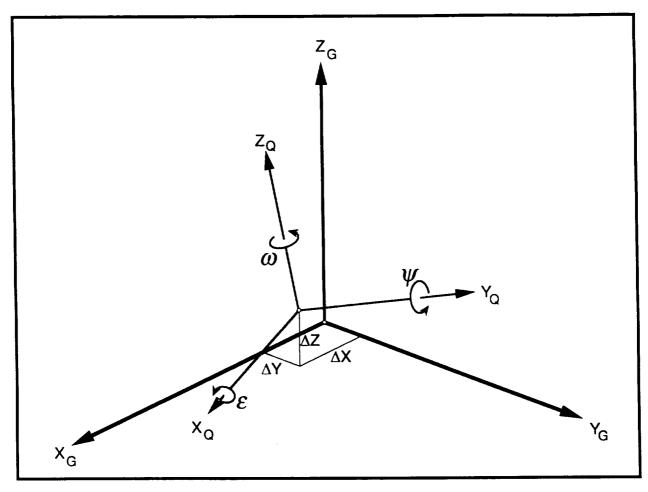


Figure 6.6 Similarity or rigid-body transformations. Nomenclature and geometry used to unify the quarterly realized reference frames into a more consistent "global" frame. The subscripts G and Q refer to the reference frames defined by the "Global" and "Quarterly" solutions, respectively.

summarized in Table 6.1 and are graphically displayed in Figure 6.7 for the translations and in Figure 6.8 for the rotations.

The poor station distribution in the tracking network prior to 1980 is quite evident in the magnitude as well as the quality of the estimates for those early years. In terms of translations, it seems that the Z-axis shift is the one which is consistently more significant than the other two. Yet, its root-mean-square variation for the quarters after 1980 is only 5.5 centimeters. The rotations are of even less significance, with rms variations of about one milliarcsecond in any one of them. What is more of interest here is the fact that the rotation about the Z-axis is very correlated with that about the X-axis, which in turn, is negatively correlated (strongly) with the rotation about the Y-axis. These estimates are based on the weighted estimates of the

Table 6.1 Transformation Parameters used to Place Station Coordinates into Uniform Reference Frame

Year	No.	ΔΧ σ	ΔΥ σ	ΔΖ σ	Scale o	Rot X σ	Rot Y σ	Rot Z σ
	Sta.	(mm)	(mm)	(mm)	(ppb)	(mas)	(mas)	(mas)
1978.25	7	123 120	26 98	-514 118	27 13.6	12 4.4	3 1.4	5 3.8
1978.50		157 66	105 62	212 73	11 8.8	-6 2.3	-1 0.8	7 2.2
1978.75	7	132 68	<i>7</i> 2 <i>7</i> 1	152 82	7 7.7	-4 2.8	-1 0.8	6 2.6
1979	14	-93 51	25 48	<b>-458 57</b>	5 6.4	10 1.8	1 0.7	-2 1.8
1979.25	15	-34 58	- <b>4</b> 1 52	-180 59	-4 7.2	5 2.0	0 0.7	0 1.9
1979.50		-38 62	21 56	351 67	-2 8.1	-8 2.1	-3 0.8	0 2.1
1979.75		48 30	-16 29	61 34	-3 3.8	0 1.0	0 0.4	2 1.1
1980	15	53 17	22 16	55 21	0 1.8	-1 0.5	0 0.3	2 0.7
1980.25	14	-18 16	17 13	22 21	1 1.8	0 0.5	-1 0.2	0 0.6
1980.50		16 10	8 10	29 13	5 1.1	0 0.4	0 0.2	0 0.5
1980.75		-16 13	51 12	53 14	2 1.3	-2 0.4	0 0.3	0 0.6
1981	15	17 19	-13 20	-67 24	3 2.1	2 0.7	-1 0.5	2 1.0
1981.25	15	18 37	0 31	-71 38	-2 3.2	2 1.2	-1 0.9	2 1.6
1981.50		-16 12	22 12	63 15	-4 1.4	-2 0.4	0 0.3	-1 0.6
1981.75		34 22	-19 20	80 27	-1 2.2	-1 0.7	2 0.6	0 1.1
1982	15	19 22	-10 24	69 32	-3 2.5	-1 0.9	1 0.6	0 1.3
1982.25		18 17	-6 18	66 21	-2 2.3	-1 0. <del>6</del>	1 0.4	0 0.8
1982.50		15 16	2 16	144 18	-9 2.0	<b>-4</b> 0.5	3 0.4	-2 0.7
1982.75		-5 15	40 15	45 18	-5 1.9	-2 0.5	0 0.4	0 0.7
1983	16	-12 21	70 19	<i>-7</i> 3 23	-1 2.4	0 0.7	-1 0.5	1 0.8
1983.25	17	-15 20	5 19	34 20	0 2.5	-1 0.6	0 0.5	-1 0.8
1983.50		-16 12	-10 15	<i>7</i> 3 12	0 1.9	-2 0.4	1 0.3	-2 0.4
1983.75		-36 10	10 10	62 11	0 1.3	-2 0.3	0 0.2	-2 0.4
1984	23	-11 10	-42 10	10 12	1 1.3	0 0.4	0 0.2	0 0.5
1984.25	23	-6 5	-2 6	-18 6	1 0.7	0 0.2	0 0.1	0 0.2
1984.50	21	14 6	13 7	-11 7	1 0.8	0 0.2	0 0.1	0 0.2
1984.75	23	98	5 8	53 9	0 0.9	-1 0.3	1 0.1	0 0.3
1985	18	1 7	7 7	-3 8	0 0.8	0 0.3	0 0.1	0 0.3
1985.25		-3 6	-1 6	-34 7	0 0.8	1 0.2	0 0.1	0 0.2
1985.50		-1 8	-2 8	60 9	-1 1.0	-1 0.3	1 0.2	-1 0.3
1985.75		-1 6	-1 6	46 7	-1 0.8	-1 0.2	0 0.1	0 0.2
1986	19	14 6	-7 6	-50 7	0 0.7	1 0.2	0 0.1	1 0.2
1986.25	21	-5 <b>7</b>	-8 7	-67 8	0 0.9	2 0.3	-1 0.1	1 0.3
1986.50	22	-1 4	15 4	- <b>4</b> 0 <b>4</b>	0 0.5	0 0.1	0 0.1	0 0.1
1986.75		-6 5	6 5	-29 5	2 0.6	0 0.2	0 0.1	0 0.2
1987	20	-19 7	-15 7	53 9	0 0.9	-1 0.2	0 0.2	-1 0.3
1987.25		-4 4	-5 5	-37 6	0 0.7	1 0.2	0 0.1	0 0.2
1987.50		8 7	-3 7	-97 8	2 1.0	3 0.2	-1 0.1	2 0.3
1987.75		-3 6	12 7	-99 8	1 0.9	2 0.2	-2 0.1	2 0.2
1988	20	10 17	13 15	-6 18	3 1.9	0 0.6	0 0.3	0 0.7
1988.25		4 13	-21 14	29 16	-2 1.8	0 0.5	0 0.3	0 0.6
1988.50	22	-4 12	-23 14	13 16	-1 1.7	0 0.5	0 0.3	0 0.6
1988.75	20	-10 23	22 27	112 30	-4 3.4	-3 0.9	1 0.6	-2 1.1

positions, so that the strongly determined stations dominate the solution, while the effect of the poorly determined ones is insignificant. The peculiarities of the recovered transformation parameters are therefore the result of an unbalanced distribution of quality tracking data rather than anything else. Despite the small magnitude of these individual constituents of the transformation, one should keep in mind that first it is the sum total that affects the solution, and second, in certain cases, as already shown, a geodesic can be affected by as much as twice that amount.

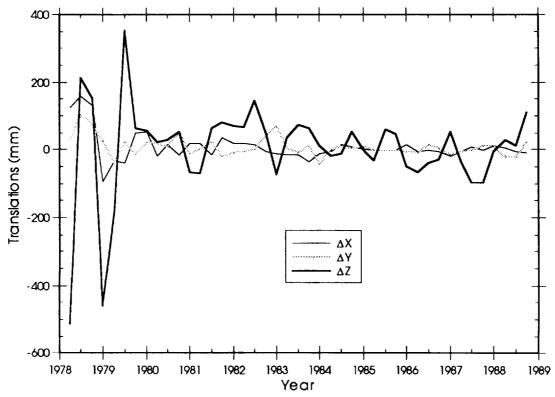


Figure 6.7 Rigid-body Transformations: Translations of the origin.

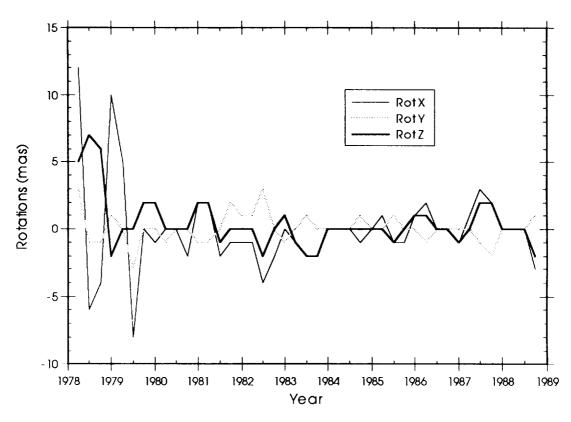


Figure 6.8 Rigid-body Transformations: Rotations about the origin.

The transformation parameters, as listed in Table 6.1, have been applied to all station positions within each quarter to produce a set of quarterly station positions in a globally consistent frame of reference. The resulting station positions used in the network adjustment are listed quarter-by-quarter in Appendix 6.

### 6.3 Geodesic Lines from the Transformed Quarterly Solution

The behavior of the recovered transformation parameters indicates a possible periodicity, perhaps varying with an annual period. The source of this effect may possibly be due to the seasonal nature of weather impediments thereby reducing the amount of tracking. However, such behavior is likely to introduce excessive variation in the behavior of the geodesics for reasons previously described. Our conjecture is that this variation should be grossly eliminated once we have accounted for the instability in the reference frame. Additionally, the reduction in the variation should be more prominent in the case of lines with greater extent, since short lines depart only slightly from their respective chords. This conjecture was tested by means of a comparison of the geodesic line lengths based on the station coordinates before having been transformed and those after applying the transformations. Weighted least squares estimates of best fitting lines were determined to yield the slopes of the observed geodesics between a set of twenty stations. We limited ourselves to this subset of stations, since they are the only ones with a significant number of determinations to recover meaningful estimates. The scatter about each line was the statistic under scrutiny. Histograms of the scatter were made for both sets of geodesics and for various subsets according to criteria based on the number of contributing determinations per line. The results for all cases examined are shown in Figure 6.9, for the lines with more than four determinations in Figure 6.10, and for our extremely robust lines with more than twelve determinations in Figure 6.11.

The obvious conclusion from these histograms is that the imposition of the global reference frame has resulted in a 30 - 40% decrease in the scatter of the line fits. That is to say the geodesic estimates are far more consistent between quarters after transforming the sites to a common origin. The original conjecture proves to be true then, and the increase in resolution is supported through this technique with a parallel increase in the consistency of the estimates.

Another way of examining the effect of the transformation is in the temporal stability of the quality of the line fits. Naturally, one expects that these quantities should follow the curve that describes the improvement in the quality of the ranging data on which they are based. We have computed the root mean square line fit scatter for each quarter in the solution and for the station subset which is nominally analyzed for the determination of the tectonic model implied by our geodesic rates between stations. The results for the pre- and after-transformation geodesic sets are shown in Figure 6.12. Even though the downward trend is expected, due to the improvement in the data, it is not nearly as clear in the case of the line fits determined on the

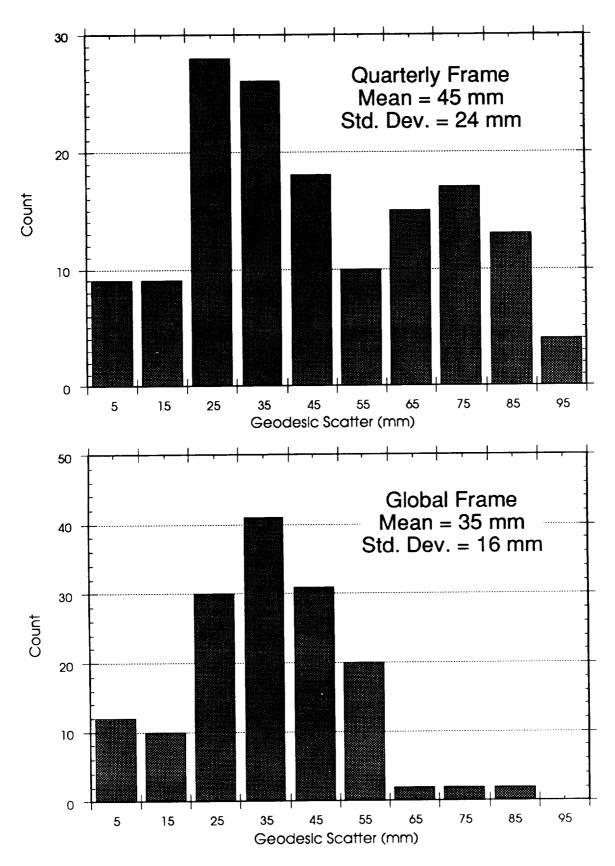


Figure 6.9 Geodesic line fit scatter distribution: Using all observed lines between 20 stations. Quarterly frame at top, global frame at bottom.

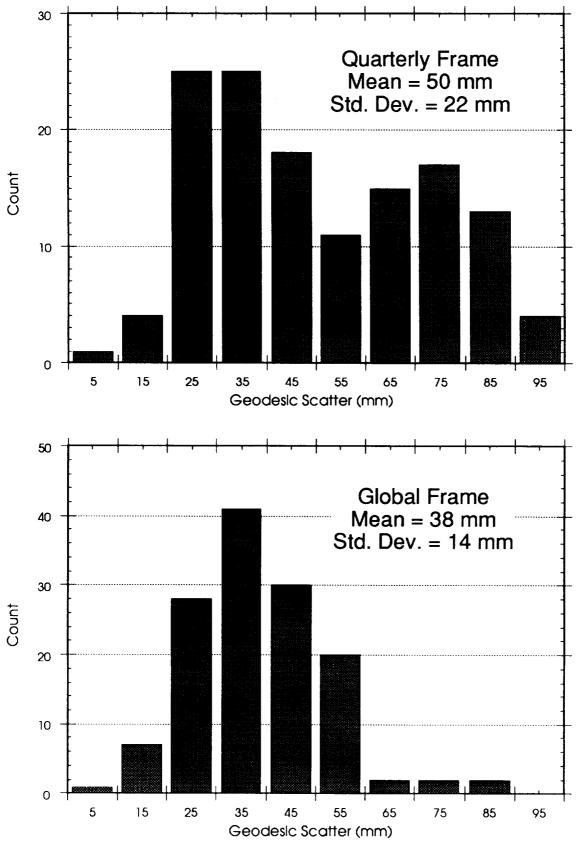


Figure 6.10 Geodesic line fit scatter distribution: Using lines with more than four determinations. Quarterly frame at top, global frame at bottom.

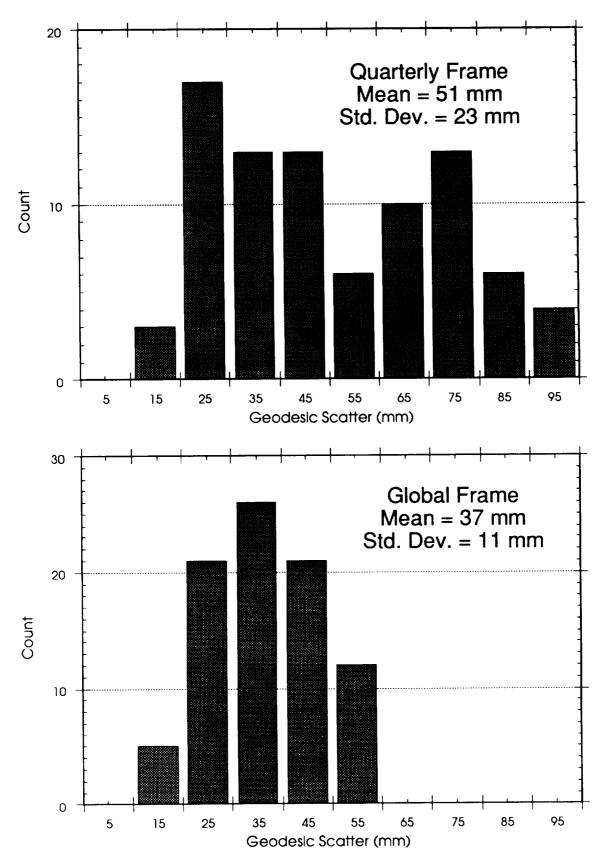


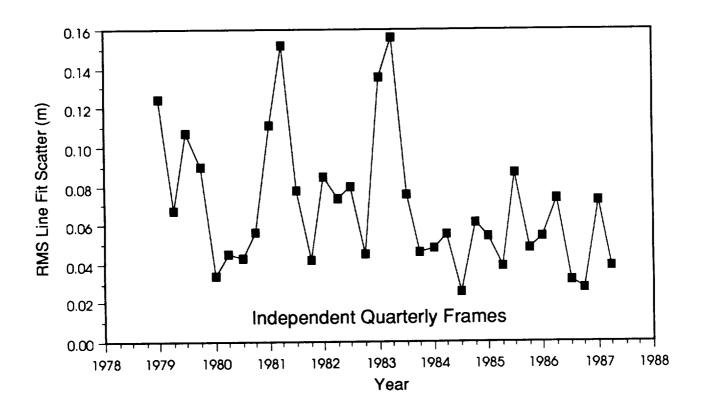
Figure 6.11 Geodesic line fit scatter distribution: Using lines with more than twelve determinations. Quarterly frame at top, global frame at bottom.

basis of quarterly determined stations in an independent frame. Not only does the trend become clearer, the rms of these scatters is now much more consistent for the entire period of time.

Finally, perhaps the best demonstration of the benefits resulting from the reference frame stabilization process is through the line fits themselves. Several examples of lines with typical fits as derived from station positions before and after the application of the transformation are shown in Figures 6.13 - 6.19. As expected, there is little to be gained in the case of short lines (e.g., Monument Peak to Quincy, Figure 6.13), but for long lines, the improved results are remarkable (e.g., Yaragadee to Arequipa (6.18) and Quincy to Matera (6.16)). An added benefit of this procedure is the fact that outliers are easier to detect, as is seen, for example, in the second and third quarter of 1983 determinations of the Quincy-to-Wettzell line (Figure 6.14).

### 6.4 Summary

In conclusion, the technique we have adopted allows for an increase in the temporal resolution of our estimates while still maintaining the same or even improved integrity of the results. It should be stressed here that this is an interim solution of the problem which we had to adopt due to software limitations. The results of the next cycle of analysis will be based on direct estimates of the station motions recovered in the global estimation procedure rather than through post-processing efforts.



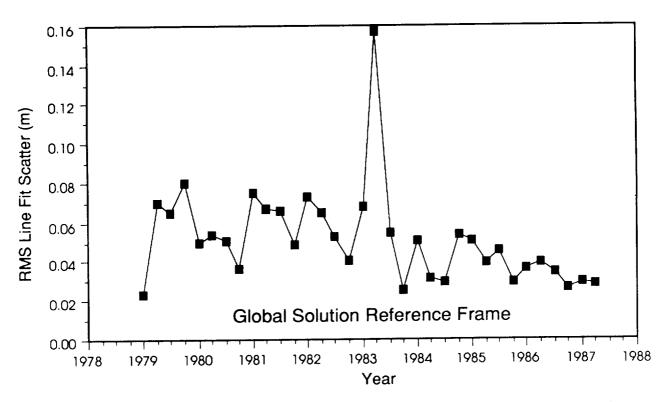


Figure 6.12 RMS line fit scatter by quarter: Before transformation at top, after transformation at bottom.

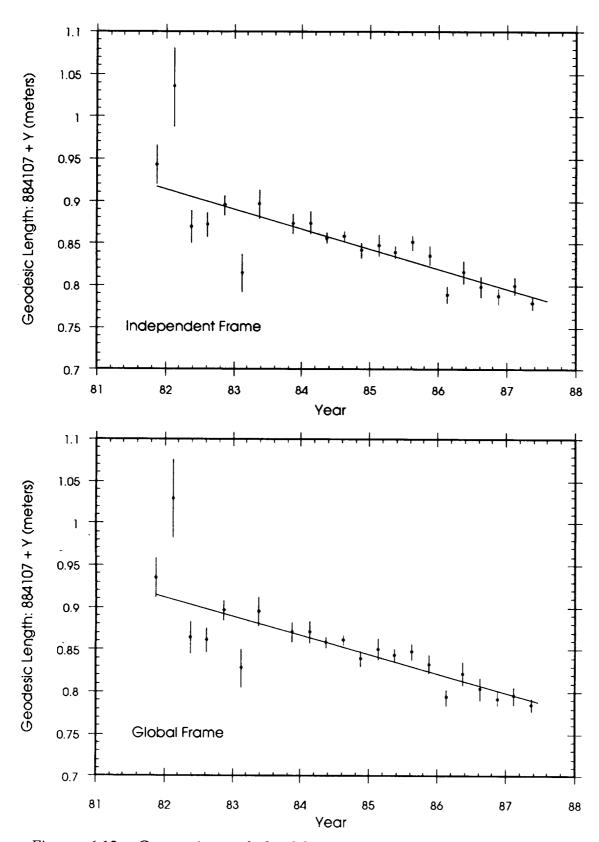


Figure 6.13 Comparison of the Monument Peak to Quincy geodesic line histories: Top - before transformation (independently determined reference frames) and bottom - after transformation (globally unified reference frame). This study was based on an earlier SL7 solution and therefore does not represent final station motion behavior.

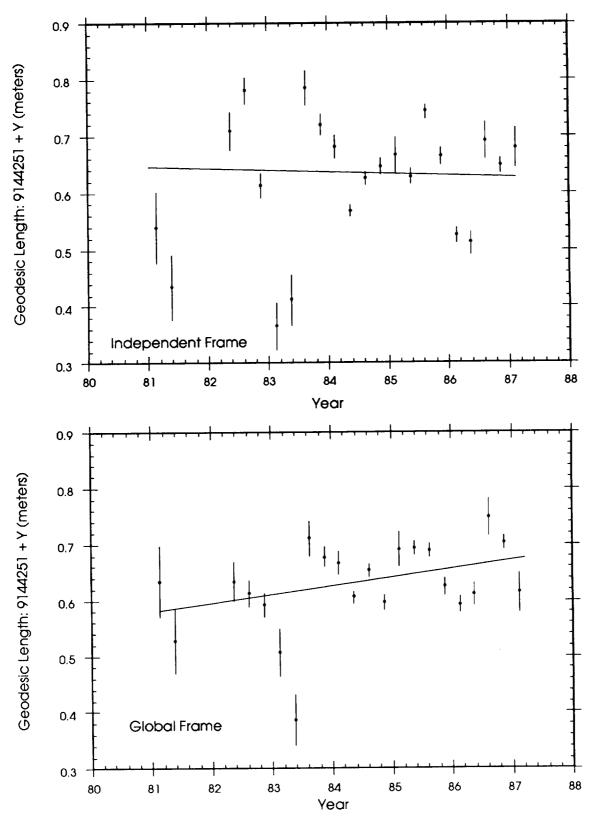


Figure 6.14 Comparison of the Quincy to Wettzell geodesic line histories: Top-before transformation (independently determined reference frames) and bottom-after transformation (globally unified reference frame). This study was based on an earlier SL7 solution and therefore does not represent final station motion behavior.

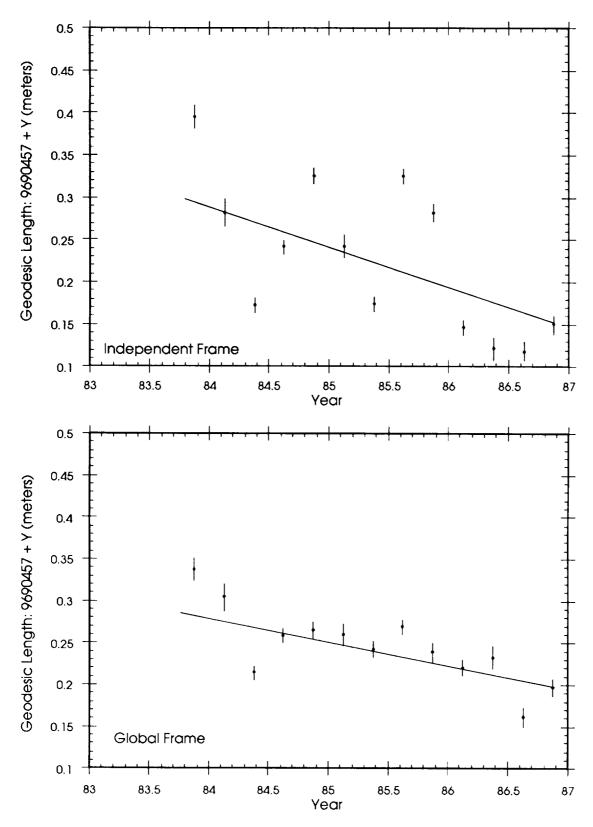


Figure 6.15 Comparison of the Simosato to RGO geodesic line histories: Top-before transformation (independently determined reference frames) and bottom-after transformation (globally unified reference frame). This study was based on an earlier SL7 solution and therefore does not represent final station motion behavior.

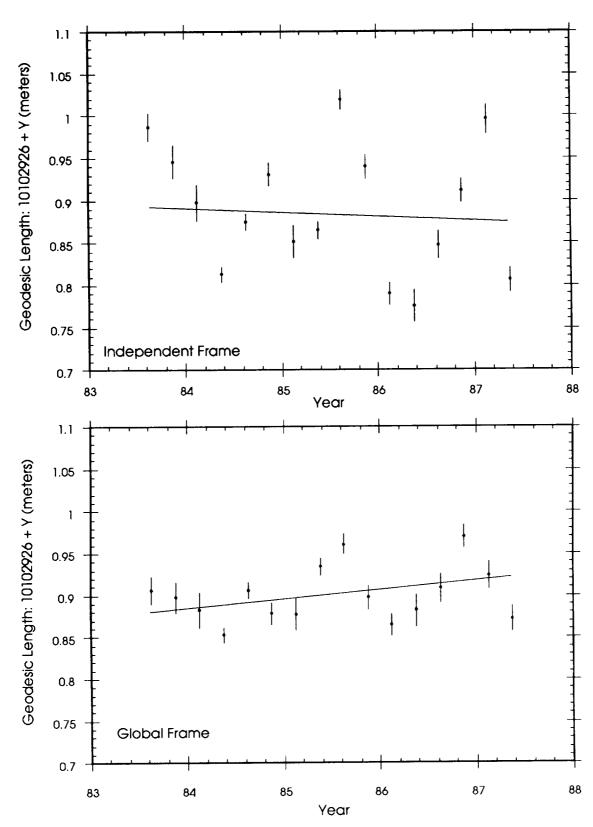


Figure 6.16 Comparison of the Quincy to Matera geodesic line histories: Top-before transformation (independently determined reference frames) and bottom-after transformation (globally unified reference frame). This study was based on an earlier SL7 solution and therefore does not represent final station motion behavior.

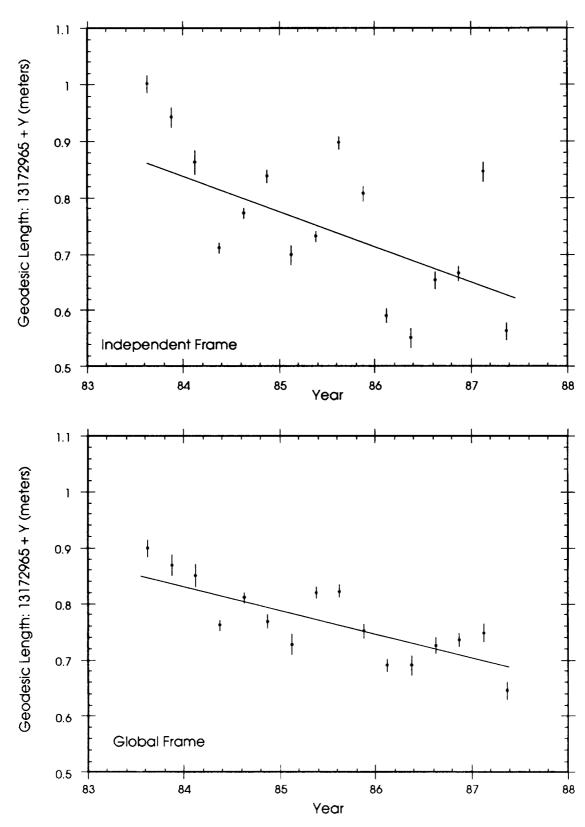


Figure 6.17 Comparison of the Maui to Matera geodesic line histories: Top-before transformation (independently determined reference frames) and bottom-after transformation (globally unified reference frame). This study was based on an earlier SL7 solution and therefore does not represent final station motion behavior.

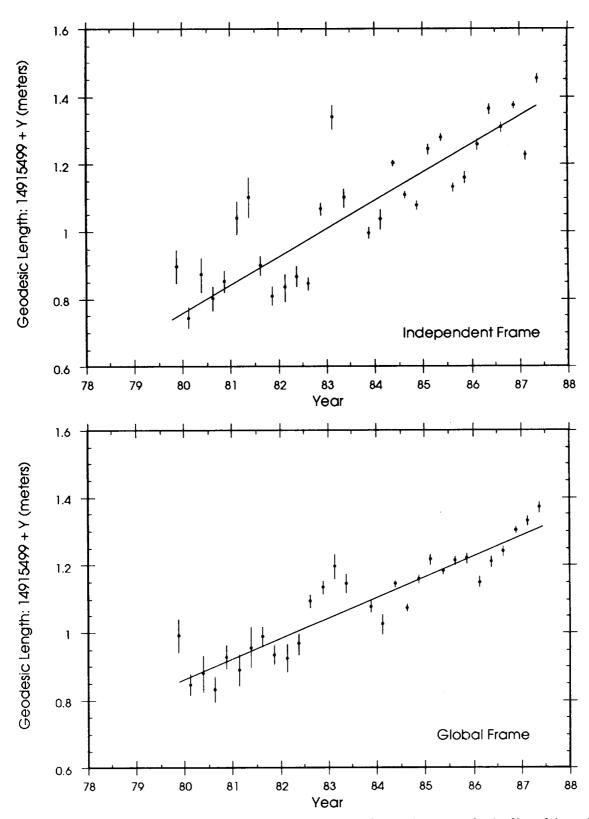


Figure 6.18 Comparison of the Yaragadee to Arequipa geodesic line histories: Top - before transformation (independently determined reference frames) and bottom - after transformation (globally unified reference frame). This study was based on an earlier SL7 solution and therefore does not represent final station motion behavior.

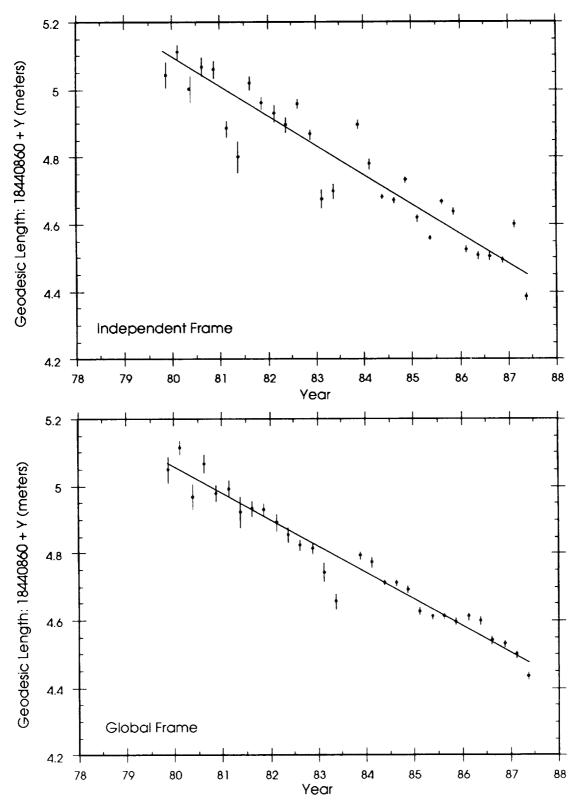


Figure 6.19 Comparison of the Yaragadee to Greenbelt geodesic line histories: Top - before transformation (independently determined reference frames) and bottom - after transformation (globally unified reference frame). This study was based on an earlier SL7 solution and therefore does not represent final station motion behavior.

# 7. Site Motion Estimation via Network Adjustment

# 7.1 Kinematic Reference Frames - Concepts

According to plate tectonic theory, all points on the Earth's surface are located on a continuously moving crust. To more easily understand the global tectonics determined by SLR and to understand regional deficiencies between the SLR results and the geologically based tectonic models (which assume rigid plate behavior), it is desirable to adopt a kinematic reference frame with respect to which we can define the linear horizontal motions of the individual SLR stations. We have elected to use the NUVEL-1 NNR (No Net Rotation) model of Argus and Gordon [1991] in the definition of the kinematic frame. NUVEL-1 NNR is based on the NUVEL-1 relative plate motion model published by DeMets et al. [1990]. This model updates the AM0-2 model of Minster and Jordan [1978], used throughout most of the SLR data reduction process. To determine the kinematic behavior of the SLR sites within this frame, standard network adjustment concepts have been applied. These concepts and the results thereof are described in the remainder of this chapter.

### 7.2 Interstation Geodesic Rates and Network Definitions

The transformed SL7.1 quarterly station coordinates are used in this, the final portion of the analysis. Geodesic distances between all possible tracking sites that have tracked LAGEOS in each quarter are computed via an algorithm derived by *Vincenty* [1975]. The uncertainty for each quarterly geodesic distance is calculated by propagating the formal station position uncertainty. The variation across time of the geodesic distances connecting pairs of stations provides the base information used to determine the north and east velocity components of the SLR sites. Linear changes in geodesic distances are computed using a weighted least-squares estimator. The uncertainty of each quarterly geodesic distance provides the weights used in the estimate of the slope. The algorithm yields a formal estimate of the uncertainty in the determined geodesic rate which is additionally scaled to reflect the fit of the geodesic distances to the linear model (i.e.,  $\chi^2=1$  criteria is assumed yielding an uncertainty of unit weight). These slopes, or geodesic rates, are used as the "observables" to determine the station motions in a least squares network adjustment described in the following section. Although for short interstation distances there is no significant difference between changes in the length of

geodesics and the chord lengths, for long distances, changes in geodesics give a more meaningful description of the relative horizontal motion between stations. The geodesic rates are used to describe the relative changes in the positions of the stations along the ellipsoidal surface which is taken to be approximately equivalent to the Earth's surface. These rates are therefore independent of all station vertical motions and their associated height uncertainties. Thus, horizontal motions within the SLR network are effectively isolated.

Two networks of stations are defined in the adjustment procedure; an "external" network of strong stations which are used for the realization of a kinematic reference system and whose motions are assumed to be known; and an "internal" network of stations whose motions are to be determined. The motions of the internal stations are estimated within a kinematic reference frame defined by the motions of the external sites within the least-squares estimation procedure. Obviously, for satisfactory closure, the adopted motions for the external stations must be consistent relatively with that observed directly by SLR.

The definition of the kinematic reference frame within a geologically compatible context is provided by the NUVEL-1 NNR model. Two SLR sites are selected to define the external network which is constrained to move with NUVEL-1 NNR motions. As was used throughout the data reduction process, the tracking stations at Maui and Greenbelt were selected as the external reference stations. Use of these sites was viable, for the geologically predicted relative motion between these sites is consistent with that deduced by SLR (e.g., the SLR rate estimate between Greenbelt and Maui is  $16 \pm 2$  mm/yr compared to the rate predicted by NUVEL-1 of 14 mm/yr). These two stations were also chosen for additional reasons, mainly having to do with the strength of the quality and quantity of laser data collected at these sites as well as both having been in continuous operation for at least 7 years and that each station is centrally located on a major tectonic plate. The motion constraint adopted in the network adjustment differs from that used in the laser data reduction in that both the north and east components of Maui's motion are constrained.

The tracking sites which make up the internal network are listed in Table 7.1 and shown in map form in Figure 7.1. These sites are distributed globally and represent the strongest stations with the longest tracking histories presently available from CDP SLR tracking campaigns. More importantly, each internal site has a resolvable geodesic rate with respect to almost all other internal and external stations used in the adjustment. A total of 230 geodesics can be constructed between the 22 tracking sites considered here. Of these, 214 actual geodesic rates can actually be calculated based on the available data. Two subsets of the geodesic rates are defined in the

Table 7.1. Internal Station Network

Site No.	Site Name	Plate
7109	Quincy, CA	No. American
7835	Owens Valley, CA	No. American
7086	McDonald Obs., TX	No. American
7122	Mazatlan, Mexico	No. American
7112	Platteville, CO	No. American
7110	Monument Pk, CA	Pacific
7035	Otay Mountain, CA	Pacific
7121	Huahine, French Polynesia	Pacific
7907	Arequipa, Peru	So. American
7097	Easter Island	Nazca
7090	Yaragadee, Australia	Indo-Australian
7843	Orroral, Australia	Indo-Australian
7834	Wettzell, Germany	Eurasian
7835	Grasse, France	Eurasian
7839	Graz, Austria	Eurasian
7810	Zimmerwald, Switzerland	Eurasian
1181	Potsdam, Germany	Eurasian
7840	Royal Greenwich Obs., U. K.	Eurasian
7838	Simosato, Japan	Eurasian or North American
7939	Matera, Italy	African

adjustment procedure. One subset contains the geodesic rates between internal and external sites, and the other subset is made up of rates between the internal sites themselves.

# 7.3 Mathematical Description of the Network Adjustment

The algorithm used to estimate the velocities of the tracking sites is based on similar algorithms used to determine static positions based on distance measurements. In classical terrestrial surveying, the problem falls into the class of trilateration problems. In our application, we essentially solve the problem in the same manner, whereby we have substituted geodesic rates for distances and components of motion for components of location. In

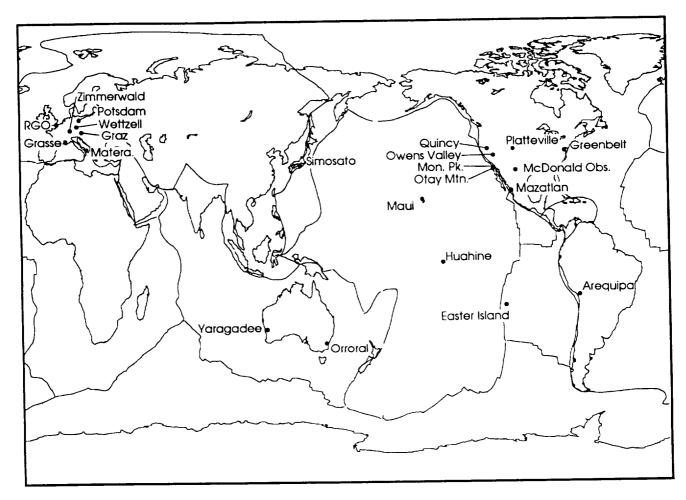


Figure 7.1 Locations of tracking sites contributing to the SL7.1 solution.

trilateration problems, the reference system is typically established by adopting a position of one of the nodes of the network and a direction toward one of the other nodes. In the same manner as described in the previous section, we have adopted the motion of two of the tracking sites. This is actually over-constraining the solution, but as mentioned above, as long as the SLR-determined motion between the constrained sites matches (to at least one standard deviation) that implied by the constraining model, the effects on the overall solution become negligible.

All geodesic rates between internal sites as well as those between internal to external sites are combined in a weighted least-squares solution which ultimately yields the unique motion vectors for each internal tracking site. Two kinds of observation equations can be written. For the external-to-internal lines the equation is written as:

$$C_{ij} = \left| \dot{X}_j \middle| \cos \left( A_{xj} - A_{ji} \right) \right| \tag{7.1}$$

where:

is the "observed" relative motion of the  $j^{th}$  internal site towards the  $i^{th}$  external station after the modeled motion of the external station has been removed, i.e.,  $C_{ij} = \dot{r}_{ij} - \dot{X}_i \cdot e_{ij}$  where  $\dot{r}_{ij}$  is "observed" relative motion between external site i and internal site j,  $\dot{X}_i$  is the constrained motion of the external site i, and  $e_{ij}$  is the unit vector at i toward j.

 $A_{xj}$  is the azimuth of the unknown motion vector  $\dot{X}_j$ .

 $A_{ii}$  is the azimuth from the internal site toward the external site.

These quantities are illustrated in Figure 7.2. The internal-to-internal lines have a somewhat similar observation equation of the form:

$$\dot{r}_{jk} = \left| \dot{X}_j \middle| \cos \left( A_{xj} - A_{jk} \right) + \middle| \dot{X}_k \middle| \cos \left( A_{xk} - A_{kj} \right) \right|$$
 (7.2)

where:

 $\dot{r}_{jk}$  is the observed relative geodesic rate between internal sites j and k  $\dot{X}_j$ ,  $\dot{X}_k$  are the motion vectors being solved for at internal sites j and k are the azimuths of  $X_j$  and  $X_k$ , respectively, and  $A_{jk}$ ,  $A_{kj}$  are the azimuths of station j to k and k to j, respectively.

These terms are also illustrated in Figure 7.2.

### 7.4 Results from the Network Adjustment

The network adjustment is performed for 20 internal sites whereby estimates of their horizontal motions are relative to the constrained motions of the two external sites. In total, 214 geodesic distance rates (out of a possible 230) were used to determine the internal site velocities. The input geodesic rates between all pairs of stations are tabulated in Table 7.2 as well as those

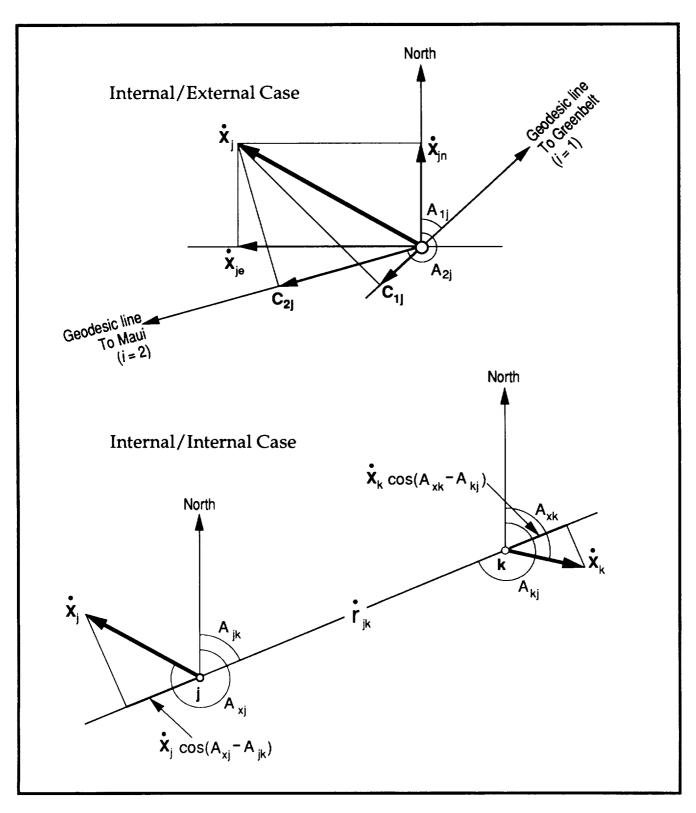


Figure 7.2 Network adjustment nomenclature used in equations (7.1) and (7.2). Top diagram illustrates the case between internal site j and the two external sites at Maui and Greenbelt. The bottom diagram illustrates the case between two internal sites, j and k.

inferred by the SL7.1 solved-for site velocities. Also shown on this table for reference, are the geodesic rates inferred by the geologic models NUVEL-1 and AM0-2.

The network adjustment provides estimates for the motions of the tracking sites as shown in Table 7.3. Actually, the estimated quantities are the site's northward and eastward velocity components, although in Table 7.3 we have elected to only show the direction and rate of the motions. Estimates of their errors in each component are also computed in the inversion and the error ellipse parameters are also given in the table. The overall weighted RMS of fit (or  $\chi$  -squared statistic) for the complete solution is

$$WRMS = \left\{ \frac{\sum \left[ \left( \dot{r}_{observed} - \dot{r}_{model} \right) / \sigma_{obs} \right]^{2}}{214} \right\}^{1/2} = 0.85$$
 (7.3)

which indicates that the uncertainties quoted from the solution are optimistic (i.e., too large) and that good network closure has been achieved.

Geophysical interpretation of these results was the main focus of a companion paper of the present volume. The reader is advised to consult *Smith et al.* [1990b] for a comprehensive discussion of the tectonic results as well as regional anomalies and their implications with respect to current geophysical theories. Another recent global analysis of SLR-derived motions has been published by *Biancale et al.* [1991].

Table 7.2. Geodesic Rates Between SLR Sites

Table 7.2. Geodesic Rates Between SLR Sites  Observed NAP NUVEL 1 AM0-2									
Emama			Rate		Rate	Rate			
From	To	Rate -7	<u>σ</u> 2	-6	<u>σ</u>	-4	-6		
Arequipa	Greenbelt					_			
Arequipa	Maui	75 (2	3	72 (2	2	61	66		
Arequipa	Easter Island	-62	7	-63	3	-80	-89		
Arequipa	Grasse	8	7	3	3	20	22		
Arequipa	Graz	5	6	4	3	20	21		
Arequipa	Huahine	94	9	98	5	70	74		
Arequipa	Matera	6	5	3	2	21	24		
Arequipa	Mazatlan	3	5	4	2	-9	-12		
Arequipa	McDonald	-2	3	-0	2	-8	-11		
Arequipa	Monument Peak	36	3	36	2	38	42		
Arequipa	Orroral	45	3	41	3	35	27		
Arequipa	Otay Mountain	43	6	35	2	38	43		
Arequipa	Owens Valley	-6	7	8	3	-8	-11		
Arequipa	Platteville	0	9	-8	5	-7	-10		
Arequipa	Potsdam	14	11	11	5	18	19		
Arequipa	Quincy	7	3	7	2	-8	-11		
Arequipa	RGO	5	5	4	3	1 <i>7</i>	19		
Arequipa	Simosato	7	6	6	2	-20	-25		
Arequipa	Wettzell	7	4	3	2	19	20		
Arequipa	Yaragadee	59	4	62	2	64	62		
Arequipa	Zimmerwald	0	16	5	6	19	21		
Easter Island	Greenbelt	-21	7	-29	2	-33	-37		
Easter Island	Maui	133	6	135	3	136	148		
Easter Island	Grasse	-33	11	-42	3	-41	-46		
Easter Island	Graz	-36	5	-37	2	-37	-43		
Easter Island	Huahine	194	16	166	6	157	1 <b>7</b> 0		
Easter Island	Matera	-48	1	-47	1	-47	-51		
Easter Island	Mazatlan	-7	6	4	3	-5	-7		
Easter Island	McDonald	7	16	-8	3	-8	-9		
Easter Island	Monument Peak	42	6	39	3	48	54		
Easter Island	Orroral	t	†	65	3	72	72		
Easter Island	Otay Mountain	+	t	41	3	49	55		
Easter Island	Owens Valley	†	†	20	4	10	9		
Easter Island	Platteville	-7	54	- <b>4</b>	5	-5	-7		
Easter Island	Potsdam	-23	11	-22	5	-32	-37		
Easter Island	Quincy	18	4	21	3	12	12		
Easter Island	RGO	-28	9	-33	2	-34	-39		
Easter Island	Simosato	78	8	81	3	57	60		
Easter Island	Wettzell	-30	11	-35	2	-35	-40		
Easter Island	Yaragadee	48	4	59	2	67	67		
Easter Island	Zimmerwald	+	+	-35	5	-38	-43		
Grasse	Greenbelt	15	9	18	3	23	23		
Grasse	Maui	-25	11	-28	4	-27	-31		
Grasse	Graz	7	7	2	4	0	0		
Grasse	Huahine	-1 <b>1</b>	25	15	4	6	3		
Grasse	Matera	-11	23 4	-2	3	-6	- <b>4</b>		
	Mazatlan	-2 17	8	16	3	22	22		
Grasse	McDonald	14	15	24	3	22	22		
Grasse			15 9		3	11	8		
Grasse	Monument Peak	15		16					
Grasse	Orroral	-18	29	-22	3	-31	-26		

Table 7.2 (continued). Geodesic Rates Between SLR Sites

		NUVEL 1 Rate	
		Rata	
Grasse Otay Mountain † † 13			Rate
	3	11	8
Grasse Owens Valley † † 18	4	21	20
Grasse Platteville -20 * 16	4	22	21
Grasse Potsdam 1 29 4	. 7	0	0
Grasse Quincy 18 8 17	3	20	20
Grasse RGO 2 7 2	3	0	0
Grasse Simosato -18 6 -19	3	0	0
Grasse Wettzell 0 6 2		0	0
Grasse Yaragadee -15 7 -14		-21	-16
Grasse Zimmerwald 5 15 -3		0	0
Graz Greenbelt 16 5 17		22	21
Graz Maui -41 6 -40		-37	-43
Graz Huahine -14 12 -9		-16	-20
O'LD		-8	-7
Giuz		21	21
Oluz Wilminin		21	21
0142		4	0
GIUZ TITOLINIA COM		-38	-32
Oluz Ollorus		-36 4	0
GIAZ Cary Mountain 10 0		20	19
Oluz Ottorio varioj		20	20
Graz Platteville 19 12 15		0	0
Graz Potsdam -12 19 -6			18
Graz Quincy 13 4 14		19	
Graz RGO 0 5 -(		0	0 0
Graz Simosato -20 7 -21		0 0	0
Graz Wettzell -1 5			-23
Graz Yaragadee -23 7 -21			
Graz Zimmerwald -11 11 -2		0	0
Greenbelt Maui 16 2		14	16
Huahine Greenbelt 36 8 29			14
	3 5	0	0
Huahine Matera -10 10 -3			-19
Huahine Mazatlan 37 9 3			14
Huahine McDonald 15 9 15			6
	5 3		0
Huahine Orroral -64 21 -77			-64
Traumine out of the second	8 3		0
Huahine Owens Valley † † -			-18
Huahine Platteville -8 27 10			-7
Huahine Potsdam -14 27 -			-23
Huahine Quincy 0 9 -			-24
Huahine RGO 12 11 10			-1
Huahine Simosato -88 11 -79			-107
Huahine Wettzell -10 12 -			-18
Huahine Yaragadee -64 8 -7			-69
Huahine Zimmerwald -12 36 1			-4
Matera Greenbelt 15 4 1			18
Matera Maui -42 7 -4			-49
Matera Mazatlan 12 5 1			17
Matera McDonald 18 8 2	1 2	. 14	16

Table 7.2 (continued). Geodesic Rates Between SLR Sites

Table 7.2 (continued). Geodesic Rates Between SLR Sites								
		Observed			NAP		NUVEL 1	AM0-2
From	То	Rate	σ		Rate	σ	Rate	Rate
Matera	Monument Peak	10	5		11	2	-0	-2
Matera	Orroral	-11	17		-15	3	-21	-18
Matera	Otay Mountain	13	2		8	1	-0	-2
Matera	Owens Valley	†	t		14	3	12	13
Matera	Platteville	24	15		14	4	13	15
Matera	Potsdam	-8	20		-6	6	-8	-7
Matera	Quincy	11	5		13	2	11	13
Matera	RGO	-2	4		-2	2	-8	-6
Matera	Simosato	-24	5		-20	3	-3	-3
Matera	Wettzell	-4	3		-0	2	-9	-7
Matera	Yaragadee	-13	6		-10	2	-14	-11
Matera	Zimmerwald	-0	14		-7	4	-8	-6
Mazatlan	Greenbelt	-0	3		-1	2	0	0
Mazatlan	Maui	40	4		39	2	43	48
Mazatlan	McDonald	-7	6		-9	2	0	0
Mazatlan	Monument Peak	35	3		32	2	47	55
Mazatlan	Orroral	-24	11		-43	2	-42	-45
Mazatlan	Otay Mountain	27	3		31	2	47	55
Mazatlan	Owens Valley	+	+		4	3	0	0
Mazatlan	Platteville	-15	12		-7	5	0	0
Mazatlan	Potsdam	22	16		22	5	21	20
Mazatlan	Quincy	4	4		3	2	0	0
Mazatlan	RGO	15	4		14	2	22	22
Mazatlan	Simosato	-1	6		-0	3	-10	-12
Mazatlan	Wettzell	14	6		13	2	21	21
Mazatlan	Yaragadee	-49	6		-51	2	-54	-58
Mazatlan	Zimmerwald	19	11		20	4	22	22
McDonald	Greenbelt	7	3		7	2	0	0
McDonald	Maui	18	4		23	2	30	34
McDonald	Monument Peak	24	4		27	2	35	41
McDonald	Orroral	-57	9		-57	3	-50	-52
McDonald	Otay Mountain	39	10		24	2	35	40
McDonald	Owens Valley	12	5		6	3	0	0
McDonald	Platteville	19	22		0	5	0	0
McDonald	Potsdam	34	17		31	5	20	20
McDonald	Quincy	5	4		6	2	0	0
McDonald	RGO	26	6		23	2	22	21
McDonald	Simosato	-1	8		0	3	-9	-11
McDonald	Wettzell	23	7		22	2	21	21
McDonald	Yaragadee	-67	6		-68	2	-67	<b>-7</b> 0
McDonald	Zimmerwald	11	15		29	4	22	22
Monument Peak	Greenbelt	19	2		18	1	14	16
Monument Peak	Maui	-0	3		-1	1	0	0
Monument Peak	Orroral	-74	10		-72	2	-67	-69
Monument Peak	Otay Mountain	-3	5		-3	2	0	0
Monument Peak	Owens Valley	-20	14		-24	3	-44	-51
Monument Peak	Platteville	11	7		8	3	-0	-2
Monument Peak	Potsdam	16	17		17	5	2	-2
Monument Peak	Quincy	-26	1		-27	1	-45	-53
Monument Peak	RGO	12	4		13	2	9	6

Table 7.2 (continued). Geodesic Rates Between SLR Sites

Table 7.2 (continued). Geodesic Rates Between SLR Sites  Observed NAP NUVEL 1 AM0-2									
E	Tro.			Rate	σ	Rate	Rate		
From	To	Rate	<u>σ</u> 5	-34	2	-55	-65		
Monument Peak	Simosato	-33	5 5	-34 9	2	-33 5	-63 0		
Monument Peak	Wettzell	13	3 4	-91	2	-97	-103		
Monument Peak	Yaragadee	-90	_	-91 19	4	- <del>9</del> 7	6		
Monument Peak	Zimmerwald	22	11		2	-51	-53		
Orroral	Greenbelt	-63	5	-51	2	-67	-55 -6 <b>7</b>		
Orroral	Maui	-83	11 2	-65	2	-67 -67	-67 -69		
Orroral	Otay Mountain	-65		-68		-67 -62	-63		
Orroral	Owens Valley	-65	55	-67 -7	3		-63 -62		
Orroral	Platteville	-34	138	-57	4	-61 -47	-62 -42		
Orroral	Potsdam	-28	60	-49	6				
Orroral	Quincy	-69	11	-69	2	-66	-66		
Orroral	RGO	-42	15	-43	4	-49	-43		
Orroral	Simosato	-14	15	-53	4	-71	-66		
Orroral	Wettzell	-33	11	-34	3	-42	-36		
Orroral	Yaragadee	12	4	3	2	0	0		
Orroral	Zimmerwald	-41	31	-32	5	-38	-33		
Otay Mountain	Greenbelt	22	5	15	2	14	16		
Otay Mountain	Maui	19	10	2	2	0	0		
Otay Mountain	Owens Valley	+	†	-24	3	-42	-50		
Otay Mountain	Platteville	9	8	5	3	-0	-2		
Otay Mountain	Potsdam	11	30	14	5	2	-2		
Otay Mountain	Quincy	-24	4	-26	2	-45	-53		
Otay Mountain	RGO	10	2	10	1	9	6		
Otay Mountain	Simosato	-42	15	-33	3	-56	-65		
Otay Mountain	Wettzell	5	1	7	1	4	0		
Otay Mountain	Yaragadee	-98	3	-88	2	-97	-102		
Otay Mountain	Zimmerwald	+	+	16	4	8	5		
Owens Valley	Greenbelt	4	3	7	2	0	0		
Owens Valley	Maui	34	17	7	2	14	17		
Owens Valley	Platteville	20	50	10	4	0	0		
Owens Valley	Potsdam	+	+	22	6	19	18		
Owens Valley	Quincy	-7	6	-1	3	0	0		
Owens Valley	RGO	†	+	16	3	20	20		
Owens Valley	Simosato	-8	8	-7	3	-9	-11		
Owens Valley	Wettzell	17	4	14	3	20	19		
Owens Valley	Yaragadee	-87	7	-79	3	-78	-80		
Owens Valley	Zimmerwald	+	+	22	5	20	20		
Platteville	Greenbelt	-6	8	-4	3	0	0		
Platteville	Maui	23	12	16	3	13	15		
Platteville	Potsdam	22	25	24	6	20	20		
Platteville	Quincy	10	7	11	4	0	0		
Platteville	RGO	20	16	15	4	21	21		
Platteville	Simosato	3	14	5	5	-8	-10		
Platteville	Wettzell	23	10	15	4	20	20		
Platteville	Yaragadee	-67	9	-69	4	-81	-83		
Platteville			21	5	21	21			
Potsdam	Greenbelt	26	13	26	5	21	20		
Potsdam	Maui	-39	17	-33	6	-36	-42		
Potsdam	Quincy	23	18	21	5	19	18		
Potsdam	RGO	7	10	8	5	0	0		

Table 7.2 (continue	). Geodesic Rates Bet	ween SLR Sites
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		Observed		NA	P	NUVEL 1	AM0-2
From	То	Rate	σ	Rate	σ	Rate	Rate
Potsdam	Simosato	-23	12	-24	6	0	0
Potsdam	Wettzell	-3	18	-3	6	0	0
Potsdam	Yaragadee	-42	14	-37	5	-35	-30
Potsdam	Zimmerwald	-0	25	6	8	0	0
Quincy	Greenbelt	7	2	6	1	0	0
Quincy	Maui	3	2	1	1	7	8
Quincy	RGO	16	4	15	2	20	19
Quincy	Simosato	-5	5	-6	2	-9	-11
Quincy	Wettzell	16	4	14	2	19	18
Quincy	Yaragadee	-79	5	-80	2	-81	-82
Quincy	Zimmerwald	30	10	21	4	20	19
RGO	Greenbelt	16	4	17	2	22	22
RGO	Maui	-27	5	-28	2	-24	-28
RGO	Simosato	-19	5	-20	3	0	0
RGO	Wettzell	0	4	-0	2	0	0
RGO	Yaragadee	-28	5	-25	2	-31	-27
RGO	Zimmerwald	8	11	6	4	0	0
Simosato	Greenbelt	-2	5	-4	2	-5	-6
Simosato	Maui	-62	6	-64	3	-88	-99
Simosato	Wettzell	-19	4	-20	3	0	0
Simosato	Yaragadee	-72	6	-70	3	-80	-77
Simosato	Zimmerwald	-14	14	-18	6	0	0
Wettzell	Greenbelt	18	4	16	2	21	21
Wettzell	Maui	-35	5	-38	2	-35	-41
Wettzell	Yaragadee	-25	5	-23	2	-30	-26
Wettzell	Zimmerwald	-0	10	0	6	0	0
Yaragadee	Greenbelt	-77	3	-79	2	-88	-88
Yaragadee	Maui	-90	5	-90	2	-97	-103
Yaragadee	Zimmerwald	-20	18	-22	5	-26	-21
Zimmerwald	Greenbelt	16	11	22	4	22	22
Zimmerwald	Maui	-15	16	-26	5	-29	-34

<sup>†</sup> Indicates that no data exists to provide observed SLR rate.

\* Indicates that rate is determined by only two points.

§ Indicates that the geodesic between the two stations is constrained within NAP.

Table 7.	.3. SL7.1	Tracking	Site	Velocities
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Station	SLR Ve	ocities	Error E	llipse Param	eters	NUVEL-1 N	NR Model
Name			Semi-Major	Semi-Minor	Orient.	Azimuth	Rate
	deg	mm/yr		mm/yr	deg	deg	mm/yr
Quincy	249	23	2.0	1.1	-15	224	20
Owens Valley	249	22	3.4	2.2	-11	226	19
McDonald	221	21	2.4	1.6	-12	239	15
Mazatlan	258	13	2.1	1.7	-28	230	13
Platteville	233	15	4.9	3.0	-20	244	18
Greenbelt	284	17	+	*	*	284	17
Monument Peal	k 287	44	2.1	1.2	-18	299	49
Otay Mountair	289	42	2.5	1.4	-40	299	49
Huahine	289	86	5.7	2.9	-51	297	74
Hawaii	299	70	*	*	*	299	<i>7</i> 0
Wettzell	47	22	3.1	1.5	42	56	25
RGO	38	23	3.5	1.5	32	49	24
Grasse	46	21	3.9	2.7	25	54	25
Zimmerwald	63	22	6.4	4.0	32	54	25
Graz	50	23	3.5	1.8	44	58	25
Potsdam	66	28	6.5	4.5	22	54	25
Simosato†	220	7	3.2	2.2	-51	127	26
Matera	46	21	3.1	1.5	43	43	29
Easter Island	99	81	3.3	2.2	-57	96	84
Arequipa	38	16	2.5	1.6	68	340	10
Orroral	21	57	3.7	1.9	-14	18	60
Yaragadee	34	65	2.4	1.6	-17	33	75

<sup>\*</sup> Greenbelt and Hawaii are constrained to move with NUVEL 1 NNR motion.
† Although the plate upon which Simosato resides is under question, we have assumed Eurasian in our analysis.

### 8. References

- Afonso, G., F. Barlier, C. Berger, F. Mignard and J. J. Walch, Reassessment of the Charge and Neutral Drag of LAGEOS and Its Geophysical Implications, J. Geophys. Res., 90, 9381-9398, 1985.
- Argus, D. F. and R. G. Gordon, No-Net-Rotation Model of Current Plate Velocities Incorporating Plate Motion Model NUVEL-1, submitted to Geophys. Res. Lett., 1991.
- Barlier, F., M. Carpino, P. Farinella, F. Mignard, A. Milani and A. M. Nobili, Non-Gravitational Perturbations on the Semimajor Axis of LAGEOS, *Ann. Geophys.*, 4A, 193-210, 1986.
- Bertotti, B. and L. Iess, The Rotation of LAGEOS, J. Geophys. Res, 96, 2431-2440, 1991.
- Biancale, R., A. Cazenave and K. Dominh, Tectonic Plate Motions Derived from LAGEOS, Earth Planet. Sci. Lett, 103, 379-394, 1991.
- Bomford, G., Geodesy, 4th edition, Oxford Univ. Press, Oxford, 1980.
- Caporali, A., A. Cenci, and M. Fermi, Study of the High-Frequency Structure of Polar Motion Derived from LAGEOS Ranging Data, J. Geophys. Res, 95, 10,965-10,972, 1990.
- Carter, W. E., D. S. Robertson, J. R. MacKay, Geodetic Radio Interferometric Surveying: Applications and Results, J. Geophys. Res., 90, 4577-4587, 1985.
- Christodoulidis, D. C., D. E. Smith, R. Kolenkiewicz, S. M. Klosko, M. H. Torrence, and P. J. Dunn, Observing Tectonic Plate Motions and Deformations from Satellite Laser Ranging, J. Geophys. Res., 90, 9249-9263, 1985.
- Christodoulidis, D. C., D. E. Smith, S. M. Klosko, and P. J. Dunn, Solid Earth and Ocean Tide Parameters from LAGEOS, in *Proc. of the Tenth Intl. Symp. of Earth Tides*, ed. by R. Vieira, 953-961, 1986a.
- Christodoulidis, D. C. R. G. Williamson, D. Chinn, and R. Estes, On the Prediction of Ocean Tides for Minor Constituents, in *Proc. of the Tenth Intl. Symp. of Earth Tides*, ed. by R. Vieira, 659-668, 1986b.
- Christodoulidis, D. C., D. E. Smith, R. G. Williamson and S. M. Klosko, Observed Tidal Braking in the Earth/Moon/Sun System, J. Geophys. Res., 93, 6216-6236, 1988.
- Coates, R. J., H. Frey, G. D. Mead, and J. M. Bosworth, Space-Age Geodesy: The NASA Crustal Dynamics Project, *IEEE Trans. on Geosc. & Rem. Sens., GE-23, 360-368, 1985.*
- Cohen, S. C. and D. E. Smith, LAGEOS Scientific Results: Introduction, J. Geophys. Res., 90, 9217-9220, 1985.
- Degnan, J. J., Satellite Laser Ranging: Current Status and Future Prospects, IEEE Trans. on Geosc. & Rem. Sens., GE-23, 398-413, 1985.
- DeMets, C., R. G. Gordon, D. F. Argus and S. Stein, Current Plate Motions, Geophys. J. Int., 101, 425-478, 1990.
- Diamante, J. M. and R. G. Williamson, Error Models for Solid Earth and Ocean Tidal Effects in Satellite Systems Analysis, Contractor Report prepared for NASA GSFC Geodynamics Branch, 1972.
- Dunn, P. J., D. E. Smith and R. Kolenkiewicz, Techniques for the Analysis of Geodynamic Effects Using Laser Data, in *The Use of Artificial Satellites for Geodesy and Geodynamics*, ed. by G. Veis, 563-575, 1973.
- Eddy, W. F., J. J. McCarthy, D. E. Pavlis, J. A. Marshall, S. B. Luthke, L. S. Tsaoussi, G. Leung and D. A. Williams, GEODYN II Users Manual, Contractor Report prepared for NASA GSFC Space Geodesy Branch, 5 vols., 1990.
- Escobal, P. R., K. M. Ong, O. H. van Roos, M. S. Schumate, R. M. Jaffe, H. F. Fliegel, and P. M. Mueller, 3-D Multilateration: A Precision Geodetic Measurement System, *Jet Prop. Lab., Tech. Memo.* 33-605, 1973.
- Farinella, P., A. M. Nobili, F. Barlier and F. Mignard, Effects of Thermal Thrust on the Node and Inclination of LAGEOS, Astron. Astrophys., 234, 546-554, 1990.
- Fitzmaurice, M. W., P. O. Minott, J. B. Abshire, and H. E. Rowe, Prelaunch Testing of the Laser Geodynamic Satellite (LAGEOS), NASA Tech. Paper 1062, 1977.
- Flinn, E. A. and M. Baltuck, The Role of NASA in Geodynamics Research: Past and Future, EOS, Trans. AGU, 70, 713,722, 1989.
- Gaignebet, J. and F. Baumont (eds.), Sixth International Workshop on Laser Ranging Instrumentation, 2 volumes, GRGS CERGA, Grasse, France, 1986.
- Gendt, G. and R. Dietrich, Determination of Geodynamical Parameters Based on LAGEOS Laser Ranging Data, Gerlands Beitr. Geophysik, Leipzig, 97, 438-449, 1988.
- Geodynamics Program Office, The National Geodynamics Program: An Overview, NASA Tech. Paper 2147, 1983.

- Gilbert, F. and A. M. Dziewonski, An Application of Normal Mode Theory to the Retrieval of Structural Parameters and Source Mechanisms for Seismic Spectra, *Phil. Trans R. Soc.*, 278A, 187-269, 1975.
- Hauck, H. and D. Lelgemann, Die Bildung der Datenmittlewerte (Normalpoints) aus Laserentfernungsmessungen. Arbeiten des Sonderforschungsbereiches 78 der TU München, Veroff. Bayer. Komm. für die Satellitengeodäsie Intern. Erdmessungen, 42, 137-141, 1982.
- Heiskanen, W. A. and H. Moritz, Physical Geodesy, W. H. Freeman, San Francisco, 1967.
- Henriksen, S. W. (ed.), National Geodetic Satellite Program, NASA Spec. Publ. 365, 2 vol., 1977.
- Husson, V., S. Wroe, and S. Wetzel, TLRS-1 and MOBLAS-7 Collocation Report, Bendix Field Engineering internal report, 1987.
- Jacchia, L. G., Revised Static Models of the Thermosphere and Exosphere with Empirical Temperature Profiles, Smithsonian Inst. Astrophys. Obs. Spec. Rpt. 332, Cambridge, Massachusetts, 1971.
- Jurdy, D. M., Reference Frames for Plate Tectonics and Uncertainties, Tectonophysics, 182, 373-382, 1990.
- Kaplan, G. H. (ed.), The IAU Resolutions on Astronomical Constants, Time Scales and the Fundamental Reference Frame, U S Naval Obs. Cir. 163, 1981.
- Kaula, W. M., The Theory of Satellite Geodesy, Blaisdell Publ. Co., Waltham, 1966.
- Kaula, W. M. (ed.), The Terrestrial Environment: Solid Earth and Ocean Physics, NASA Confr. Rpt. 1579, 1970.
- Klosko, S. M., Y. Radway, M. H. Torrence, and D. E. Smith, Baseline Estimation from Simultaneous Tracking (BEST): Recent SLR Results from Quincy to Monument Peak, paper presented to the NASA Crustal Dynamics Meeting, Pasadena, April, 1990.
- Kolenkiewicz, R., D. E. Smith, D. C. Christodoulidis, S. M. Klosko, M. H. Torrence, and P. J. Dunn, Crustal Motion in the Western United States, Mexico, South America, and Easter Island from LAGEOS Satellite Laser Ranging, EOS, Trans. AGU, 66, 246, (abstract), 1985.
- Kolenkiewicz, R., V. Husson, P. J. Dunn, M. Abresch, and S. Poulouse, Collocation Results from TLRS-1 and MOBLAS-7, paper presented to the NASA Crustal Dynamics Meeting, Pasadena, March, 1987.
- Kovalevsky, J., and I. I. Mueller, Comments on Conventional Terrestrial and Quasi-Inertial Reference Systems, in Reference Coordinate Systems for Earth Dynamics, ed. by E. M. Gaposchkin and B. Kolaczek, 375-384, D. Reidel, 1981.
- Lerch, F. J., S. M. Klosko, G. B. Patel, and C. A. Wagner, A Gravity Model for Crustal Dynamics (GEM-L2), J. Geophys. Res., 90, 9301-9311, 1985.
- Lieske, J. H., Precession Matrix Based on IAU(1976) System of Astronomical Constants, Astron. Astrophys., 73, 282, 1979.
- Lieske, J. H., T. Lederle, W. Fricke, and W. Morando, Expressions for the Precession Quantities Based upon the IAU(1976) System of Astronomical Constants, Astron. Astophys., 58, 1, 1977.
- Lieske, J. H. and E. M. Standish, Planetary Ephemerides, in Reference Coordinate Systems for Earth Dynamics, ed. by E. M. Gaposchkin and B. Kolaczek, 295-304, D. Reidel, 1981.
- Majer, V., SOLVE Program Users Guide, Contractor Report prepared for NASA GSFC Space Geodesy Branch, 1986.
- Marini, J. W. & C. W. Murray Jr., Correction of Laser Range Tracking Data for Atmospheric Refraction at Elevations above 10 Degrees, NASA Doc. No. X-591-73-351, 1973.
- Marsh, J. G., F. J. Lerch, B. H. Putney, D. C. Christodoulidis, T. L. Felsentreger, B. V. Sanchez, D. E. Smith, S. M. Klosko, T. V. Martin, E. C. Pavlis, J. W. Robbins, R. G. Williamson, O. L. Colombo, N. L. Chandler, K. E. Rachlin, G. B. Patel, S. Bhati, and D. S. Chinn, An Improved Model for the Earth's Gravitational Field: GEM-T1, NASA Tech. Memo. 4019, 1987.
- Marsh, J. G., F. J. Lerch, B. H. Putney, D. C. Christodoulidis, D. E. Smith, T. L. Felsentreger, B. V. Sanchez, S. M. Klosko, E. C. Pavlis, T. V. Martin, J. W. Robbins, R. G. Williamson, O. L. Colombo, D. D. Rowlands, W. F. Eddy, N. L. Chandler, K. E. Rachlin, G. B. Patel, S. Bhati, and D. S. Chinn, A New Gravitational Model for the Earth from Satellite Tracking Data: GEM-T1, J. Geophys. Res, 93, 6169-6215, 1988.
- Martin, C. F., M. H. Torrence, and C. W. Misner, Relativistic Effects on an Earth-Orbiting Satellite in the Barycenter Coordinate System, J. Geophys. Res, 90, 9403-9410, 1985.
- Masters, E. G., A. Stolz, and B. Hirsch, On Filtering and Compressing LAGEOS Laser Ranging Data, Bull. Geod., 57, 121-130, 1983.
- McCarthy, D. D., C. Boucher, R. Eanes, T. Fukushima, T. Herring, J. Lieske, C. Ma, H. Montag, P. Pâquet, C. Reigber, J. Ries, B. E. Schutz, E. M. Standish, C. Veillet, and J. Wahr, IERS Standards (1989), IERS Tech. Note 3, Observatory de Paris, France, 1989.
- Melbourne, W., R. J. Anderle, M. Feissel, R. King, D. D. McCarthy, B. D. Tapley, and R. Vicente, Project MERIT Standards, U. S. Naval Obs. Cir. 167, 1983.

- Merson, R. H., The Motion of a Satellite in an Axi-symmetric Gravitational Field, Geophys. J., 4, 17-52, 1961.
- Merson, R. H. and D. G. King-Hele, Use of Artificial Satellites to Explore the Earth's Gravitational Field: Results from Sputnik 2 (1957β), Nature, 182, 640-641, 1958.
- Minster, J. B., and T. H. Jordan, Present-Day Plate Motions, J. Geophys. Res., 83, 5331-5354, 1978.
- Molnar, P. and J. M. Stock, Relative Motions of Hotspots in the Pacific, Atlantic and Indian Oceans since Late Cretaceous Time, *Nature*, 327, 587-591, 1987.
- Moritz, H., Geodetic Reference System 1980, Bull. Geod., 62, 348-358, 1988.
- Moritz, H. and I. I. Mueller, Earth Rotation Theory and Observations, F. Ungar, New York, 1987.
- Mueller, I. I., Introduction to Satellite Geodesy, F. Ungar Publ. Co., New York, 1964.
- Mueller, I. I., Reference Coordinate Systems for Earth Dynamics: A Preview, in Reference Coordinate Systems for Earth Dynamics, ed. by E. M. Gaposchkin and B. Kolaczek, 1-22, D. Reidel, 1981.
- Mueller, I. I. (ed.), Proceedings of the International Conference on Earth Rotation and Terrestrial Reference Frames, Dept. of Geod. Sci. & Surv., The Ohio State University, 1985.
- Murdoch, A. and W. Decker, Crustal Dynamics Satellite Laser Ranging Network Preliminary TOPEX/Poseidon Laser Network Support Plan, NASA Rpt. CDSLR-03-0002, 1989.
- NASA Office of Space Science and Applications, Solid Earth Science in the 1990's, Volume 1 Program Plan, NASA Tech. Memo. 4256, 1991.
- Newhall, X X, E. M. Standish, and J. G. Williams, DE 102: A Numerically Integrated Ephemeris of the Moon and Planets Spanning Forty-Four Centuries, Astron. Astrophys., 125, 150-167, 1983.
- O'Keefe, J. A., A. Eckels, and R. K. Squires, Vanguard Measurements Give Pear-Shaped Component of Earth's Figure, Science, 129, 565-566, 1959.
- Olsen, P., Drifting Mantle Hotspots, Nature, 327, 559-560, 1987.
- Pagiatakis, S. D., The Response of a Realistic Earth to Ocean Tide Loading, Geophys. J. Int. 103, 541-560, 1990.
- Pavlis, E. C., Secular Polar Motion from 14 Years of Laser Ranging to LAGEOS, paper presented to the 18th NASA Crustal Dynamics Meeting, Pasadena, April, 1990.
- Pavlis, E. C., Polar Motion from Satellite Laser Ranging to LAGEOS, NASA Tech. Memo., in preparation, 1991.
- Pavlis, E. C., R. G. Williamson, and D. E. Smith, High Resolution Polar Motion from the LAGEOS Tracking, EOS, Trans. AGU, 69, 1154, (abstract), 1988.
- Putney, B., R. Kolenkiewicz, D. Smith, P. Dunn and M. Torrence, Precision Orbit Determination at the NASA Goddard Space Flight Center, *Adv. Space Res.*, 10(3), 197-203, 1990.
- Rapp, R. H. and N. K. Pavlis, The Development and Analysis of Geopotential Coefficient Models to Spherical Harmonic Degree 360, J. Geophys. Res., 95, 21,885-21,911, 1990.
- Ries, J.C., The Along-Track Acceleration of LAGEOS, EOS Trans. AGU, 72, April 23 supplement, 95, 1991.
- Ries, J. C., C. Huang and M. M. Watkins, Effect of Genral Relativity on a Near-Earth Satellite in the Geocentric and Barycentric Reference frames, *Phys. Rev. Lett.*, 61, 903-906, 1988.
- Rubincam, D. P., Atmospheric Drag as the Cause of the Secular Decrease in the Semimajor Axis of LAGEOS's Orbit, Geophys. Res. Lett., 7, 468-470, 1980.
- Rubincam, D. P., On The Secular Decrease in the Semimajor Axis of LAGEOS's Orbit, Celest. Mech., 26, 361-382, 1982.
- Rubincam, D. P., Postglacial Rebound Observed by LAGEOS and the Effective Viscosity of the Lower Mantle, J. Geophys. Res., 89, 1077-1087, 1984.
- Rubincam, D. P., LAGEOS Orbit Decay Due to Infrared Radiation from Earth, J. Geophys. Res, 92, 1287-1294, 1987.
- Rubincam, D. P., Yarkovsky Thermal Drag on LAGEOS, J. Geophys. Res, 93, 13,805-13,810, 1988.
- Rubincam, D. P., Drag on the LAGEOS Satellite, J. Geophys. Res., 95, 4881-4886, 1990a.
- Rubincam, D. P., The LAGEOS Along-Track Acceleration: A Review, paper presented to the First William Fairbank Meeting on Relativistic Gravitational Experiments in Space, Rome, Italy, September 10-14, 1990b.
- Rubincam, D. P. and N. R. Weiss, Earth Albedo and the Orbit of LAGEOS, Celest. Mech., 38, 233-296, 1986. Rubincam, D. P., P. Knocke, V. R. Taylor, and S. Blackwell, Earth Anisotropic Reflection and the Orbit of LAGEOS, J. Geophys. Res., 92, 11,662-11,668, 1987.
- Scharroo, R., K. F. Wakker, B. A. C. Ambrosius, and R. Noomen, On the Along-Track Acceleration of the LAGEOS Satellite, J. Geophys. Res. 96, 729-740, 1991.
- Schneider, M., Satellitengeodäsie, B. I. Wissenschaftsverlag, Mannheim, 1988.
- Seeber, G., Satellitengeodäsie, Walter de Gruyter, Berlin, 1988.

- Sellers, P. C. and P. A. Cross, A Pseudo Short-Arc Technique for Precise Regional Satellite Laser Ranging Baselines, Man. Geod., 15, 207-227, 1990.
- Shawe, M. E. and A. G. Adelman, Precision Laser Tracking for Global and Polar Motion, IEEE Trans. on Geosc. & Rem. Sens., GE-23, 391-397, 1985.
- Smith, D. E. and P. J. Dunn, Long-Term Evolution of the LAGEOS Orbit, Geophys. Res. Lett, 7, 437-440, 1980.
- Smith, D. E. and F. O. Vonbun, The San Andreas Fault Experiment, Acta Astr., 1, 1445-1452, 1974.
- Smith, D. E., D. C. Christodoulidis, R. Kolenkiewicz, P. J. Dunn, S. M. Klosko, M. H. Torrence, S. Fricke, and S. Blackwell, A Global Geodetic Reference Frame from LAGEOS Ranging (SL5.1AP), J. Geophys. Res., 90, 9221-9233, 1985.
- Smith, D. E., M. H. Torrence, P. J. Dunn and E. C. Pavlis, Definition of the Vertical from LAGEOS Laser Ranging, EOS Trans. Amer. Geophys. U., 71, 1275, abstract, 1990a.
- Smith, D. E., R. Kolenkiewicz, P. J. Dunn, J. W. Robbins, M. H. Torrence, S. M. Klosko, R. G. Williamson, E. C. Pavlis, N. B. Douglas and S. K. Fricke, Tectonic Motion and Deformation from Satellite Laser Ranging to LAGEOS, J. Geophys. Res., 95, 22,013-22,041, 1990b.
- Stolz, A., M. A. Vincent, P. L. Bender, R. J. Eanes, M. M. Watkins, and B. D. Tapley, Rate of Change of the Quincy-Monument Peak Baseline from a Translocation Analysis of LAGEOS Laser Range Data, Geophys. Res. Lett., 16, 539-542, 1989.
- Tapley, B. D., B. E. Schutz and R. J. Eanes, Station Coordinates, Baselines, and Earth Rotation from LAGEOS Laser Ranging: 1976-1984, J. Geophys. Res., 90, 9235-9248, 1985.
- Torrence, M. H., S. M. Klosko and D. C. Christodoulidis, The Construction and Testing of Normal Points at Goddard Space Flight Center, Fifth Int'l. Workshop on Laser Ranging Instrumentation, Herstmonceux, 1984.
- Van Dam, T. M. and J. M. Wahr, Displacements of the Earth's Surface Due to Atmospheric Loading: Effects on Gravity and Baseline Measurements, J. Geophys. Res., 92, 1281-1286, 1987.
- Veillet, C. (ed.), Seventh International Workshop on Laser Ranging Instumentation, OCA/CERGA, Grasse, 1990.
- Vincenty, T. Direct and Inverse Solutions of Geodesics on the Ellipsoid with Application of Nested Equations, Surv. Rev., 22, 176-183, 1975.
- Vondrák, J., Problem of Smoothing Observational Data, Bull. Astron. Czecho., 28, 84, 1977.
- Wahr, J. M., The Forced Nutations of an Ellipsoidal Rotating, Elastic and Oceanless Earth, Geophys. J. R. Astron. Soc., 64, 705-727, 1981.
- Wells, D. E. and P. Vanicek, Least Squares Spectral Analysis, Bedford Institute of Oceanography Report BI-R-78-8, 1978.

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## LAGEOS Geodetic Analysis - SL7.1

### Appendix 1

Tracking Station Eccentricity Information

Site	Station	Occ	Occ.	Location	Plate	Start	End	Station	Eccentr	icity
No.	Number		System	Location	11410	Date		orth	east	uр
			<del></del>	ONDREION	THEACIAN		31-DEC-91	.000	.000	.000
1148 1181	11480901 11813901	ONDLAS GDRLAS	OND. FIXED GDR FIXED	ONDREJOV POTSDAM, E	EURASIAN EURASIAN	01-JAN-88 01-JAN-74	31-DEC-91	.000	.000	.000
1863	18635101	MDNLAS	MDN. FIXED	MAIDANAK	EURASIAN	01-JUL-90	31-DEC-91	.000	.000	.000
1866	18665201	DNVLAS	DUN. FIXED	DUNAOVCY	EURASIAN	01-JUL-90	31-DEC-91	.000	.000	.000
1867	18675301	EVPLAS	EVP. FIXED	EVPATORIA	EURASIAN	01-JUL-90	31-DEC-91 31-DEC-91	.000. 000.	.000 .000	.000 .000
1873 1884	18734901 18844401	SIMLAS RGALAS	SIM. FIXED RGA FIXED	SIMEIZ RIGA, USSR	EURASIAN EURASIAN	01-MAY-76 20-SEP-87	31-DEC-91	.000	.000	.000
1893	18931801	CRMLAS	CRIMEA FIX	KATZIVELY	EURASIAN	01-MAY-76	31-DEC-91	.000	.000	.000
1953	19532001	CUBLAS	CUBA FIXE	SANTIAGO D	NORTH AM	01-MAY-76	31-DEC-91	.000	.000	.000
7148	11480901	ONDLAS	OND. FIXED	ONDREJOV	EURASIAN EURASIAN	01-JAN-88 01-JAN-74	31-DEC-91 31-DEC-91	.000 .000	.000 .000	.000 .000
7181 7863	11813901 18635101	GDRLAS MDNLAS	GDR FIXED MDN. FIXED	POTSDAM, E MAIDANAK	EURASIAN	01-JUL-90	31-DEC-91	.000	.000	.000
7866	18665201	DNVLAS	DUN. FIXED	DUNAOVCY	EURASIAN	01-JUL-90	31-DEC-91	.000	.000	.000
7867	18675301	<b>EVPLAS</b>	EVP. FIXED	EVPATORIA	EURASIAN	01-JUL-90	31-DEC-91	.000	.000	.000
7873	18734901	SIMLAS	SIM. FIXED	SIMEIZ	EURASIAN EURASIAN	01-MAY-76 20-SEP-87	31-DEC-91	.000 .000	.000 .000	.000 .000
7884 7893	18844401 18931801	RGALAS CRMLAS	RGA FIXED CRIMEA FIX	RIGA, USSR KATZIVELY	EURASIAN	01-MAY-76	31-DEC-91 31-DEC-91	.000	.000	.000
7953	19532001	CUBLAS	CUBA FIXE	SANTIAGO D	NORTH AM	01-MAY-76	31-DEC-91	.000	.000	.000
7035	70351301	TL0306	TLRS-3	OTAY MOUNT	PACIFIC	24-JUN-88	31-DEC-88	N .006	E .017	2.587
7046	70461501	MT0127	MTLRS-1	BEAR LAKE	NORTH AM	03-AUG-90	31-DEC-90	N1.776	E1.946	1.335
7051 7051	70510101 70510202	ML0102 ML0206	MOBLAS-1 MOBLAS-2	QUINCY, CA OUINCY, CA	NORTH AM NORTH AM	27-AUG-74 09-JUL-76	27-NOV-74 30-NOV-76		W .001 W .003	3.680 3.604
7051	70510202	ML0200 ML0210	MOBLAS-2	OUINCY, CA	NORTH AM	01-JAN-79	30-MAY-79	S .006	E .004	3.619
7051	70510804	ML0803	MOBLAS-8	QUINCY, CA	NORTH AM	01-FEB-81	21-MAY-81	S .022	E .023	3.279
7061	70611201	TL0202	TLRS-2	EASTER ISL	NAZCA	10-JAN-83	02-AUG-83	.000	.000	1.736
7061 7062	70611202 70620201	TL0205 ML0202	TLRS-2 MOBLAS-2	EASTER ISL OTAY MOUNT	NAZCA PACIFIC	19-MAR-84 28-AUG-74	12-DEC-84 14-DEC-74	.000 S .005	.000 .000	1.735 3.570
7062	70620302	ML0303	MOBLAS-3	OTAY MOUNT	PACIFIC	30-AUG-76	30-APR-77	.000	.000	3.615
7062	70620303	ML0306	MOBLAS-3	OTAY MOUNT	PACIFIC	29-JUN-78	30-MAY-79	S .011	W .010	3.568
7062	70621104	TL0115	TLRS-1	OTAY MOUNT	PACIFIC	04-OCT-81	09-JAN-82	N .031	W1.601	3.415
7062 7063	70621205 70632101	TL0203 STALAS	TLRS-2 GSFC FIXED	OTAY MOUNT GORF, CSFC	PACIFIC NORTH AM	12-SEP-83 01-MAY-76	04-JAN-84 29-AUG-81	.000 .000	.000 .000	1.794 3.036
7064	70640101	ML0101	MOBLAS-1	GORF, GSFC	NORTH AM		30-JUN-74	.000	.000	2.978
7064	70640102	ML0105	MOBLAS-1	GORF, GSFC	NORTH AM		30-NOV-77		E .002	2.966
7065	70650201	ML0201	MOBLAS-2	GORF, GSFC	NORTH AM		30-JUN-74	.000	.000	3.417
7065 7065	70650203 70650302	ML0207 ML0302	MOBLAS-2 MOBLAS-3	GORF, GSFC GORF, GSFC	NORTH AM NORTH AM		21-NOV-77 09-JUL-76	S .013 S .081	E .002 W .176	3.468 3.465
7066	70662701	WFCLAS	WAL. FIXED	WALLOPS IS	NORTH AM		01-JUN-79	.000	.000	9.080
7067	70670101	ML0103	MOBLAS-1	BERMUDA IS	NORTH AM		16-JUL-76	.000	.000	3.701
7067	70670102		MOBLAS-1	BERMUDA IS	NORTH AM	•	09-NOV-78		W .008	3.689
7068 7068	70680201 70680202	ML0204 ML0209	MOBLAS-2 MOBLAS-2	GRAND TURK GRAND TURK	NORTH AM NORTH AM		05-MAR-76 07-NOV-78		E .005 W .029	3.578 3.678
7069	70692201	RAMLAS	PAFB FIXED	PATRICK AI	NORTH AM	•		.000	.000	3.436
7070	70700201	ML0203	MOBLAS-2	WALLOPS IS	NORTH AM		28-FEB-75	.000	.000	3.360
7080	70802401	MLRS07	MLRS	MCDONALD O			03-JUN-88	N .004	E .005	1.756
7080	70802402	MLRS08	MLRS MT PS	MCDONALD O			21-SEP-88 12-SEP-89	N .004 N .004	E .005 E .005	1.756 1.756
7080 7080	70802403 70802404	MLRS09 MLRS10	MLRS MLRS	MCDONALD	NORTH AM		28-SEP-89	N .004	E .005	1.756
7080	70802405		MLRS	MCDONALD	NORTH AM	27-SEP-89	18-NOV-89		E .005	1.756
7080	70802406		MLRS	MCDONALD	NORTH AM		15-JAN-90	N .004	E .005	1.756
7080 7080	70802407 70802408		MLRS MLRS	MCDONALD MCDONALD	NORTH AM NORTH AM		25-JAN-90 03-APR-90	N .004 N .004	E .005 E .005	1.756 1.756
7080	70802409		MLRS	MCDONALD	NORTH AM	•	29-APR-90	N .004	E .005	1.756
<b>708</b> 0	70802410		MLRS	MCDONALD	NORTH AM		06-JUN-90	N .004	E .005	1.756
7080	70802411		MLRS	MCDONALD	NORTH AM		25-SEP-90	N .004	E .005	1.756
7080 7080	70802412 70802413		MLRS MLRS	MCDONALD MCDONALD	NORTH AM NORTH AM		01-DEC-90 09-APR-91	N .004 N .004	E .005 E .005	1.756 1.756
7080	70802413		MLRS	MCDONALD	NORTH AM		31-DEC-91	N .004	E .005	1.756
7081	70810201	ML0205	MOBLAS-2	PATRICK AI	NORTH AM		07-MAY-76		.000	3.422
7082	70820101	ML0104	MOBLAS-1	BEAR LAKE,	NORTH AM		30-NOV-76		E .003	3.774
7082	70820102 70821102		MOBLAS-1 TLRS-1	BEAR LAKE, BEAR LAKE,	NORTH AM NORTH AM		20-AUG-79 06-MAY-81		E .005 E1.112	3.817 3.517
7082 7082	70821103 70821104		TLRS-1	BEAR LAKE,	NORTH AM			N .998	E1.112 E1.207	3.521
7083	70830301		MOBLAS-3	GORF, GSFC	NORTH AM	01-JAN-75	15-JUN-75	.000	.000	2.873
7084	70840201		MOBLAS-2	OWENS VALL			31-MAR-78		.000	3.493
7085	70850101		MOBLAS-1	GOLDSTONE,	NORTH AM		31-MAR-78 31-MAY-80		W .008 W .007	3.866
7086 7086	70860101 70861102	ML0109 TL0105	MOBLAS-1 TLRS-1	MCDONALD C MCDONALD C			09-AUG-80		W .140	3.788 3.536
7086	70862403		MLRS	MCDONALD C				S5.315	E5.591	1.994
7086	70862404	MLRS02	MLRS	MCDONALD C	NORTH AM				E5.590	1.977
7086	70862405		MLRS	MCDONALD C			30-JUL-87 01-FEB-88	\$5.308 \$5.308	E5.590 E5.590	1.997 1.977
7086	70862406	MLRS04	MLRS	MCDONALD C	NORTHAM	1 30-JUL-0/	01-1-ED-00	55.500	لىرى. ئارىي	1.7//

				T1:	Dieto	Ctart	End	Station	Eccentr	icity
Site	Station		Occ.	Location		Start Date		rth	east	up
No.	Number	Name	System							3.185
7090	70900501		MOBLAS-5	YARAGADEE,	AUSTRALI AUSTRALI	01-JUL-79 27-JUL-83	27-JUL-83 19-NOV-84	N .003 N .003	E .011 E .011	3.185
7090		ML0503	MOBLAS-5 MOBLAS-5	YARAGADEE, YARAGADEE,	AUSTRALI	19-NOV-84	05-SEP-85	N .003	E .011	3.185
7090 7090		ML0504 ML0505	MOBLAS-5	YARAGADEE,	AUSTRALI	05-SEP-85	16-APR-87	N .003	E .011	3.185
7090	70900505	ML0506	MOBLAS-5	YARAGADEE,	AUSTRALI	23-APR-87	13-AUG-87 26-AUG-87	N .003 N .003	E .011 E .011	3.185 3.185
7090	70900506	ML0507	MOBLAS-5	YARAGADEE, YARAGADEE,	AUSTRALI AUSTRALI	13-AUG-87 26-AUG-87	26-AUG-87 05-AUG-89	N .003	E .011	3.185
7090 7090	70900507 70900508	ML0508 ML0509	MOBLAS-5 MOBLAS-5	YARAGADEE,	AUSTRALI	05-AUG-89	31-DEC-91	N .003	E .010	3.177
7091	70910301	ML0305	MOBLAS-3	HAYSTACK O	NORTH AM	05-DEC-77	01-APR-78	.000 S .016	E .003 W .003	3.748 3.381
7091	70910702	ML0702	MOBLAS-7	HAYSTACK O	NORTH AM NORTH AM	10-JUN-79 09-AUG-88	14-NOV-80 17-OCT-88	N1.556	E .121	3.476
7091	70911103	TL0147 TL0156	TLRS-1 TLRS-1	HAYSTACK O WESTFORD	NORTH AM	10-OCT-90	12-DEC-90		E .059	3.497
7091 7092	70911104 70920801	ML0802	MOBLAS-8	KWAJALEIN,	PACIFIC	15-AUG-79	01-NOV-80	S .015	E .045	3.142 3.198
7096	70960601	ML0602	MOBLAS-6	AMERICAN S	PACIFIC	10-JUN-79 11-NOV-87	14-NOV-80 29-FEB-88	.000 N .000	.000 E .000	1.496
7097	70971201	TL0210	TLRS-2 TLRS-2	EASTER ISL EASTER ISL	NAZCA NAZCA	22-SEP-88	31-DEC-89	N .000	E .000	1.474
7097 7097	70971202 70971203	TL0212 TL0214	TLRS-2	EASTER ISL	NAZCA	06-OCT-89	31-DEC-90	N .000	E .000	1.482
7100		ML0304	MOBLAS-3	GORF, GSFC	NORTH AM		18-NOV-77 13-OCT-78	.000 N .005	W .002 E .021	3.513 3.191
7100		ML0401	MOBLAS-4	GORF, GSFC GORF, GSFC	NORTH AM NORTH AM	01-MAR-78 01-FEB-82	01-JUN-82	N .119	W .648	3.150
7101	71010602 71010801	ML0603 ML0801	MOBLAS-6 MOBLAS-8	GORF, GSFC	NORTH AM	01-AUG-78	30-MAY-79	N .168	W .691	3.133
7101 7102	71020305	ML0309	MOBLAS-3	GORF, GSFC	NORTH AM	01-DEC-84	31-DEC-91	N .058	E .018 W .004	3.488 3.205
7102	71020402		MOBLAS-4	GORF, GSFC	NORTH AM	15-MAY-79 01-DEC-82	15-NOV-82 31-MAR-83	S.002 N.008	E .048	3.154
7102	71020403	ML0403	MOBLAS-4 MOBLAS-4	GORF, GSFC GORF, GSFC	NORTH AM NORTH AM	01-DEC-82 01-APR-83	31-JUL-83	5.019	E .042	3.196
7102 7102	71020404 71020501	ML0404 ML0501	MOBLAS-5	GORF, GSFC	NORTH AM	01-APR-78	17-MAY-79	S .009	E .002	3.208
7102	71021106		MOBLAS-5	GORF, GSFC	NORTH AM	21-OCT-88	01-JAN-89 06-MAR-89	N1.566	E .018 E .018	3.267 3.267
7102	71021107	TL0149	MOBLAS-5	GORF, GSPC	NORTH AM NORTH AM		10-MAY-79	.000	W .033	3.192
7103	71030601 71030602		MOBLAS-6 MOBLAS-6	GORF, GSFC GORF, GSFC	NORTH AM		02-NOV-82	S .046	W .006	3.166
7103 7104	71040701	ML0701	MOBLAS-7	GORF, GSFC	NORTH AM		04-JUN-79	N .069	E .062 W .026	3.130 3.149
7105	71050701	ML0703	MOBLAS-7	GORF, GSFC	NORTH AM NORTH AM		15-JUN-81 01-FEB-83	N .016 N .016	W .026	3.149
7105	71050702 71050703		MOBLAS-7 MOBLAS-7	GORF, GSFC GORF, GSFC	NORTH AM		22-AUG-83	N .017	E .031	3.168
7105 7105	71050703		MOBLAS-7	GORF, GSFC	NORTH AM	22-AUG-83	22-MAR-84		E .031	3.168
7105	71050705		MOBLAS-7	GORF, GSFC	NORTH AM			N .017 N .017	E .031 E .031	3.168 3.168
7105	71050708		MOBLAS-7	GORF, GSFC GORF, GSFC	NORTH AM NORTH AM		27-MAR-86		E .031	3.168
7105 7105	71050709 71050710		MOBLAS-7 MOBLAS-7	GORF, GSFC	NORTH AM			N .017	E .031	3.168
7105 7105	71050711		MOBLAS-7	GORF, GSFC	NORTH AM		27-JUL-88	N .017	E .031 E .031	3.168 3.168
7105	71050712		MOBLAS-7	GORF, GSFC	NORTH AM		08-JAN-89 14-JUN-89	N .017 N .017	E .031	3.168
7105	71050713		MOBLAS-7 MOBLAS-7	GORF, GSFC GREENBELT	NORTH AM NORTH AM		02-AUG-89	N .017	E .031	3.168
7105 7105			MOBLAS-7	GREENBELT	NORTH AM	03-AUG-89	12-OCT-89	N .017	E .031	3.168
7105	71050716	ML0716	MOBLAS-7	GREENBELT	NORTH AM		24-JUL-90	N .035 N .014	E .040 E .033	3.162 3.153
7105		ML0717	MOBLAS-7	GREENBELT GREENBELT		25-JUL-90 01-SEP-90	31-AUG-90 31-DEC-91	N .014	E .033	3.153
7105 7109			MOBLAS-7 MOBLAS-8	QUINCY, CA	NORTH AM	1 01-OCT-81	29-JUL-82	N .012	E .011	3.225
7109			MOBLAS-8	QUINCY, CA	NORTH AM	15-AUG-82	12-MAR-85		E .011 E .011	3.124 3.124
7109	71090803		MOBLAS-8	QUINCY, CA	NORTH AN	12-MAR-85 1 15-AUG-85	15-AUG-85 18-SEP-86	S .029 S .029	E .011	3.124
7109			MOBLAS-8 MOBLAS-8	QUINCY, CA QUINCY, CA	NORTH AM		12-DEC-88		E .011	3.124
7109 7109			MOBLAS-8	QUINCY, CA	NORTH AM	1 12-DEC-88			E .011	3.124
7109		7 ML0810	MOBLAS-8	QUINCY, CA	NORTH AM		03-JUL-83	S .029 S .007	E .011 W .003	3.124 3.520
7110			MOBLAS-3 MOBLAS-4	MOUNT LAGU MOUNT LAGU		13-JUL-81 15-AUG-83			W .015	3.209
7110 7110			MOBLAS-4	MOUNT LAGE		19-NOV-8	6 30-APR-88		W .015	3.209
7110			MOBLAS-4	MOUNT LAGI		29-APR-88		S .033 S .033	W .015 W .015	3.209 3.209
7110	7110040		MOBLAS-4	MOUNT LAGU MOUNT LAGU	J PACIFIC J PACIFIC	15-JUN-88 13-DEC-88			W .015	3.209
7110 7111			MOBLAS-4 TLRS-1	VANDENBER	G PACIFIC	28-APR-82	25-MAY-82	S1.162	W1.051	3.312
7112			MOBLAS-2	PLATTEVILL	NORTH AN		1 13-OCT-84	N .005	W .002	3.511 1.351
7112	7112150	2 MT0116	MTLRS-1	PLATTEVILL	NORTH AN		30-SEP-88 23-FEB-90	S2.705 N .007	E .011 E .022	2.628
7112		3 TL0407 4 MT0128	TLRS-4 MTLRS-1	PLATTEVILL PLATTEVILL	NORTH AN		31-DEC-90		E .042	1.347
7112 7114			MOBLAS-2	OWENS VAL	L NORTH AN	4 08-JUN-79	31-JAN-81	S.003	W .008	3.622
7114		2 TL0114	TLRS-1	OWENS VAL	L NORTH AN		l 29-SEP-81 2 22-JAN-83	N1.512 N1.520	W .442 W .364	3.466 3.521
7114			TLRS-1 MOBLAS-3	OWENS VAL GOLDSTONE	L NORTH AN NORTH AN				W .029	3.615
7115 7120			MOBLAS-3 MOBLAS-1	LURE OBS.,	PACIFIC	15-JUN-80	22-JAN-82	S .013	E .009	3.602
712	1 7121010	1 ML0111	MOBLAS-1	HUAHINE, S	PACIFIC	01-FEB-83	13-APR-86		E .006 W .007	3.662 3.182
712	2 7122060	1 ML0605	MOBLAS-6	MAZATLAN,	NORTH AM	M UI-MAK-8	3 16-MAR-8	100.61	44 .007	5.104

Site	Station	Occ	Occ.	Location	Plate	Start	End	Station	n Eccent	ricity
No.	Number		System			Date		rth	east	up
7122	71220602	ML0606	MOBLAS-6	MAZATLAN,	NORTH AM	27-MAY-84	15-DEC-85	N .001	W .007	3.182
7122	71220603	ML0607	MOBLAS-6	MAZATLAN,	NORTH AM	16-DEC-85	21-JAN-87	N .001	W .007	3.182
7122	71220604	ML0608	MOBLAS-6	MAZATLAN, MAZATLAN,	NORTH AM NORTH AM	28-JAN-87 17-AUG-88	17-AUG-88 12-DEC-91	N .001 N .002	W .007 W .006	3.182 3.181
7122 7122	71220605 71220606	ML0609 ML0610	MOBLAS-6 MOBLAS-6	MAZATLAN, MAZATLAN,	NORTH AM	17-AUG-66 13-JAN-89	22-JUN-89	N .002 N .002	W .006	3.181
7122	71220607		MOBLAS-6	MAZATLAN	NORTH AM	23-JUN-89	03-OCT-89	N .002	E .006	3.181
7122	71220608	ML0612	MOBLAS-6	MAZATLAN	NORTH AM	04-OCT-89	31-DEC-91	N .002	E.006	3.181
7123	71231201	TL0209 TL0211	TLRS-2 TLRS-2	HUAHINE, S HUAHINE, S	PACIFIC PACIFIC	14-JUL-87 16-MAR-88	31-DEC-87 01-SEP-88	N .000 N .000	E .000 E .000	1.453 1.437
7123 7123	71231202 71231203	TL0213	TLRS-2	HUAHINE	PACIFIC	24-APR-89	03-SEP-89	N .000	E .000	1.482
7123	71231204	TL0215	TLRS-2	HUAHINE	PACIFIC	15-MAR-90	31-DEC-90	N .001	E .003	1.459
7125	71251501	MT0104	MTLRS-1	GORF, GSFC	NORTH AM	01-MAY-85	23-JUL-85	N .354	E2.118	1.338
7125	71251302	TL0304 TL0208	TLRS-3 TLRS-2	GREENBELT GREENBELT	NORTH AM NORTH AM	15-SEP-87 06-NOV-85	28-JAN-88 19-MAY-87	N .000 N .000	E .000 E .000	2.580 2.486
7130 7206	71301201 72062601	MCLAS1	2.7 METER	MCDONALD O	NORTH AM	01-MAY-76	29-JUN-85	5.810	W .041	5.328
<b>72</b> 10	72102301	HOLLAS	HALEAKALA	LURE OBS.,	PACIFIC	01-MAY-76	31-MAR-84	N .752	.000	.848
<b>7</b> 210	72102302	HOLLAS	HALEAKALA	LURE OBS.,	PACIFIC	01-APR-84	15-JUL-87	N .752	E .000	.848
7210	72102303	HOLLAS	HALEAKALA	LURE OBS.,	PACIFIC PACIFIC	16-JUL-87 04-AUG-89	04-AUG-89 31-DEC-91	N .752 N .753	E .000 E .001	. <b>84</b> 8 . <b>84</b> 8
7210 7220	72102304 72201101	HOLLAS TL0124	HALEAKALA TLRS-1	HALEAKALA MOUNT LAGU	PACIFIC	30-AUG-83	02-NOV-83		E .656	3.248
7220	72201102	TL0132	TLRS-1	MOUNT LAGU	PACIFIC	28-DEC-84	10-JAN-85	.000	.000	.000
7220	72201103	TL0133	TLRS-1	MOUNTLAGU	PACIFIC	13-JAN-85	27-FEB-85	.000	.000	.000
7220	72201104	TL0134	TLRS-1	MOUNT LAGU	PACIFIC	03-MAR-85	23-MAR-85	.000	.000	.000
7220 7236	72201105 72362901	TL0135 WUHLAS	TLRS-1 WUH. FIXED	MOUNT LAGU WUHAN	PACIFIC EURASIAN	24-MAR-85 01-JAN-88	13-MAY-85 31-DEC-91	.000 .000	.000 .000	.000 .000
7265	72651101	TL0126	TLRS-1	BARSTOW, C	NORTH AM	18-JAN-84	06-MAR-84	N .470	W1.502	3.491
7274	72741101	TL0136	TLRS-1	MOUNT LAGU	PACIFIC	16-MAY-85	18-JUL-85	.000	.000	.000
7288	72881301	TL0305	TLRS-3	BARSTOW, C	NORTH AM		16-JUN-88	N .000	E .003	2.584
7288 7288	72881402 72881403	TL0403 TL0406	TLRS-3 TLRS-4	BARSTOW, C MOJAVE	NORTH AM NORTH AM	23-JAN-89 21-OCT-89	19-APR-89 31-JAN-90	N .005 N .013	E .011 E .004	2.610 2.617
<b>7288</b>	72881404	TL0410	TLRS-4	MOJAVE	NORTH AM		22-FEB-91	N .008	E .012	2.637
<b>729</b> 5	<b>729515</b> 01	MT0116	MTLRS-1	RICHMOND	NORTH AM		21-JUL-88	N2.611	E .196	1.341
7295	72951102	TL0157	TLRS-1	RICHMOND	NORTH AM		17-APR-91	N .166	E1.565	3.288
7300 7301	73001701 73011701	HT0103 HT0104	HTLRS-1 HTLRS-1	MINAMI TOR OKINAWA	EURASIAN EURASIAN	10-JAN-89 03-AUG-89	24-MAR-89 04-SEP-89	.000 .000	. <b>00</b> 0 . <b>00</b> 0	.000 .000
7302	73021701	HT0105	HTLRS-1	TUSIMA	EURASIAN	03-OCT-89	25-NOV-89	.000	.000	.000
7307	73071701	HT0102	HTLRS-1	ISIGAKI-SI	PACIFIC	18-JUL-88	17-SEP-88	.000	.000	.000
7308	73085001	CRLLAS	CRLLAS	TOKYO	PACIFIC	01-JAN-90	31-DEC-91	.000	.000	.000
7400 7401	74001101 74011101	TL0127 TL0128	TLRS-1 TLRS-1	SANTIAGO, CERRO TOLO	SOUTH AM SOUTH AM	07-MAR-84 14-MAY-84	10-MAY-84 30-JUN-84	.000 N1.580	.000 E .119	.000 3.309
<b>74</b> 01	74011302	TL0311	TLRS-3	CERRO TOLO	SOUTH AM		02-JUN-90	N .022	E .009	2.699
7401	74011303	TL0313	TLRS-3	CERRO TOLO	SOUTH AM		13-MAR-91	N .017	E .004	2.701
7403	74031301	TL0312	TLRS-3	AREQUIPA	SOUTH AM	14-JUN-90	31-DEC-90	N .013	E.011	2.683
7510 7510	75101501 75101602	MT0109 MT0213	MTLRS-1 MTLRS-2	ASKITES, G ASKITES	EURASIAN EURASIAN	21-MAY-86 25-MAY-87	22-JUL-86 29-AUG-87	N2.546 N2.619	E .026 E .073	1.344 1.358
7510	75101603		MTLRS-2	ASKITES	EURASIAN	05-AUG-89	02-NOV-89		E .059	1.357
7510	75101504		MTLRS-1	ASKITES	EURASIAN	03-NOV-89			E .006	1.358
7512 7512	75121501	MT0111	MTLRS-1	KATAVIA, R	EURASIAN	05-SEP-86	19-OCT-86 15-MAY-87		E.073	1.340
7512 7512	75121602 75121503		MTLRS-2 MTLRS-1	KATAVIA, R KATAVIA	EURASIAN EURASIAN	19-MAR-87 10-OCT-89	28-OCT-89		E .070 E .075	1.353 1.344
7515	75151501		MTLRS-1	DIONYSOS	EURASIAN	27-JUL-86	31-AUG-86		E .014	1.328
<b>75</b> 15	75151502	MT0114	MTLRS-1	DIONYSOS	EURASIAN	20-JUL-87	23-OCT-87		E .003	1.329
7515 7517	75151503 75171601		MTLRS-1	DIONYSOS	EURASIAN EURASIAN	15-DEC-89 27-MAY-86	31-MAR-90 01-SEP-86	N2.616 N2.592	E .028 E .058	1.333 1.360
7517 7517	75171001		MTLRS-2 TLRS-1	ROUMELLI ROUMELLI	EURASIAN	20-JUL-87	28-AUG-87		E .058	3.309
7517	75171503		MTLRS-1	ROUMELLI	EURASIAN	22-OCT-87	11-DEC-87	N2.576	E .014	1.339
7517	75171104		TLRS-1	ROUMELLI	EURASIAN	16-APR-89	27-JUN-89		E .072	3.238
7520 7520	75201501 75201502	MT0108 MT0120	MTLRS-1 MTLRS-1	KARITSA KARITSA	EURASIAN EURASIAN	18-MAK-86 07-JUN-89	14-MAY-86 08-AUG-89		E .020 E .070	1.339 1.354
7525	75251601		MTLRS-2	XRISOKALAR	EURASIAN	03-SEP-86	13-SEP-86	N2.572	E .103	1.370
7525	75251602	MT0210	MTLRS-2	XRISOKALAR	EURASIAN	14-SEP-86	15-SEP-86	N2.572	E .103	1.370
7525 7525	75251603		MTLRS-2	XRISOKALAR	EURASIAN	15-SEP-86	19-OCT-86		E.103	1.371
7525 7525	75251104 75251105		TLRS-1 TLRS-1	XRISOKALAR XRISOKALAR	EURASIAN EURASIAN	10-SEP-87 19-NOV-89	11-DEC-87 31-MAR-90		E .078 E .018	3.263 3.260
7530		ML0214	MOBLAS-2	BAR GIYYOR	AFRICAN	02-AUG-85			E .579	2.024
7530	75300202	ML0215	MOBLAS-2	BAR GIYYOR	AFRICAN	08-AUG-89	31-DEC-91	N .000	E .579	2.024
7540 7541		MT0106	MTLRS-1	MATERA, IT	EURASIAN	08-JAN-86	17-MAR-86		E .022	1.321
7541 7543		MT0206 MT0222	MTLRS-2 MTLRS-2	MATERA, IT NOTO	EURASIAN EURASIAN	08-DEC-85 22-OCT-90	13-MAR-86 13-DEC-90		E .115 E .264	1.336 1.361
7544		MT0222 MT0214	MTLRS-2 MTLRS-2	LAMPEDUSA,	AFRICAN	14-SEP-87	11-DEC-87		E .016	1.363
7544	75441502	MT0119	MTLRS-1	LAMPEDUSA	AFRICAN	21-MAR-89	05-JUN-89	N2.686	E .038	1.346
<b>754</b> 5	75451601	MT0205	MTLRS-2	PUNTA SA M	EURASIAN	19-OCT-85	07-DEC-85	N2.607	E .089	1.348

						C1 = =4	End	Station	Eccentri	icity
Site	Station		Occ.	Location		Start			east	up
No.	Number	Name	System			Date				
7545	75451602	MT0215	MTLRS-2	PUNTA SA M	EURASIAN	08-JAN-88	24-MAR-88 24-APR-90	N2.632 N .038	E .037 E1.565	1.361 3.249
<b>754</b> 5	75451103	MT0220	MTLRS-2	PUNTA SA M BOLOGNA, I	EURASIAN EURASIAN	01-JAN-90 28-MAR-88	04-IUN-88	N2.648	E .112	1.349
7546	75461601 75501601	MT0216 MT0207	MTLRS-2 MTLRS-2	BASOVIZZA	EURASIAN	18-MAR-86	20-MAY-86		E .552	1.346
7550 7550	75501601	MT0207	MTLRS-2	BASOVIZZA	EURASIAN	23-MAY-89	26-JUL-89	N2.631	E .045 E .087	1.353 1.328
7575	75751501	MT0112	MTLRS-1	DIYARBAKIR	ARABIAN ARABIAN	23-MAR-87 07-SEP-89	15-MAY-87 29-SEP-89	N2.625 N2.676	E .067 E .166	1.350
7575	75751502	MT0122	MTLRS-1 TLRS-1	DIYARBAKIR MELENGICLI	EURASIAN	02-APR-87	16-MAY-87	N1.574	E.103	3.318
7580 7580	75801101 75801102	TL0141 TL0152	TLRS-1	MELENGICLI	EURASIAN	16-OCT-89	12-NOV-89		E .230	3.245 1.344
7585	75851501	MT0113	MTLRS-1	YOZGAT	EURASIAN	25-MAY-87 15-AUG-89	03-JUL-87 07-SEP-89	N2.581 N2.603	E .168 E .153	1.344
7585	75851502	MT0121	MTLRS-1	YOZGAT YIGILCA	EURASIAN EURASIAN	20-MAY-87	03-JUL-87	N1.576	E .036	3.307
7587 7587	75871101 75871102	TL0142 TL0151	TLRS-1 TLRS-1	YIGILCA	EURASIAN	05-JUL-89	11-OCT-89	N1.559	E.198	3.273
7590	75901601	MT0204	MTLRS-2	MONTE GENE	EURASIAN	01-SEP-85	19-OCT-85	N2.307 N2.407	E .513 E .030	1.132 1.371
7596	75961601	MT0202	MTLRS-2	WETTZELL,	EURASIAN EURASIAN	01-MAR-85 07-AUG-85	16-APR-85 31-DEC-85		E.006	1.341
7596	75961502	MT0105	MTLRS-1 MTLRS-1	WETTZELL, WETTZELL,	EURASIAN	01-FEB-85	23-MAR-85	N2.524	E .009	1.333
7597 7597	75971501 75971502	MT0103 MT0104	MTLRS-1	WETTZELL,	EURASIAN	29-MAR-85	03-APR-85	N2.585	E .001	1.324
7599	75991501	MT0102	MTLRS-1	WETTZELL,	EURASIAN	01-SEP-84	31-DEC-84 01-OCT-90	N2.304 N .792	E .055 E2.004	1.368 1.349
7602	76021601	MT0221	MTLRS-2	TROMSOE	EURASIAN EURASIAN	05-AUG-90 01-AUG-78	31-DEC-91	.000	.000	.000
7805	78053301	FINLAS	FIN. FIXED SWI. FIXED	KIRKKONUM BERN, SWIT	EURASIAN	01-MAY-84	31-DEC-91	.000	.000	.000
7810 7811	78104801 78113801	ZIMLAS POLLAS	POL. FIXED	BOROWIEC,	EURASIAN	01-JAN-83	31-DEC-87	.000	.000	.000
7811	78113802	POLLAS	POL. FIXED	BOROWIEC,	EURASIAN	01-JAN-88	31-DEC-91	.000 .000	,000 ,000	.000 .000
7824	78244501	SPNLAS	SPN. FIXED	SAN FERNAN	EURASIAN AFRICAN	01-MAY-76 25-OCT-83	31-DEC-91 31-DEC-91	.000	.000	.000
7831	78314601	HELLAS	EGY. FIXED NL. FIXED	HELWAN, EG KOOTWIJK O	EURASIAN	01-MAY-76		.000	.000	.000
7833	78333201 78343001	KOOLAS WETLAS	GER. FIXED	WETTZELL,	EURASIAN	01-MAY-76	31-DEC-91	.000	.000	.000
7834 7835	78353101	GRASSE	FRA. FIXED	GRASSE, FR	EURASIAN	01-MAY-76	21-MAR-83		.000 .000	.000 .000
7835	78353102	GRASSE	FRA. FIXED	GRASSE, FR	EURASIAN	23-DEC-83 01-AUG-83	31-DEC-91 31-DEC-91	.000 N .000	E .000	.000
7837	78373701	CHILAS	SO FIXED	SHANGHAI SIMOSATO H	EURASIAN EURASIAN	01-MOG-83			.000	2.100
7838	78383601 78393401	SHOLAS AUSLAS	SHO FIXED GRAZ FIXED	GRAZ, AUST	EURASIAN	01-SEP-83	31-JUL-88	.000	.000	.000
7839 7839	78393402		GRAZ FIXED	GRAZ, AUST	EURASIAN	31-JUL-88	31-DEC-91		.000 .000	.000 .000
7840	78403501		RGO FIXED	ROYAL GREE	EURASIAN	30-MAR-83 01-AUG-84	31-DEC-91 31-DEC-91		.000	.000
7843	78432501		NLRS HTLRS-1	ORRORAL VA	AUSTRALI PACIFIC	01-JAN-88	31-MAR-8	.000	.000	.000
7844 7853	78441701 78531501		MTLRS-1	OWENS VALL	NORTH AM	01-OCT-88	30-NOV-8	8 52.674	W .014	1.321
7853	78531502		MTLRS-1	OWENS VALL	NORTH AM		31-DEC-90		E .004 .000	1.330 1.703
7882	78821201		TLRS-2	CABO SAN L CABO SAN L	PACIFIC PACIFIC	01-FEB-84 21-MAR-88	10-MAR-8 01-AUG-8		E1.525	3.254
7882	78821102		TLRS-1 TLRS-4	ENSENADA	PACIFIC	25-APR-89	13-JUL-89	N .006	E .006	2.626
7883 7883	78831401 78831402		TLRS-4	ENSENADA	PACIFIC	14-JUL-89	06-OCT-89		E .006	2.626 3.571
7885	78851101	TL0119	TLRS-1	MCDONALD C			10-OCT-82 28-AUG-83		E .543 .000	.000
7886	78861101		TLRS-1	QUINCY, CA QUINCY, CA	NORTH AM		14-JUL-84	.000	.000	.000
7886	78861102 78861103		TLRS-1 TLRS-1	QUINCY, CA	NORTH AM	1 06-AUG-84	08-SEP-84		.000	.000
7886 7886			TLRS-1	QUINCY, CA	NORTH AM	1 10-SEP-84	18-DEC-84		.000 E .678	.000 3.339
7887		TL0121	TLRS-1	VANDENBERG		25-JAN-83 4 25-JAN-82			E .467	3.419
7888			TLRS-1 TLRS-2	MOUNT HOPK GORF, GSFC	NORTH AM NORTH AM				.000	1. <b>72</b> 0
7889 7889			TLRS-2	GORF, GSFC	NORTH AM	4 01-AUG-85	15-OCT-8		.000	.000
7889			TLRS-3	GORF, GSFC	NORTH AM		4 01-AUG-8 23-FEB-80		.000 E .379	.000 3.257
7890			TLRS-1	AUSTIN, TX AUSTIN, TX	NORTH AN				W1.510	3.301
7890			TLRS-1 TLRS-1	FLAGSTAFF,	NORTH AN			1 S.001	W1.574	3.384
7891 7892			TLRS-1	VERNAL, UT	NORTH AN	и 07-MAY-8			E1.562	3.358 3.332
7892		2 TL0118	TLRS-1	VERNAL, UT	NORTH AN				E1.570 .000	.000
7894			TLRS-1	YUMA PROVI MOUNT WILS	NORTH AN				.000	.000
7895			TLRS-1 TLRS-1	JET PROPUL	PACIFIC	24-OCT-80	) 06-JAN-8	1 N1.510	E .459	3.314
7896 7897			TLRS-1	MCDONALD (	O NORTH AN				E .102 E .126	3.197 3.333
7897	7897110	2 TL0102	TLRS-1	MCDONALD (	NORTH AN			S1.549 N1.541	E .126	3.313
7899			TLRS-1 TLRS-1	GORF, GSFC GORF, GSFC	NORTH AN				E .326	3.311
7899 7907			SAO-2	AREQUIPA,	SOUTH AN	и 01-SEP-70	15-JUN-8	8 .000	.000	.000
7907			SAO-2	AREQUIPA,	SOUTH AN	4 15-JUN-88			.000 E .579	.000 2.024
7917	7 7917420	1 SAO302	SAO-3	GORF, GSFC	NORTH AN	M 01-SEP-84 M 22-AUG-8			E .001	2.464
7918			TLRS-3 TLRS-3	GORF, GSFC GORF, GSFC	NORTH A				E .001	2.464
7918 7918			TLRS-4	GREENBELT	NORTH A	M 01-FEB-88	23-DEC-8		E .006	2.603
791			TLRS-4	GREENBELT	NORTH A	M 06-MAR-9	0 24-JUL-9	N .011	E .005	2.615

Site	Station	Occ.	Occ.	Location	Plate	Start	End	Station	Eccent	ricity
No.	Number	Name	System			Date	Date	north	east	up
<b>79</b> 18	<b>791814</b> 05	TL0409	TLRS-4	GREENBELT	NORTH AM	24-JUL-90	04-OCT-9	0 N .007	E.005	2.613
7919	<b>791914</b> 01	TL0401	TLRS-4	GORF, GSFC	NORTH AM	18-NOV-85	02-APR-8	7 N.000	E .011	2.591
<b>792</b> 0	<b>792</b> 01101	TL0137	TLRS-1	GORF, GSFC	NORTH AM	29-JUL-85	15-JAN-86	N1.556	E .143	3.287
<b>792</b> 0	79201102	TL0138	TLRS-1	GORF, GSFC	NORTH AM	16-JAN-86	19-DEC-8	6 N1.586	E .081	3.319
<b>792</b> 0	79201103	TL0139	TLRS-1	GORF, GSFC	NORTH AM	21-DEC-86	20-JAN-87	7 N1.586	E .081	3.319
<b>792</b> 0	79201104	TL0140	TLRS-1	GORF, GSFC	NORTH AM	21-JAN-87	06-FEB-87	N1.586	E .081	3.319
<b>792</b> 0	<b>7920</b> 1105	TL0145	TLRS-1	GORF, GSFC	NORTH AM	03-FEB-88	08-MAR-8	8 N1.586	E .081	3.319
<b>792</b> 0	79201306	TL0307	TLRS-3	GREENBELT	NORTH AM	03-OCT-88	15-FEB-89	N1.566	E .849	2.700
<b>792</b> 0	79201307	TL0308	TLRS-3	GREENBELT	NORTH AM	16-FEB-89	18-JUN-89	N1.567	E .857	2.695
7920	79201308	TL0309	TLRS-3	GREENBELT	NORTH AM	19-JUN-89	12-OCT-8	9 N1.566	E .858	2.696
<b>792</b> 0	79201309	TL0310	TLRS-3	GREENBELT	NORTH AM	12-OCT-89	16-NOV-8	39 N1.569	E .860	2.697
<b>792</b> 0	79201110	TL0155	TLRS-1	GREENBELT	NORTH AM	04-SEP-90	31-DEC-9	0 N1.572	E .054	3.241
<b>792</b> 1	79214301	SAO401	SAO-4	MOUNT HOPK	NORTH AM	10-FEB-68	06-MAR-8	32 .000	.000	.000
7929	79294101	SAO101	SAO-1	NATAL, BRA	SOUTH AM	31-OCT-70	01-OCT-8	1 .000	.000	.000
7939	79394101	SAO102	SAO-1	MATERA, IT	EURASIAN	01-MAY-83	31-JUL-91	.000	.000	.000
<b>794</b> 0	79404701	GRELAS	GRE. FIXED	NATIONAL T	EURASIAN	01-MAY-84	31-DEC-9	1 .000	.000	.000
<b>794</b> 3	79434201	SAO301	SAO-3	ORRORAL VA	<b>AUSTRALI</b>	15-JUN-76	10-MAR-8	32 .000	.000	.000
<b>79</b> 99	79991101	TL0106	TLRS-1	MCDONALD O	NORTH AM	09-AUG-80	11-AUG-8	.000	.000	.000
8833	88331501	MT0101	MTLRS-1	KOOTWIJK O	EURASIAN	01-APR-84	31-MAY-8	.000	.000	.000
8833	88331602	MT0201	MTLRS-2	KOOTWIJK O	EURASIAN	15-NOV-84	28-FEB-85	.000	.000	.000
8833	88331603	MT0203	MTLRS-2	Kootwijk o	EURASIAN	18-APR-85	31-AUG-8		.000	.000
8833	88331604	MT0217	MTLRS-2	Kootwijk o	EURASIAN	04-JUN-88	24-MAY-8		.000	.000
8833	<b>883316</b> 05	MT0220	MTLRS-2	KOOTWIJK O	EURASIAN	05-NOV-89	31-DEC-9	000. 0	.000	.000

# LAGEOS Geodetic Analysis - SL7.1

## Appendix 2

Monthly Tracking Summaries by Station

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
			<del></del>			(cm)	(cm)	(cm)
1181	8309	2	15	15	15	17	32	16
1181	8310	7	45	34	34	8	26	10
1181	8311	6	64 71	64	64	-25	34 20	-25 12
1181 1181	8312 8401	10 12	71 96	67 52	67 52	-6 -5	30 16	-12 -14
1181	8402	10	58	39	39	-5 4	22	-14 -2
1181	8403	23	163	93	93	4	19	-2
1181	8404	9	55	36	<b>36</b>	5	16	2
1181	8405	5	37	22 28	22	16	24	8
1181 1181	8406 8407	5 8	41 58	28 40	28 40	0 - <b>12</b>	16 19	-2 -14
1181	8408	17	123	72	72	-18	36	-15
1181	8409	4	38	27	27	1	22	-4
1181	8410	7	64	33	33	-4	10	-7
1181 1181	8411 8412	10 6	110 31	34 15	34 15	<b>4</b> -1	14 16	-2 -9
1181	8502	3	20	13 17	17	-1 19	50	- <del>9</del> -1
1181	8503	<b>2</b> 5	16	ii	ii	-8	26	i
1181	8504	5	35	24	24	5	19	0
1181	8505	5 5	40	13	13	-5 27	12	-5
1181 1181	8506 8507	5 7	45 83	16 <b>2</b> 9	16 29	-37 3	<b>4</b> 0 16	-21 -5
1181	8509	11	99	34	34	10	17	-3 7
1181	8510	11	76	15	15	2	10	-3
1181	8511	3	<b>2</b> 0	15 77	15	19	23	18
1181 1181	8512 8601	3 3	37 26	37 15	37 15	-3 14	32 19	-8 14
1181	8602	13	140	63	63	12	21	9
1181	8603	12	118	25	25	2	12	2
1181	8604	3	30	30	30	23	35	20
1181 1181	8605 8606	3	22	8	8	2	17	2
1181	8609	1	14	9	9	-2	7	3
1181	8610	5	38	13	13	-8	12	
1181	8611	4	44	24	24	9	13	
1181 1181	8612 8702	<i>7</i> 15	67 120	24	24	-5 24	10	
1181	8702 8703	15 24	129 216	71 23	71 23	-2 <b>4</b> -7	35 9	-27 -7
1181	8704	6	44	12	12	<b>-6</b>	11	-10
1181	8705	14	144	29	29	-3	8	-13
1181	8706	4	34	11	11	-1	8	-6
1181 1181	8707 8708	8 10	<i>69</i> 91	21 34	21 34	-2 -5	8 12	-8 -8
1181	8709	13	115	39	38	-5 53	33 <b>4</b>	- <del>0</del> -6
1181	8710	14	116	44	44	2	11	-ĕ
1181	8711	4	48	30	30	11	16	4
1181	8712 8801	6 7	54 63	28 20	28 20	11	13	3
1181 1181	8801 8802	7 4	63 34	30 25	30 25	6 16	10 18	6 16
1181	8803	1	8	سه	<i>₩</i>	10	10	10
1181	8804	5 5	61	36	36	11	14	12 5
1181	8805	5	61	23	23	7	11	5
1181 1181	8806 8807	2 7	11 42	10 7	10 7	14 11	18 15	4
1181	8808	9	42 93	,	,	11	15	6
1181	8809	ıí	<i>7</i> 5	40	40	9	19	8
1181	8810	15	178	64	64	23	27	17
1181	8811	4	32 300	32	32	20	29 25	20
1181 1181	8901 8902	18 16	200 175	200 173	200 173	10 11	27 29 25 27	6
1181	8903	14	138	138	138	8	2/ 26	10 6
1181	8904	8	103	103	103	11	18	6
1181	8905	11	110	108	108	3	22	1
1181	8906	1	6 m	6	6	14	18	-3 -2 0
1181 1181	8907 8909	3 2	23 19	22 19	22 19	6	16	-2
1181	8910	3	19 29	19 29	19 29	-6 -8	18 24	0 -8
1181	9001	4	25	29 25	25 25	-6 24	33	15
1101	9002	17	185	182	182	-3	31	2 -3
1181 1181	9003	6	<i>7</i> 1	70	70	11	28	

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
Mantber	Date	1 40000	11			(cm)	(cm)	(cm)
1181 1181 1181 1181 1181	9004 9006 9007 9008 9009	1 7 15 8	13 57 164 81 3	13 56 164 81 3	13 56 163 81 3	-17 17 10 24 29	20 31 75 48 113	-18 12
1181 1181 1873 1873 1873 1873 1873	9010 9012 8907 8910 9003 9004 9009 9010	22 4 1 2 2 5 1 7	252 42 3 6 2 5 7 36	252 42	251 41	36 158	383 1011	
1873 1873 1884 1884 1884 1884	9011 8709 8710 8711 8712 8801 8809	6 2 19 8 4 4	22 142 68 28 28 33	142 30	1 <b>25</b> 0	128 1371	535 1490	246 -1
1884 1884 1884 1884 1884 1884	8810 8811 8812 8901 8902 8903	34 11 7 2 17 3	336 101 64 23 245 43 175	75 63 23 245 43 175	75 63 15 245 43 175	44 -86 -146 -110 -78 -160	105 118 205 137 106 186	192 56 32 51 25
1884 1884 1884 1884 1884 1884	8905 8910 8911 8912 9003 9004 9005	2 4 3 12 29 16	21 30 18 127 355 195	21 30 18 127 355 195	17 24 18 127 355 195	-98 -129 -64 -127 -138 -124 433	134 169 92 157 165 150 449	51 33 63 32 31 31
1893 1893 1893 1893 1893 1893	8902 8903 8905 8906 9002 9003	3 2 4 1 2 6 4	36 19 25 11 7 64 23	36 19 25 11 7 64 23	0 0 0 0 0	465 585 502 528 465 474	483 620 532 572 477 492	-1 -1 -1 -1 -1
1893 1953 1953 1953 1953 1953	9011 8803 8804 8805 8810 8811 8812	2 5 3 12 17 8	14 53 15 138 200 84	5 4 2 37 185 84	5 4 2 37 183 84	14 -31 9 34 43 21	17 36 26 53 61 48	-60 -106 -115 -22 -24 -41
1953 1953 1953 1953 1953 1953 1953 1953	8901 8902 8906 8911 8912 9001	15 15 2 12 9 4	143 93 7 107 70	140 76 7 107 70 19	140 76 7 106 70 19	21 37 5 63 43 38 57 61	52 35 84 59 63 61 70	-47 -1 -5 -19
1953 1953 7035 7035 7051 7051 7051	9002 9012 8808 8809 7604 7605 7606	2 13 26 30	9 125 362 451	9 125 278 345	9 125 278 345	29 3 4	42 4 10	2 3 6 -85 -16
7051 7051 7051 7051 7051 7051	7607 7608 7609 7610 7611 7903	3 2 5 11 1	22 4 20 30 13	22 4 20 27 13	22 4 20 27 13	19 -26 13 -9 7	26 33 40 33 12	-22 -20 <i>-</i> 7
7051 7051 7051 7051 7051 7051	7904 7905 8102 8103 8104	7 5 2 20 45	66 62 34 387 686	65 61 34 387 668	65 61 34 387 668	-2 -17 -11 -1 6	12 19 14 16 17	-7 -24 -26 -7 0

Station	Deti	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
	·					(ent)	(ent)	(СП.)
7051	8105	37	537	526	526	9	14	1
7061 7061	8303 8304	9 18	47 128	31 120	31 117	3 -1	8 13	13
7061	8305	23	263	257	248	-1 -6	13 16	6 <b>4</b>
7061	8306	20	218	208	204	-1	17	5
7061 7061	8307 8405	1 5	7 28	27	27	3	6	14
7061	8406	1	15	15	15	6	8	19
7061 7061	8407 8408	15 2	104 11	99 11	95 11	-4 2	150 19	15 10
7061	8409	5	22	20	20	10	12	19 20
7061	8410	8	51 25	50	50	8	11	16
7061 7061	8411 8412	7 3	25 23	25 22	25 22	3 1	9 6	12 14
7062	7606	J			-	•	O	-19
7062 7062	7607 7608	1	16					-3
7062	7610	5	16 <b>4</b> 5	42	42	-18	49	9
7062	7611	49	508	494	490	1	34	
7062 7062	7612 7702	19 17	186 220	186 217	186 217	0 - <b>4</b> 5	<b>2</b> 0 51	<b>-4</b> 5
7062	7703	16	192	164	164	-20	29	-42
7062	7704 7807	14	162	156	156	-4	21	-16
7062 7062	7807 7808	7 29	65 357	64 352	64 352	5 - <b>3</b>	20 11	- <b>4</b> -7
7062	7809	11	128	125	125	-8	22	7
7062 7062	7811 7812	3 5	34 32	34 32	22 32	64 -5	122	14
7062	7901	3	18	32 18	32 18	-5 6	20 38	-8 5
7062	7902	10	118	118	112	13	33	5
7062 7062	7903 7904	7 22	63 256	63 25 <b>4</b>	63 254	-7 -17	18 28	-19 -14
7062	7905	10	110	1 <b>09</b>	109	-13	20	-14
7062 7062	8110 8111	14 20	113 156	105 156	102 156	-6 1	14 10	-2 7
7062	8112	18	151	151	151	5	14	14
7062 7062	8201 8309	<b>2</b> 5	9 57	9 57	9 54	7	9	18
7062 7062	8310	12	129	111	108	9 9	10 10	14 11
7062	8311	4	<b>7</b> 0	70	<del>69</del>	6	7	13
7062 7062	8312 8401	2 4	14 27	4 27	4 23	13 15	15 17	11 18
7063	7602					13	.,	-34
7063 7063	7605 7606	14 6	146 81	146 48	144 48	-31 -47	46 60	-14
7063	7704	8	64	64	64	50	58	-26
7063 7063	7705 7707	1 1	<b>14</b> 1	14	14	61	<del>69</del>	-37
7063 7063	7708	3	38	1 38	0 38	-14 -37	0 <b>4</b> 5	-1 -5
7063	7709	1	15	15	15	-16	91	-71
7063 7063	<i>7</i> 710 <i>7</i> 711	12 3	135 40	130 40	130 40	-21 -12	28 14	-4 19
7063	<i>7</i> 712	2	30	30	30	9	15	-5
7063 7063	7801 7802	1 1	10 9	10 9	10	53	59	<b>3</b> 6
7063	7803	15	187	184	9 183	-13 <i>-</i> 7	1 <b>4</b> 1 <b>4</b>	-26 -11
7063	7804	13	195	183	183	12	22	-15
7063 7063	7807 7808	5 8	59 91	55 89	55 89	12 2	23 6	7 -6
7063	7809	8	90	89	89	-4	12	7
7063 7063	7812 7901	2 1	21 2	21	21	25	34	12
7063	7901 7902	7	7 <u>1</u>	69	$\boldsymbol{\Theta}$	-3	24	-6
7063	7903	14	197	185	185	6	18	-3
7063 7063	7904 7905	12 17	182 205	177 188	1 <i>77</i> 188	7 7	13 14	-3 -4
7063	7909	22	262	245	245	-2	9	-4 -4
7063	<i>7</i> 910 <i>7</i> 911	33 23	488 284	483 282	483 282	1 -6	12 18	-4 -2 -6 -2
7063								

7063 7063 7063 7063 7063 7063 7063 7063	8001 8002 8003 8004 8005 8007 8008 8009 8010 8012 8101 8102 8103 8104 8105 8106	Passes  16 3 22 11 11 5 13 31 22 9 2 9 33	123 24 317 183 159 51 131 340 171	101 22 316 175 115 42 102 273 149	101 21 316 175 115 42 102	Residual (cm)  3 -10 -2 0 -1 3	Residual (cm)  10 16 6 6 8 6	-2 -7 -3 -5 -3 0
7063 7063 7063 7063 7063 7063 7063 7063	8002 8003 8004 8005 8007 8008 8009 8010 8012 8101 8102 8103 8104 8105	3 22 11 11 5 13 31 22 9	24 317 183 159 51 131 340 171	22 316 175 115 42 102 273	21 316 175 115 42 102	-10 -2 0 -1 3	16 6 6 8	-3 -5 -3
7063 7063 7063 7063 7063 7063 7063 7063	8002 8003 8004 8005 8007 8008 8009 8010 8012 8101 8102 8103 8104 8105	3 22 11 11 5 13 31 22 9	24 317 183 159 51 131 340 171	22 316 175 115 42 102 273	21 316 175 115 42 102	-10 -2 0 -1 3	16 6 6 8	-3 -5 -3
7063 7063 7063 7063 7063 7063 7063 7063	8003 8004 8005 8007 8008 8009 8010 8012 8101 8102 8103 8104 8105	22 11 11 5 13 31 22 9 2	317 183 159 51 131 340 171 114	316 175 115 42 102 273	316 175 115 4 <u>2</u> 102	-2 0 -1 3	6 6 8	-3 -5 -3
7063 7063 7063 7063 7063 7063 7063 7063	8004 8005 8007 8008 8009 8010 8012 8101 8102 8103 8104 8105	11 11 5 13 31 22 9 2	183 159 51 131 340 171 114	175 115 42 102 273	175 115 42 102	0 -1 3	6 8	-3
7063 7063 7063 7063 7063 7063 7063 7063	8005 8007 8008 8009 8010 8012 8101 8102 8103 8104 8105	11 5 13 31 22 9 2	159 51 131 340 171 114	115 42 102 273	115 42 102	-1 3	8	-3
7063 7063 7063 7063 7063 7063 7063 7063	8007 8008 8009 8010 8012 8101 8102 8103 8104 8105	5 13 31 22 9 2	51 131 340 171 114	42 102 273	42 102	3	6	^
7063 7063 7063 7063 7063 7063 7063 7063	8008 8009 8010 8012 8101 8102 8103 8104 8105	13 31 22 9 2 9	131 340 171 114	102 273		_		
7063 7063 7063 7063 7063 7063 7063 7063	8009 8010 8012 8101 8102 8103 8104 8105	31 22 9 2 9	171 114			2	7	-1
7063 7063 7063 7063 7063 7063 7063 7063	8012 8101 8102 8103 8104 8105	9 2 9	114	149	273	3	9	1
7063 7063 7063 7063 7063	8101 8102 8103 8104 8105	2 9			147	1 0	14 8	-3 1
7063 7063 7063 7063	8102 8103 8104 8105	9		114 36	114 36	3	9	6
7063 7063 7063	8103 8104 8105	20	36 140	36 140	36 140	2	15	i
7063 7063	8104 8105		536	536	508	ī	124	1
7063	8105	4	27	25	25	15	23	2
		8	70	58	58	-4	13	-4
7063	0100	3	26	21	21	3	10	-7 -6
7063	8107	12	138	138	137	-3 <b>4</b>	1 <del>4</del> 9	-0 -2
7063	8108	14	242	242	241 5	-32	38	0
7064	7711	1	5	5	3	-32	30	-44
7067	7602 7606	2	9	2	2	-2	27	
7067 7067	7806	1	ģ	9	9	32	36	16
7067	7807	7	40	37	37	12	23	-23
7067	7808	11	100	94	94	-1	9	-23
7067	7809	7	56	52	52	4	16 11	1 5
7068	7809	4	26	2 <del>4</del> 14	24 14	-2 0	29	-70
7069	7903	2 4	14 27	19	19	30	33	-55
7069 7060	7904 7908	1	4	15		-		
7069 7069	7909	i	2	1	1	6	0	-44
7069	7910	2	11	9	7	33	46	<b>-45</b>
7069	8001	1	6	6	5	-3	28 20	-65 - <b>86</b>
7069	8002	3	19	18	16 14	-21 -4	30 9	-00 -78
7069	8003	3	14	1 <b>4</b> 5	14 5	- <del>14</del> -14	21	-89
7069	800 <u>4</u> 8008	1 1	5 3	3	3	-24	49	-89
7069 7080	8802	16	233	199	199	-5	10	-3 -3 -3
7080	8803	49	716	624	624	-4	7	-3
7080	8804	28	377	282	282	-2	5	-3 0
7080	8805	20	257	18	18	-1	4	U
7080	8806	20	266	~	33	-1	4	-1
7080	8807	19	250 64	33	33	-1	•	•
7080	8808 8809	6 31	429	195	195	-4	6	-4
7080 7080	8809	51	12	34	34	7 -2	11	1
7080	8810	66	958	<i>7</i> 85	<b>785</b>	-2	13	-2
7080	8811	66 33 22	477	477	477	-1 -5 -5 -9 -4 -5	16	1 -2 -2 -5 -4 -8 -5 -6 -10
7080	8812	22	296	296	296	-5	10 <b>14</b>	-5 -1
7080	8901	34 27 28 12	471 221	471 321	<b>471</b> 321	-5 -9	17	-8
7080 7080	8902 8903	2/	321 262	262	262	4	12	-5
7080 7080	8904	12	179	179	179	-5	9	-6
7080	8905	32	460	460	460	-10 -8 -7	18	-10
7080	8906	32 27 22 17	270	259	259	-8	15 25	-9 -7
7080	8907	22	243	243	243	-// 10	35 29	-/ -11
7080	8908	17	249	249	249	-18 -4	6	-11 -4
7080 7080	8909	32	476	123 99	123 99	-2	18	-1
7080 7080	8909 8910	26	466	466	466	-2 0	27 5	0
7080 7080	8911	36 17	182	33	33	-1	5	0 6 3 1
7080	8911			149	149	-1	7	3
7080	8912	6	68	68	68	2	7 6	1 1
7080	9001	30	337	171	171 107	-1 -6	6 7	-1 _ <b>1</b>
7080	9001	~	2.17	107	107 224	-6 -11	15	-3
7080	9002	23 15	2.36 157	224 157	224 157	-11 -7	16	-1
7080	9003	15 5	157 64	64	64	1	11	3
7080 7080	9004 9005	5 11	130	130	130	1	12	-1 -4 -3 -1 3 5
7080 7080	9006	3	35	35	35 43	-6	15	2
7080	9007	4	35 <b>43</b>	35 43	43	1	10	

Station	_	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual	Residual	Estimate
						(cm)	(cm)	(cm)
7080	9008	2	16	16	16	2	5	
7080	9009	10	92	92	92	5	9 5	
7080	9010	12	119	119	119	-1		
7080	9011	25	229	229	229	3	13	
7080 7082	9012 7605	11	103	103	103	4	11	-23
7082 7082	7606							- <u>2.5</u> -1
7082	7607							-10
7082	7609	4	12	11	11	-19	25	
7082	7610	6	42	40	33	67	122	
7082 7082	7611 7903	31 7	323 26	307 22	306 22	0 11	30 16	-14
7082 7082	7904	8	73	70	70	1	16	-6
7082	7905	10	113	90	90	39	53	46
7082	7907	21	246	243	243	10	27	31
7082	7908	8	91	91 240	91	12	22	26
7082 7082	8104 8105	22 10	243 132	240 125	240 125	-10 -6	16 11	-8 -10
7082 7082	8311	5	39	38	37	-6	11	-10 -1
7082	8312	6	65	65	65	-5	11	-3
7082	8401	4	33	33	27	-12	14	-9
7084	7802	8	55	55	55	-3	50	8
7084	7803 7803	1 <b>4</b> 21	162 196	127 162	127 162	28 -14	38 30	15 -8
7085 7085	7803 7804	2	3	3	3	12	30 20	2
7086	7909	ī	22	22	22	-21	24	-10
7086	7910	19	236	228	228	0	13	1
7086	7911	24	305	301	301	3	16	2
7086 7086	7912 8001	32 26	379 284	377 283	377 283	1 4	12 10	1 2
7086	8002	27	394	263 387	387	-1	9	-3
7086	8003	24	340	322	321	- <u>2</u>	8	-3 -3
7086	8004	18	305	296	296	8	15	7
7086	8005	8	108	108	108	5	10	6
7086 7086	8007 8008	8 9	52 87	52 73	52 72	-9 -13	13 14	-11 -12
7086	8209	7	79	73	72	-13	14	-12
7086	8210	11	68	61	58	-7	22	
7086	8211	6	41	40	40	-7	14	-5
7086	8212	19	168	136	136	-11	15	0
7086 7086	8301 8302	21 16	93 99	68 95	67 95	-13 0	16 12	-15 -2
7086	8303	11	132	32 32	32 32	- <b>4</b>	13	- <u>7</u> -4
7086	8304	18	185	124	124	11	16	10
7086	8305	7	55	40	39	17	27	5
7086	8306	5	39	39 ~~	39	4	17	9
7086 7086	8307 8309	3 10	37 129	37 62	37 62	3 -1	11 9	13
7086	8310	3	42	42	42	-1 -5	7	-3 -5
7086	8311	20	258	135	133	2	9	2
7086	8312	13	157	153	152	0	19	1
7086	8401	4	41	41	41	1	8	0
7086 7086	8402 8403	3 4	35 53	15 47	15 <b>4</b> 7	1 -11	6 13	3 -11
7086	8404	16	150	147	146	-11 -1	12	0
7086	8405	14	165	142	139	-8	12	-6
7086	8406	10	99					
7086	8407	21	264	248	246	-9	13	-8
7086	8408	12	145	140	120	0	10	4
7086 7086	840 <del>9</del> 8410	12 5	153 66	140 63	139 63	0 -3	10 9	-6 -1
7086	8411	5	70	65	65	7	11	7
7086	8412	8	139	126	126	1	9	4
7086	8501	4	54	54	54	-5	9	-5
7086	8502	11	1 <i>7</i> 1	122	121	-1	17 127	-2
7086 7086	8503 8504	4 11	43 145	43	36	-7	137	6
7086 7086	850 <del>4</del> 8505	12	155					
7086	8506	10	134	132	132	1	11	-2 -3
7086	8507	22	354	346	346	4	9	-3

Station	_	No. of	Observ.	Obs. after	Obs. after	Mean Residual	RMS of Residual	Bias Estimate
Number	Date	Passes	Acquired	Engr. Edit	Dynam. Edit	(cm)	(cm)	(cm)
7086	8508	31	385	380	380	-2	15 12	-2 3
7086	8509	20	192	186	186 321	0 3	13 13	2
7086	8510 8511	26 37	340 551	321 537	537	-1	9	0
7086 7086	8512	41	604	5 <del>69</del>	5 <del>69</del>	0	5	0
7086	8601	44	647	629	629	1	6	0
7086	8602	41	584	573	573 500	-1 -3	9 9	-3 -3
7086	8603	41	538 138	503 125	502 125	-3 -3	ģ	-6
7086 7086	8604 8605	10 <b>23</b>	128 271	240	240	Ö	7	
7086	8606	4	61	54	54	-1	9	-1
7086	8607	7	99	83	83	-13 10	17 12	-3
7086	8608	3	33 100	33 91	33 91	10 -5	11	-5
7086	8609 8610	9 3	109 51	30	17	-23	26	-10
7086 7086	8610	3	51	20	20	-6	7	
7086	8611	21	299	287	287	-3 -5	8	2
7086	8612	16	232	202	194 165	-5 3	12 8	2 -1
7086	8701 8702	20 22	253 273	165 267	264	-8	17	-2 -3
7086 7086	8702 8703	40	594	496	489	-4	9	-3
7086	8704	31	452	429	429	-6	11	-4 -6
7086	8704	-		105	188	-4	11	-0 -3
7086	8705	18 ~	214 322	195 291	285	-3	7	-4
7086 7086	8706 8707	22 33	412	396	393	-8	10	-7
7086	8708	17	212	212	212	-6	8	-7
7086	8709	15	195	168	157	.9 .5	12 7	-6 -6
7086	8710	38	544	429 392	427 392	-3 -6	9	-6
7086 7086	8711 8712	35 49	461 567	270	270	<b>-</b> 4	7	-4
7086	8801	27	349	25 <del>9</del>	259	-4	8	-3
7086	8802	3	30	29	26	0 0	15 14	-4 4
7090	7910	13	91 95	89 94	89 94	-1	14	Õ
7090 70 <del>9</del> 0	7912 8001	8 15	227	227	227	i	10	0
7090	8002	48	649	640	639	-1	11	1
7090	8003	47	675	673	672	1	8 8	3
7090	8004	37	545 468	545 468	544 468	2 2	9	3 5
7090 7090	8005 8006	32 27	435	435	434	4	10	4
70 <del>9</del> 0	8007		7 <del>69</del>	<b>76</b> 0	<b>7</b> 58	0	8	4
<b>709</b> 0	8008	56	946	946	944	0	7 8	<b>4</b> 5
7090	8009	62 50	880 876	878 876	877 875	2 2	10	7
7090 7090	8010 8011	59 42	611	601	601	2 2 4	13	7 7 6
7090 7090	8012	28	442	441	440	4	12	6 7
7090	8101	31 52 38 27	405	405	404 822	3 2 -2 -3 -1	13 14	4
7090	8102 8103	52 39	822 539	822 539	538	-2	10	1
7090 7090	8104	27	377	376	376	-3	16	-3
<b>709</b> 0	8105	38	5 <del>59</del>	549	548	-1	12	1
7090	8106	38 50	589 402	563 691	562 691	0 -3	8 12	1 2 -3
7090 7090	8107 8108	50 32	693 401	691 401	400	-3 -1	9	0
7090 7090	8109	48	<i>77</i> 0	<b>76</b> 5	763	-1 -2 -2 -3	10	0
<b>709</b> 0	8110	66	962	950	950	-2	9 <b>1</b> 1	-1 -2
7090	8111	40	654	649 973	647 971	-3 -1	13	-3
7090 7090	8112 8201	64 60	1007 941	973 938	937	- <b>2</b>	10	-2 -3 -3 -4 -2 -3
7090 7090	8201 8202	61	9 <del>69</del>	9 <del>69</del>	967	-2 -6 -2 5	53	-4
7090	8203	49	<b>786</b>	<b>786</b>	784	-2	12	-2
7090 7090	8204	9	150	150	150 273	.5 _a	19 11	.3 -3
7090	8205	27 21	404 302	374 214	373 212	-3 -4	11	Ű
7000	8206	21 23	302 429	425	424	-3	8	-2
7090 7090	8207	74	429	124				
7090	8207	26	<b>47</b> 3	426	426	1	9	-3
7090 7090 7090	8207 8208 8209	26 27	473 487	426 474	426 473	1 1	9 14	-3 2 2
7090	8207 8208	26	<b>47</b> 3	426	426	1	9	-2 -3 2 2 -1

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
Number	Date	rasses	Acquired	Eng r. Ean	Dynam. Eun	(cm)	(cm)	(cm)
7090	8212	11	167	166	166	5	11	0
7090	8301	25	427	406	405	2	10	0
7090	8302	16 20	278 514	278 516	277 516	3 2	16 15	3 6
7090 7090	8303 8304	29 24	516 3 <b>%</b>	516 3%	396	2	12	4
70 <del>9</del> 0	8311	22	393	393	393	0	5	1
7090	8312	10	177	177	177	9	19	14
7090	8401	23	363	363	363	-2	5	0
7090	8402	12	235	235	235	-5	9	0
7090	8403	12	155	144	144	-10	16	-4
7090 7090	8404 8405	12 36	194 498	194 491	193 490	-1 0	7 7	-1 1
70 <del>9</del> 0 70 <del>9</del> 0	8406	36	561	532	532	-2	6	1
7090	8407	$\widetilde{\mathbf{z}}$	396	396	396	2	7	ŝ
7090	8408	19	313	310	310	-2	10	-1
7090	8409	38	618	617	617	1	8	3
7090	8410	36	632	632	632	-2	7	0
7090	8411	29	437	349	349	-1	7	0
7090 7090	8411 8412	32	444	88 439	88 438	0 0	4 7	1 2
7090	8501	32 39	571	571	568	0	37	3
7090	8503	64	893	893	892	ő	8	ŏ
7090	8504	58	821	821	821	Ō	8	1
7090	8505	54	<i>7</i> 36	736	<i>7</i> 35	-1	5	1
7090	8506	49	764	764	762	-1	6	1
7090	8507	29	432	432	429	-1	9	1
7090 7090	8508 8509	32 39	504 645	494 162	494 159	0 -1	12 19	-1 <i>-7</i>
7090	8509	<i>39</i>	040	483	483	0	10	3
7090	8510	36	517	517	513	-1	18	1
7090	8511	30	326	326	311	-3	16	1
7090	8512	29	348	348	340	1	8	2
7090	8601	34	494	494	481	-1	10	0
7090	8602	25 26	406	404 500	401 500	-5	13	1
7090 7090	8603 8604	36 44	519 637	503 628	502 619	4 3	11 10	4 3
7090	8605	27	454	300	294	1	7	3
7090	8606	<u>-</u> 35	566	345	344	2	8	3
7090	8607	21	340	262	260	-1	10	
7090	8608	31	50 <del>9</del>	3 <i>7</i> 3	372	-1	6	7
7090	8609	20	328	320	313	-1	9	
7090 7090	8610 8611	28 21	487 274	465 232	459 231	0 4	7 7	4
<b>709</b> 0	8612	23	389	312	308	2	7	4
7090	8701	24	430	404	404	-2	11	2
7090	8702	25	452	452	451	-2	12	4
7090	8703	13	256	128	127	1	5	4
7090	8704	10	181	129	129	-1	4	3
7090 7090	8705 8706	21 4	306 42	254 38	254 34	-7 -1	11 13	-1 -1
7090	8707	12	173	165	165	-1 -2	7	1
7090	8708	2	35	35	23	<u>-</u> 9	19	-7
7090	8709	13	245	244	233	-5	13	-1
7090	8710	15	276	132	80	13	24	19
7090	8711	31	486	300	295	1	9	9
7090 7090	8712 8801	18 25	348 442	270 377	270 376	1 -2	7 8	3 4
70 <del>9</del> 0 70 <del>9</del> 0	8802	32 32	528	324	319	0	9	2
7090	8803	22	367	276	256	2	8	4
7090	8804	13	231	194	194	-3	5	-1
7090	8805	12	154	128	128	-2	5	0
7090	8806	17	202	186	172	-1	8	1
7090	8807	23	424	372	325	-3	17	2
7090 7090	8808 8809	15	237	168	168	-1	5	2
7090 7090	8809 8810	9 18	118 230	33 61	31 52	4 -7	10 14	1 0
7090	8811	25	419	243	32 240	- <i>/</i> -1	12	-2
7090	8812	24	410	249	234	-5	12	-2 -1
7090	8901	16	194	108	108	-5	9	-5

7090 8903 25 445 410 10 0 8 2 4 7090 8906 8906 29 4 327 21 11 8 4 4 11 11 11 10 10 6 11 4 1 8 5 1 7090 8906 31 571 195 11 11 10 10 6 11 4 1 8 5 1 7090 8906 31 571 195 11 10 10 9 6 11 4 3 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
7,700	Mulliber	Date	1 40000				(cm)	(cm)	(cm)
7,700	····						_	•	2
7,000	7090	8903	25		410				4
1,000   1,00							-		و۔
100   100								9	11
7090 9809 21 337 226 211 -3 8 8 -1 7090 98010 21 367 367 367 367 367 367 367 367 367 367								14	-3
7090 9809 21 337 226 211 -3 8 8 -1 7090 98010 21 367 367 367 367 367 367 367 367 367 367					195	181			-5
7090 8909 21 337 226 211 3 3 8 3 7 7090 8910 21 367 367 330 4 8 8 3 7 7090 8911 226 476 404 383 4 6 127 2 4 4 7090 8912 26 476 404 383 4 6 127 2 4 4 7090 8912 26 476 404 383 4 6 127 2 4 4 7090 900 9001 23 403 403 403 361 3 8 0 0 7090 9002 23 369 368 408 408 361 3 8 0 0 7090 9002 25 3 369 368 408 408 1 3 18 0 1 1 1 1 8 0 0 7090 9002 25 3 369 368 408 408 1 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1					22	22			-23
7990 8910 21 367 367 367 397 4 8 1 7 7990 8911 228 521 484 407 2.2 8 1 7 7990 8912 26 476 404 383 4 4 17 2.2 4 7 7990 9001 23 404 404 383 4 4 17 2.2 7 7990 9001 23 404 404 383 4 4 17 2.2 7 7990 9001 25 408 408 408 384 4 1 17 2.2 7 7990 9001 25 408 408 408 384 4 1 17 2.2 7 7 7 1990 9003 25 478 478 478 478 478 4 18 1 8 0 0 7 7 1 16 5 5 1 16 5 1	7090				226				-1 2
April	7090		21				-4 2		1
7,990 9010 22 349 361 361 36 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0									4
7,000 9002 22 349 361 361 36 3 8 0 0 7000 9003 25 478 478 478 44 9 0 0 7000 9004 13 224 224 228 218 -1 16 5 5 7000 9005 16 224 224 224 228 -1 16 5 5 7000 9005 16 224 224 228 218 -1 16 5 5 7000 9005 15 220 219 219 22 11 3 3 15 7000 9006 15 220 219 219 22 11 3 2 2 11 3 2 2 1 1 1 1 1 1 1 1 1			26 22			354	-4	17	-2
7090 9003 25 478 478 478 478 478 478 478 478 9 0 0 7090 9004 13 224 218 218 1-1 8 8 0 0 7090 9005 16 224 219 218 218 1-1 8 8 0 0 7090 9006 15 220 219 219 2 111 3 3 7090 9006 15 220 219 219 2 111 3 3 7090 9006 15 220 219 219 22 111 3 3 7090 9006 15 220 219 219 22 111 3 3 7090 9007 8 13 219 219 218 2 10 1 7090 9008 13 219 219 218 2 10 1 7090 9008 13 219 229 228 2 20 4 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7							-3		
7090         9004         13         224         218         218         -1         6         5           7090         9005         16         244         244         243         -1         16         5           7090         9006         15         220         219         219         2         11         3           7090         900         8         130         130         128         3         15           7090         900         20         374         374         366         -2         111           7090         9011         23         650         650         648         3         12           7090         9011         33         650         650         648         3         12           7091         790         9011         36         425         425         40         757           7091         790         9012         19         292         292         292         290         4         12         25         8           7091         780         5         8         56         56         52         24         32         19 <t< td=""><td></td><td>9003</td><td>25</td><td></td><td></td><td>478</td><td></td><td></td><td>0</td></t<>		9003	25			478			0
7090 9005 16 244 244 243 -1 18 3 7090 9006 15 220 219 219 2 11 3 3 7090 9006 15 5220 219 219 2 11 1 3 3 7090 9006 15 5200 219 229 2 11 1 3 3 7090 9008 13 219 219 218 2 110 1 9 7090 9008 13 219 219 218 2 110 1 9 7090 9008 13 219 219 218 2 110 1 9 7090 9008 13 219 219 218 2 110 1 9 7090 9010 24 435 435 425 40 757 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7									ō
7090 9007 8 130 120 128 3 15   7090 9008 13 219 219 218 2 10   7090 9009 20 374 374 374 366 -2 11   7090 9010 24 435 435 435 425 40 757   7090 9011 33 650 668 3 12   7090 9011 33 650 668 3 12   7091 7802 10 62 62 62 62 121 3 13 13 29   7091 7803 20 137 121 121 121 3 13 13 29   7091 7804 5 5 88 56 56 56   7091 7908 2 12 2 12 12 13 3 17 7 19   7091 7909 16 167 199 199 139 5 1 17 19   7091 7909 16 167 199 199 139 15 10 27   7091 7910 27 391 358 333 5 20 32   7091 7910 27 391 358 333 5 20 32   7091 7911 26 429 411 411 41 4 20 23   7091 7911 26 429 411 418 11 4 4 20 23   7091 7091 8001 22 309 302 303   7091 8002 42 554 482 482 2 1 13 29   7091 8004 6 25 25 25 25 0 16 29   7091 8004 6 25 25 25 25 0 16 29   7091 8006 3 11 148 125 122 10 21   7091 8006 4 52 25 25 25 0 16 29   7091 8006 4 52 25 25 25 25 0 16 29   7091 8006 4 52 25 25 25 0 16 29   7091 8006 4 52 25 25 25 25 0 16 29   7091 8006 4 52 25 25 25 25 0 16 29   7091 8006 4 52 25 25 25 25 0 10 21 40   7091 8006 13 179 170 170 120 29   7091 8007 10 105 82 82 0 0 10 29   7091 8009 46 461 305 305 44 10 20   7091 8009 77 10 105 82 82 0 0 10 29   7091 8009 12 12 12 12 12 12 12 12 13 33   7091 8009 13 179 170 170 170 170 170 170 170 170 170 170			16						3
7,900 900,8 13 319 219 218 2 10 77090 9009 20 3374 374 366 -2 11 1 97090 9010 24 435 435 445 445 445 445 425 420 757 7090 9011 33 680 660 648 3 112 9009 9011 31 91 292 292 292 290 -6 16 16 7091 7800 1 10 62 62 62 62 -12 25 8 8 7091 7804 5 20 137 121 121 -3 13 29 199 7091 7804 5 28 2 22 22 22 23 3 17 7 51 7091 7909 16 16 167 159 159 159 15 17 32 7091 7909 16 16 167 159 159 159 15 17 32 7091 7910 27 391 388 353 5 20 32 7091 7911 26 429 4411 4411 44 20 23 7091 7912 21 339 303 303 313 -1 21 22 23 7091 7912 21 339 303 302 302 -1 133 25 7091 8001 22 309 302 302 302 -1 133 25 7091 8002 42 554 4482 482 482 2 1 13 25 7091 8004 6 6 25 125 122 100 21 40 7091 8006 3 3 21 148 125 122 100 21 40 7091 8006 3 3 21 19 19 19 28 34 45 56 7091 8006 3 3 21 19 19 19 28 34 56 7091 8006 3 3 21 19 19 19 28 34 56 7091 8006 3 3 21 19 19 19 28 34 56 7091 8006 3 3 21 19 19 19 28 34 56 7091 8006 3 3 21 19 19 19 28 34 56 7091 8006 3 3 21 19 19 19 28 34 56 7091 8006 3 3 21 19 19 19 28 34 56 7091 8006 13 179 177 126 126 127 100 21 40 7091 8006 3 3 21 19 19 19 28 34 56 7091 8006 13 179 177 126 126 127 170 18 800 10 37 531 505 504 -2 116 33 7091 8011 21 280 280 280 280 -1 1 16 29 7091 8006 13 179 177 126 126 126 -15 19 19 19 28 34 56 7091 8006 13 179 177 126 126 126 -15 19 19 19 7091 8006 13 179 177 126 126 126 -15 19 19 19 7091 8006 13 179 177 126 126 126 -15 19 13 7091 8006 13 179 177 126 126 126 -15 19 13 7091 8006 11 144 143 143 143 13 3 3 11 144 143 144 143 144 144	7090								3
7090 9009 20 374 336 425 40 757 7090 9010 24 435 435 435 425 40 757 7090 9011 33 4650 650 648 40 312 7090 9011 33 4650 650 648 40 40 757 7090 9011 30 40 40 40 40 40 40 40 40 40 40 40 40 40									
7,090 9010 24 435 425 40 757 7090 9011 33 650 650 689 3 12 7090 9012 19 292 292 292 492 62 7091 7803 20 137 121 121 121 3 13 13 29 7091 7804 5 56 56 56 56 24 32 19 7091 7908 2 2 27 27 2 2 2 2 3 17 7091 7908 2 2 27 2 2 2 2 2 2 3 17 7091 7908 2 2 27 2 2 2 2 2 3 17 7091 7909 16 16 76 159 159 5 17 7091 7910 27 391 388 353 5 20 32 7091 7911 26 429 411 411 411 4 4 20 2 2 7091 7912 21 333 333 333 -1 21 22 7091 7912 21 333 333 333 -1 21 22 7091 8001 22 309 302 302 302 -1 13 25 7091 8001 12 309 302 302 302 302 302 302 302 302 302 303 303									
7090 9011 33 650 650 648 3 12 7090 9012 19 292 292 290 6 16 7091 7802 10 157 121 121 121 3 13 29 7091 7803 20 157 121 121 121 3 13 29 7091 7804 5 5 26 6 26 24 32 19 7091 7908 2 72 22 22 22 3 177 51 7091 7909 16 16 167 159 159 5 177 32 7091 7910 27 391 358 353 5 20 7091 7911 26 429 411 411 4 4 20 23 7091 7912 21 333 333 333 333 -1 21 28 7091 7912 21 333 333 333 333 -1 12 28 7091 8001 22 309 302 42 11 13 25 7091 8002 42 554 482 482 2 1 13 25 7091 8003 11 148 125 122 10 21 0 21 7091 8004 6 25 25 25 25 25 0 16 29 7091 8005 3 2 11 148 125 122 10 21 0 21 7091 8006 4 5 2 5 2 5 2 5 2 0 0 10 7091 8006 3 179 170 105 82 82 82 0 0 10 7091 8009 27 366 349 349 2 14 33 7091 8010 27 366 349 349 2 14 33 7091 8010 37 531 505 504 2 11 16 24 7091 8010 37 531 505 504 2 11 16 24 7091 8010 37 531 505 504 2 11 16 24 7091 8010 37 531 505 504 2 11 16 24 7091 8010 37 531 505 504 2 11 16 24 7091 8010 37 531 505 504 2 11 16 24 7091 8010 37 531 505 504 2 11 16 24 7091 8010 17 177 126 126 126 115 19 7091 8010 37 531 505 504 2 11 16 24 7091 8010 37 531 505 504 2 11 16 24 7091 8010 37 531 505 504 2 11 16 24 7091 8010 17 177 126 126 126 115 19 7091 9010 9 12 8 122 122 122 10 12 11 14 14 14 14 14 14 14 14 14 14 14 14						425	-40		
70000         9012         19         292         292         290         6         16         8           7091         7802         10         62         62         62         -12         12         25         8           7091         7803         20         137         121         121         121         3         13         29           7091         7804         5         58         56         56         52         24         32         19           7091         7908         16         167         159         159         5         17         30           7091         7911         26         429         411         411         4         20         32           7091         7911         26         429         411         411         4         20         23           7091         8001         22         309         302         302         302         11         13         25           7091         8001         22         309         302         302         11         13         25           7091         8002         42         254         482	7090 7090					648		12	
7091   7802   10	7090		19		292			16	٥
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7092         8011         1         14         14         14         13         24         7           7096         7908         3         26         24         24         -20         25         -23           7096         7909         2         14         14         14         -23         25         -15           7096         7910         7         73         71         71         -13         17         -13           7096         7911         6         51         50         50         -24         27         -18           7096         7912         6         94         93         91         2         34         -11           7096         8002         5         45         44         44         -10         19         -9           7096         8003         20         231         208         208         4         16         -5           7096         8004         11         143         143         143         6         14         7           7096         8005         5         59         54         54         1         13         4	7092	8009			120		-3	17	0
7092         8011         1         14         14         14         13         24         7           7096         7908         3         26         24         24         -20         25         -23           7096         7909         2         14         14         14         -23         25         -15           7096         7910         7         73         71         71         -13         17         -13           7096         7911         6         51         50         50         -24         27         -18           7096         7912         6         94         93         91         2         34         -11           7096         8002         5         45         44         44         -10         19         -9           7096         8003         20         231         208         208         4         16         -5           7096         8004         11         143         143         143         6         14         7           7096         8004         11         122         122         122         5         14         1	7092			122	109	107	8	18	10
7096         7908         3         26         24         24         -20         25         -15           7096         7909         2         14         14         14         -23         25         -15           7096         7910         7         73         71         71         -13         17         -13           7096         7911         6         51         50         50         -24         27         -18           7096         7912         6         94         93         91         2         34         -11           7096         8002         5         45         44         44         -10         19         -9           7096         8003         20         231         208         208         4         16         -5           7096         8004         11         143         143         143         6         14         7           7096         8005         5         59         54         54         1         13         4           7096         8006         11         122         122         122         5         14         1	7092	8011	1	14	14		13	24 25	.22
7096 7910 7 73 71 71 -13 17 -13 7096 7911 6 51 50 50 -24 27 -18 7096 7912 6 94 93 91 2 34 -11 7096 8002 5 45 44 44 -10 19 -9 7096 8003 20 231 208 208 4 16 -5 7096 8004 11 143 143 143 163 6 14 7 7096 8005 5 59 54 54 1 13 4 7096 8006 11 122 122 122 5 14 1 7096 8007 12 107 101 101 13 21 9 7096 8008 11 106 105 105 4 16 2 7096 8009 6 62 58 57 -6 15 -6 7096 8009 6 62 58 57 -6	7096	7908					-2U 22	25 25	-23 -15
7096 7911 6 51 50 50 -24 27 -18 7096 7912 6 94 93 91 2 34 -11 7096 8002 5 45 44 44 -10 19 -9 7096 8003 20 231 208 208 -4 16 -5 7096 8004 11 143 143 143 143 6 14 7 7096 8005 5 59 54 54 1 133 4 7096 8006 11 122 122 122 5 14 1 7096 8007 12 107 101 101 13 21 9 7096 8008 11 106 105 105 4 16 2 7096 8009 6 6 62 58 57 -6 15 -6 7096 8010 13 129 127 127 0 9 9 1	7096	7909	2	14			-23 -13	17	-13
7096 7912 6 94 93 91 2 34 -11 7096 8002 5 45 44 44 -10 19 -9 7096 8003 20 231 208 208 -4 16 -5 7096 8004 11 143 143 143 6 14 7 7096 8005 5 59 54 54 1 13 4 7096 8006 11 122 122 122 5 14 1 7096 8007 12 107 101 101 13 21 9 7096 8008 11 106 105 105 4 16 2 7096 8009 6 62 58 57 -6 15 -6 7096 8010 13 129 127 127 0 9 9 1	7096			<i>/3</i> 51	71 50		-24	27	-18
7096 8002 5 45 44 44 -10 19 -9 7096 8003 20 231 208 208 -4 16 -5 7096 8004 11 143 143 143 6 14 7 7096 8005 5 59 54 54 1 133 4 7096 8006 11 122 122 122 5 14 1 7096 8007 12 107 101 101 13 21 9 7096 8008 11 106 105 105 4 16 2 7096 8009 6 62 58 57 -6 15 -6 7096 8010 13 129 127 127 0 9 9 1	7096 7096	7911 7912		94		91	2	34	-11
7096 8006 11 122 122 5 14 1 7096 8007 12 107 101 101 13 21 9 7096 8008 11 106 105 105 4 16 2 7096 8009 6 62 58 57 -6 15 -6 7096 8010 13 129 127 127 0 9 1 1	7096		5	45	44	44	-10		-9
7096 8006 11 122 122 5 14 1 7096 8007 12 107 101 101 13 21 9 7096 8008 11 106 105 105 4 16 2 7096 8009 6 62 58 57 -6 15 -6 7096 8010 13 129 127 127 0 9 1 1	7096	8003		231	208	208	-4		-5
7096 8006 11 122 122 5 14 1 7096 8007 12 107 101 101 13 21 9 7096 8008 11 106 105 105 4 16 2 7096 8009 6 62 58 57 -6 15 -6 7096 8010 13 129 127 127 0 9 1 1	7096	8004	11	143	143	143			/ A
7096 8007 12 107 101 101 13 21 9 7096 8008 11 106 105 105 4 16 2 7096 8009 6 62 58 57 -6 15 -6 7096 8010 13 129 127 127 0 9 1	7096	8005	5	59 100					
7096 8009 6 6 2 30 127 127 0 9 1 7096 8010 13 129 127 127 0 9 1 1 17 4	7096	8006		122 107		101	13		ģ
7096 8009 6 6 2 30 127 127 0 9 1 7096 8010 13 129 127 127 0 9 1 1 17 4	7096	8007				105			2
7096 8010 13 129 127 127 0 9 1 7096 8010 13 129 127 127 0 177 4	7096 7004	BUUB RAAD		62 62	58	57	-6	15	
7090 0010 10 17 1	7096	8010		129		127	0	9	
7070 0011	70 <del>9</del> 6	8011	9	94		94	10	17	4

Station	ъ.	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng r. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
						(CIII)	(CIII)	(CIII)
7097	8711	3	42	30	29	1	10	13
7097	8712	21	270	201	172	-14	17	-4
7097 7097	8801 8802	10 18	149 273	121 260	121 2 <b>44</b>	-9 -11	11 1 <b>4</b>	2 -2
7097	8810	2	15					
7097 7097	8811 8812	4 4	56 38	4 <u>2</u> 17	42 17	-23 -25	35 89	-6 12
7097	8901	12	36 157	17 1 <b>44</b>	143	-25 -1	28	13 1
7097	8902	14	190	191	191	-16	32	-9
7097 7097	8903 8910	15 2	192 28	190 63	190 63	-8 -9	17 12	0 -1
7097	8911	8	93	93	93	-15	30	-5
7097 7097	8912 9001	10 17	132 184	132 184	132 181	-11 12	15	1
7097	9002	19	227	226	226	-12 -14	64 26	- <u>4</u> -17
7097	9012	11	138	138	138	-15	17	
7100 7100	<i>77</i> 10 <i>7</i> 711	4 1	36 17	36 17	36 17	-46 -39	52 44	-64 -47
7101	7902	3	29	26	26	-17	22	-24
7101	7903 8205	5	53	52 1	52 16	-19	24	-45
7101 7101	8205 8206	1	16	16	16	13	16	-1 0
7102	7903	9	128	123	123	2	20	ŏ
7102 7102	7904 7911	2 15	21 170	21 156	21 156	18 20	20 32	1 23
7102	7912	20	279	251	244	15	31	21
7102	8001	4	29 16	14	13	-6	21	-7
7102 7102	8002 8003	2 19	16 288	16 239	13 238	3 -4	41 13	-1 -1
7102	8004	14	223	223	223	-9	16	-11
7102 7102	8006 8007	1 3	14 14	14 10	14 10	-5 3	7 5	2 0
7102	8009	8	110	99	99	6	13	9
7102	8010	16	139	134	134	-3	15	-1
7102 7102	8011 8012	2 1	8 2	8 2	8 2	11 -3	16 <b>4</b>	-39 13
7102	8101	3	25	25	25	-33	40	<b>-4</b> 5
7102 7102	8102 8103	1 4	9 29	9 29	9 27	19 -18	26 73	14
7102	8104	2	15	25	D	-10	/3	3
7102	8106	1	6	6	6	16	20	6
7102 7102	8107 8108	3 2	36 17	36 17	36 17	-2 1	19 9	-3 3
7102	8109	7	86	85	85	-21	24	-18
7102 7102	8110 8111	18 3	256 25	256 25	256 25	-2 -1	5 9	-1 10
7102	8201	5	35	33	33	-1 -1	5	10 2
7102	8202	4	25	25	20	8	408	1
7102 7102	8203 8204	7 14	86 235	86 235	82 234	17 -3	162 13	7 3
7102	8209	2	30	26	24	13	20	3
7102 7102	8210 8211	5	<b>7</b> 5	72	72	3	11	16
7102	8305	6	101	101	101	-31	32	6 -29
7102	8306	26	294	286	286	6	16	5
7103 7103	7902 7903	3 8	16 102	13 50	13 50	1 0	14 26	-6 -11
7103	7904	7	94	87	90 87	6	17	-3
7103	8208	5	30	28	27	7	15	
7103 7103	8209 8210	5 32	35 566	35 541	35 540	0 -2	10 12	5 4
7103	8211							-1
7104 7104	7902 7904	1 10	17 136	16 134	16 134	7 -3	18 14	1 <b>4</b> -5
7104	790 <del>1</del> 7905	2	130	134	134	-3 2	20	-5 -12
7105	8103	29	466	466	466	5	14	6
7105 7105	8107 8108	10 15	1 <del>69</del> 217	1 <del>69</del> 217	1 <del>69</del> 217	-3 -1	8 5	-2 -4
7105	8109	23	323	323	323	-1 -1	8	- <del>1</del> -1
7105	8110	15	1 <i>7</i> 7	1 <b>7</b> 7	177	0	5	-1

Station	_	No. of	Observ.	Obs. after	Obs. after	Mean Residual	RMS of Residual	Bias Estimate
Number	Date	Passes	Acquired	Eng r. Edit	Dynam. Edit	(cm)	(cm)	(cm)
	<del></del>					, , , , , , , , , , , , , , , , , , ,		
7105	8111	4	29	29	29	-2	7	7
7105	8112	1	19	19	19	14	15	13
7105	8201	8	116	116	116	3 0	8 12	2 6
7105	8202	19	242 218	242 218	240 218	2	10	7
7105 7105	8203 8204	14 14	220	220	219	ō	13	3
7105 7105	8205	15	235	235	232	1	14	4
7105	8206	7	133	133	132	-1	7 7	0
7105	8207	22	369	369 227	367 337	0 0	7	1
7105	8208 8209	22 22	357 288	337 288	287	2	8	2
7105 7105	8210	32	484	484	484	1	12	5
7105	8211	$\widetilde{\mathbf{z}}$	3 <del>69</del>	3 <del>69</del>	3 <del>69</del>	<u>o</u>	11	2 -1
7105	8212	13	140	138	136	-7 2	133 6	-1 -3
7105	8301	9	140	140 30	140 30	2 -10	11	-3 -3
7105	8302	3 11	30 121	30 70	30 70	-10 -2	6	-3
7105 7105	8303 8304	17	251	215	212	0	8	-4
7105	8305	20	279	278	278	-1	13	0
7105	8306	18	221	183	183	-1	15 8	1 5
7105	8309	16	231	229 438	228 438	3 2	7	3
7105	8310	26 20	438 320	436 319	319	1	4	3
7105 7105	8311 8312	16	226	226	226	0	8	6
7105	8401	13	200	200	200	4	8	3 7
7105	8402	8	151	150	150	1 1	6 7	-4
7105	8403	7	131	89 42	89 42	-3	4	1
7105 7105	8403 8404	13	158	158	158	4	8	3
7105 7105	8405	41	602	588	587	-1	6	0
7105	8406	16	294	294	293	1 -6	4 7	0 0
7105	8407	11	175	1 <i>7</i> 3 312	173 312	-0 -4	8	-1
7105 7105	8408 8409	21 19	313 289	289	289	-2	7	-1
7105 7105	8410	7	64	64	64	0	3	0
7105	8411	10	181	181	181	-4	8	2 3
7105	8412	13	195	192 78	192 78	4 3	9 6	1
7105	8501	7 20	<i>7</i> 8 264	78 258	258	2	5	1
7105 7105	8502 8503	31	452	450	449	-3	6	3
7105	8504	26	408	408	408	2	9	1 1
7105	8505	22	354	330	330 24	0 -2	5 2	1
7105	8505	35	486	24 486	481	3	13	2
7105 7105	8506 8507	35 31	481	449	449	0	6	1
7105	8507	<b>31</b>		32	32	8	11	1
7105	8508	23	377	377	377	1 1	9 10	1 3
7105	8509	35 15	560 180	554 180	554 180	2	6	1
7105 7105	8510 8511	15 11	152	152	152	2	9	2
7105	8512	23	281	281	281	3	5	3
<b>7</b> 105	8601	23	294	294	294	3 1	6 6	2 0
7105	8602	6	<b>49</b> 1 <b>4</b> 5	48 139	48 139	2	8	4
7105 7105	8603 8604	14 19	263	263	262	4	9	2
7105 7105	8605	33	435	385	385	0	5	_
7105	8606	29	322	186	186	1	7 5	-1
7105	8607	7	80	39 87	38 87	3 -1	5 5	-1
7105	8608	14 14	101 156	8/ 155	67 155	3	7	
7105 7105	8609 8610	20	248	230	230	2	7	0
7105	8611	38	552	542	541	1	6	1
7105	8612	23	412	293	293	1 -2	5 9	1
7105	8612	~	214	<i>7</i> 9 300	79 300	-2 - <b>4</b>	10	-2
7105	8701 8702	22 22	316 383	383	383	-2	10	1
7105		20	466	429	428	0	7	1
7105 7105	8703	30						_
7105	8703 8704	30 19	307	291	291	-2	6	1
7105 7105 7105 7105 7105 7105	8703 8704 8705 8706	19 34 21				-2 0 -1	6 8 7	1 1 0

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
Number	Date	rasses	Acquired	Eng 1. Eun	Dynam. Eur	(cm)	(cm)	(cm)
7105	8707	30	401	396	395	0	5 5	0
7105 7105	8708 8708	26	393	376	376	1	5	0 -1
7105	8709	20	291	291	291	-1	5	0
7105	8710	36 35	5 <b>4</b> 5	519 500	519 500	0	6	-1 -1
7105 7105	8711 8712	35 21	511 <b>29</b> 6	509 289	509 289	0 0	4 7	-1 1
7105	8801	10	139	118	117	7	10	5
7105	8802	12	147	119	119	0	9	1
7105 7105	8803 8804	13 18	144 258	105 242	105 242	3 0	<b>4</b> 5	<b>4</b> 0
7105	8805	7	109	109	109	1	5 5 5	ĭ
7105	8806	19	289	289	289	1	5	1
7105 7105	8807 8808	8 21	114 318	109 280	100 279	-2 1	15 5	0 0
7105	8809	31	519	327	301	Ô	ğ	1
7105	8810	54	836	535	53 <b>4</b>	1	6	0
7105 7105	8811 8812	15 37	21 <b>4</b> 610	1 <i>7</i> 5 511	163 511	-7 -3	14 8	-5 -1
7105	8901	3/ 26	<b>42</b> 1	345	345	-3 -1	6	-1 -1
7105	8901			7	7	-10	14	1
7105	8902	25	360	360	359	-3	10	1
7105 7105	8903 8904	17 27	213 <b>4</b> 55	206 448	206 448	4 -2	7 6	<b>4</b> -1
7105	8905	3	59	59	<del>59</del>	3	12	1
7105	8906	3	12	12	12	3	9	Ó
7105 7105	8907 8908	10 9	152 113	26 65	26 53	0 -16	10 21	-6 1
7105	8909	á	19	15	8	-13	15	6
7105	8910	19	255	1 <del>6</del> 1	161	-3	6	-2
7105 7105	8910 8911	14	202	94 176	82 173	2 2	15 10	-1 6
7105	8912	14	158	147	147	-3	8	ő
7105	9008	2	40	40	40	1	3	
7105 7105	900 <del>9</del> 9010	24 21	380 359	380 359	380 359	-3 -3	6 11	
7105	9011	30	464	464	464	-3 1	11	
7109	8110	15	232	231	231	5	11	6
7109 7109	8111 8201	1 <b>4</b>	6 <b>49</b>	6 31	6 29	18 11	26 32	49 20
7109	8202	3	37	31	2	11	32	20
7109	8203	5	70	70	69	4	17	11
7109 7109	8205 8206	22 29	433 563	421 416	420 407	5 6	13 12	8
7109	8207	18	354	306	294	6	16	7
7109	8208	8	84	84	83	6	8	5
7109 7109	820 <del>9</del> 8210	29 32	5 <b>47</b> 5 <b>31</b>	5 <b>47</b> 531	519 512	0 2	8 1 <b>1</b>	9 6
7109	8211	18	303	303	298	1	10	4
7109	8212	10	148	148	148	4	7	4
7109 7109	8301 8302	21 3	302 45	302 45	302 45	3 -1	6 7	2 -6
7109	8303	6	<del>2</del> 6	<del>2</del> 6	<del>%</del>	4	8	8
7109	8304	16	244	244	244	1	7	2
7109 7109	8305 8306	19 5	268 41	268 39	268 31	3 -27	7 49	3 -4
7109	8307	49	<b>72</b> 0	<i>7</i> 19	718	-2	8	3
7109	8308	50	883	883	877	1	5	0
7109 7109	8309 8310	52 21	889 335	889 335	881 335	0 -1	8 7	1 0
7109	8311	3	26	26	26	1	6	4
7109	8312	5	62	62	62	-1	4	3
7109 7109	8401 8402	18 16	332 307	332 307	330 307	1 -1	5 5	<b>4</b> 6
7109 7109	8402 8403	16 13	307 222	307 222	221	-1 -6	9	1
7109	8404	44	860	860	858	-1	8	4
7109	8405	60 25	1143	1143	1142	0	5	3 2
7109 7109	8406 8407	35 51	619 962	619 959	617 956	-1 -2	6 8	2
/109		~ .			1063	-	-	

Station		No. of	Observ.	Obs. after	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
Number	Date	Passes	Acquired	Eng I. Edit	- Jimin. Buit	(cm)	(cm)	(cm)
						_	•	0
7109	8409	41	816	816	815	-2	8	0 -1
7109	8410	<del>39</del>	662	661	661	-2 -3	6 8	2
7109	8411	7	124	12 <del>4</del>	124 210	-3 -3	7	3
7109	8412	13	210	210 293	293	-1	8	Ō
7109	8501	17	293 234	293 234	234	Ô	5	0
7109	8502	13 17	315	55	55	-5	7	2
7109	8503 8503	17	313	257	257	-1	6	4
7109 7109	8504	24	464	458	458	0	5	2
7109	8505	40	786	781	780	-1	4	2
7109	8506	43	882	882	880	-1	6	2 1
7109	8507	43	802	781	<b>780</b>	-2	8 13	1
7109	8508	45	914	456	456 420	-6 5	1.5 8	3
7109	8508		<b>50</b> /	420 500	420 596	2	12	4
7109	8509	31 25	596	596 449	448	1	7	1
7109	8510	25 25	456 436	436	436	i	7	1
7109	8511	25 25	466	466	465	Ō	4	1
7109 7100	8512 8601	11	159	159	159	-1	7	2
7109 7109	8602	13	248	247	247	-1	9	-1
7109	8603	29	433	433	432	0	10	2
7109	8604	19	319	315	315	-2	9	0
7109	8605	21	341	23	23	-4	6	-5
7109	8606	37	734	628	608	4	11 7	-3
7109	8607	51	945	748	748 542	-3 5	8	4
7109	8608	30	597	544 250	542 357	0	5	•
7109	8609	18	359	35 <del>9</del> 529	525	-1	6	-1
7109	8610	32 23	545 408	408	408	ó	5	
7109	8611 8612	25 14	215	179	179	1	5	3
7109 7109	8701	15	270	270	270	2	6	4
7109 7109	8702	13	215	215	215	3	7	5
7109	8703	20	361	280	279	3	8	3
7109	8704	28	539	286	286	0	6	4 2
7109	8705	27	488	417	417	-2 0	8 6	3
7109	8706	37	673	671	670	-2	7	2
7109	8707	36	613	612 887	612 887	-2 -2	6	<u>-</u>
7109	8708	48	913 501	501	500	-2	7	1
7109	8709	27 32	501 598	565	565	-2	6	0
7109 7100	8710 8711	32 15	222	145	145	-3	7	1
7109 7109	8712	1	6	6	6	-1	2	6
7109	8801	8	121	119	119	-5	9	0
7109	8802	27	519	377	376	1	8	2
7109	8803	28	509 225	454	453	0	7	3
7109	8804	12	225	198	198	2 0	7 5 5	3 3 3
7109	8805	29	526	489	483 457	2	8	2
7109	8806	27	494 604	477 565	519	ō	14	2 1
7109	8807 8808	32 38	722	584	584	-1	5	2 3
7109 7109	8809	44	865	579	561	0	8	3
7109 7109	8810	46	760	561	512	-4	11	-1 6
7109	8811	15	262	173	168	2	12	6
7109	8812	16	295	78 100	<b>78</b>	-2	4	0 0
7109	8812			100	95	-/	11 9	-3
7109	8901	23	419	395	394	-/	8	-3 6
7109	8902	20	314	300 103	300 102	-3	9	1
7109	8903	12	194	78	78	-8	11	-2
7109 7109	8903 8904	35	610	605	605	-3	8	-1
7109 7109	8904 8905	13	202	132	132	-5	9	-9
7109 7109	8906	19	256	118	118	10	26	2
7109	8907	51	907	510	510	-3	10	-1
7109	8908	39	650	386	386	-1	10	1
=-00		6	97	97	90	-2	7	2
7109	8909		· ·					
7109 7109	8910	26	395	418	382	-2 F	11 17	-1 6
7109 7109	8910 8911	26 10	395 147	147	121	0 -4 -2 -7 -7 -2 -3 -8 -3 -5 10 -1 -2 -2 5	17	-1 6 -3
7109 7109 7109	8910 8911 8912	26 10 18	395 147 264	147 264	121 264	-3	17 6	-1 6 -3 6
7109 7109	8910 8911	26 10	395 147	147	121	-2 5 -3 6 -4	17	-2 -1 -9 2 -1 1 2 -1 6 -3 6

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
			w-1			(cm)	(cm)	(cm)
7109	9003	26	4 <del>69</del>	4 <del>69</del>	4 <del>69</del>	5	15	3
7109	9004	2	41	41	41	5 -8	21	3 -3
7109	9005	19	342	342	342	-5	14	1
7109	9006	7 ~	105	105	105	-3 0	7 7	-1
7109 7109	9007 9008	27 6	308 94	308 94	308 94	3	6	
7109 7109	9009	22	393	393	393	-3	7	
7109	9010	17	283	283	283	0	8	
7109	9011	19	239	239	239	-9 0	14	
7109 7110	9012 7601	7 1	37 2	37	37	8	10	
7110	8107	5	36	36	36	-1	16	4
7110	8108	8	58	53	53	12	17	8
7110	8109	27	383	377	374	5	9	7
7110	8110 8111	20 25	292 289	274 268	267 268	12 5	17 13	13 8
7110 7110	8112	16	193	164	164	-3	14	3
7110	8201	6	84	83	83	-1	14	3
7110	8202	9	111	111	111_	0	9	6
7110	8203	2	17	17	17	18	31 17	24
7110 7110	8204 8205	3 13	30 171	30 164	30 164	5 - <b>4</b>	17 12	6 -1
7110	8206	12	159	129	129	-2	7	•
7110	8207	29	331	330	324	0	8	-1
7110	8208	6	74 160	64	63	-3	16	-1
7110 7110	8209 8210	20 53	168 677	168 663	166 654	-11 -6	57 12	2 -3
7110	8211	24	301	301	298	-1	14	-3 - <b>4</b>
7110	8212	34	427	427	424	-2	6	-1
7110	8301	21	282	282	281	-3	7	-5 3
7110 7110	8302 8303	9 12	141 193	141 193	141 193	0 0	9 6	3 1
7110	8304	17	311	311	309	-3	8	-2
7110	8305	6	111	111	111	1	16	ō
7110	8306	14	199	185	185	3	12	-1
7110 7110	8307 8310	4 33	48 460	48 458	46 458	-6 4	11 10	3 6
7110	8311	11	166	166	166	2	5	6
7110	8312	12	106	106	106	1	5	0
7110	8401	32	515	515	514	3	6	5
7110 7110	8402 8403	27 25	<b>43</b> 0 337	430 336	430 336	0 -2	7 9	5 3
7110	8404	33	525	486	484	2	10	7
7110	8405	24	361	361	361	-3	7	Ô
7110	8406	49	744	744	743	-1	5	-1
7110	8407	30	374 735	374	374	1	6	2
7110 7110	8408 8409	47 43	735 751	734 750	<i>7</i> 32 748	0 -1	8 8	1 1
7110	8410	28	472	472	470	-1	5	0
7110	8411	25	434	434	434	-2	7	2 5 -2 3
7110	8412	8	137	137	136	2	13	5
7110 7110	8501 8502	15 28	266 449	266 446	265 446	-3 2	6 6	-2 3
7110	8503	24	413	411	410	0	8	6
7110	8504	61	992	989	984	-1	6	0
7110	8505	39	630	628	625	0	5	1
7110 7110	8506 8507	64 47	1108 793	1108 792	1105 <i>7</i> 90	0 -1	5 10	1 1
7110	8508	11	198	198	197	-8	17	
7110	8509	23	414	414	414	0	11	2
7110	8510	7	121	121	121	3	11	2 2 3 2
7110	8511 8512	38 22	631 404	630	6 <b>3</b> 0	4	8	
7110 7110	8512 8601	23 31	404 557	403 557	401 556	0 0	6 6	1 0
7110	8602	22	287	287	287	-2	9	-3
7110	8603	34	528	523	520	3	11	-3 5
7110	8604	34	559	559 205	558 265	-2	6	-2
7110 7110	8605 8606	30 38	398 669	385 567	385 566	0 3	5 8	0
7110	8607	30 29	399	335	335	-3	7	U

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
						(cm)	(cm)	(cm)
7110	8608	7	108	107	107	3	8	4
7110 7110	8609	29	442	435	432	-1	6	
7110	8610	37	615	612	611	1	6	-2
7110	8611	33	522	181	181	3	7	
<i>7</i> 110	8611			341	339	-1	5 <b>7</b>	0
7110	8612	16	225	211	210	-2 6	10	5
7110	8701	15	201	201	201 316	2	9	5
7110	8702	20	317 204	317 202	202	7	12	5 7
7110 7110	8703 8704	14 44	690	599	597	1	7	5
7110	8705	30	462	396	395	1	7	1_
7110	8706	46	661	658	658	2	7	5
7110	8706					_	,	3
7110	8707	53	837	814	807	1 -1	6 5	3 0
7110	8708	47	<i>77</i> 6	<i>77</i> 3	<i>77</i> 3 455	0	6	1
7110	8709	35	457	455 445	445 445	1	5	i
7110	8710 8711	31 22	465 339	314	312	4	8	7
7110	8711 8712	13	157	157	157	6	9	7
7110 7110	8801	13	189	186	186	5	7	8
7110	8802	31	390	286	286	-1	7	1
7110	8803	48	<b>786</b>	<i>7</i> 53	<b>748</b>	0	5	4
7110	8804	24	387	298	297	1	6	1
7110	8804			42	42	0	5 4	3 3
7110	8805	39	660	649 353	649 250	1 1	6	2
7110	8806	35	552	252 289	230 289	i	4	2
7110 7110	8806 8807	44	687	645	606	i	11	2
7110 7110	8808	16	258	237	226	1	5	2
7110	8809	35	597	501	501	2	7	3
7110	8810	56	847	670	642	-1	9	-1
7110	8811	28	503	360	333	0	13	5
7110	8812	22	351	34	34	-1 -7	5 11	-1 0
7110	8812		250	178	178 343	-/	8	-2
7110	8901 8902	22 7	350 120	344 120	120	-6 7	16	10
7110 7110	8903	34	556	502	502	-3	7	2
7110	8904	32	546	546	546	0	7	1
7110	8905	15	218	165	165	-7	11	-13
7110	8906	39	514	317	316	9	15	7 4
<b>7</b> 110	8907	30	508	214	213	<b>4</b> 7	8 11	2
7110	8908	32	484	276 416	274 404	ó	6	1
7110	8909	33 24	444 365	408	357	ĭ	13	Ō
7110 7110	8910 8911	26 41	664	645	619	0	10	5
7110	8912	33	482	472	470	1	9	3 5
7110	9001	32	480	460	451	5	12	5
<b>7</b> 110	9002	39	650	619	618	0	13 15	5 2 9
7110	9003	34	470	465 171	463 168	-1 12	18	9
7110	9004	12	192 634	1 <i>7</i> 1 590	586	7	18	3
7110 7110	9005 9006	41 44	676	6 <b>4</b> 1	636	3	11	3
7110 7110	9007	35	499	499	498	4	11	
7110	9008	23	323	323	323	6	12	
7110	9009	25	422	422	422	1	6	
7110	9010	42	727	727	726	1	10	
7110	9011	35	622	622	619	1	13 11	
7110	9012	19	212	212	211 57	4 -7	12	-8
7112	8103	3 10	57 135	<i>57</i> 135	135	-15	22	-15
7112	8104 8105	10 19	264	264	264	-10	11	-12
7112 7112	8105 8106	12	126	126	126	-6	12	-14
7112 7112	8107	33	309	286	285	-6	67	-6
7112	8108	27	275	211	207	0	126	-8
7112	8109	16	140	134	130	- <u>5</u>	17	-8
7112	8110	15	151	150	150	-7	11	-12
7112	8111	20	214	209	204	-5 -7 5 -7	109	-2 =
7112	8112	5	74 ***	7 <b>4</b>	74 4	-/ -1	13 20	-5 _ <b>∆</b>
7112	8201	10	80 126	<i>6</i> 7 136	66 133	-1 -21	197	-12 -2 -5 -4 -2
7112	8202	11	136	130	133		•	_

Station		No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual	Residual	Estimate
						(cm)	(cm)	(cm)
7112	8203	11	130	130	130	-6	11	-3
7112	8204	13	197	194	194	-3	9	-3 -7
7112	8205	13	168	168	168	-11	14	-11
7112 7112	8206 8207	14 21	224 320	222 319	221 313	-10 -7	12 88	12
7112	8207 8208	21	320 22	21	21	-7 -12	00 14	-13 -12
7112	8209	11	97	95	95	-5	16	-13
7112	8210	35	486	465	<b>465</b>	-2	11	0
7112 7112	8211 8212	30 10	488 131	486 131	485 131	-1 -2	10 8	-1 -4
7112	8301	5	59	59	49	- <del>7</del>	19	-13
7112	8302	5	57	57	57	-12	14	-18
7112 7112	8303 8304	13 5	178 47	171 <b>4</b> 6	170 46	-8 -3	14 8	-1 <b>4</b> -10
7112	8305	2	<b>2</b> 7	27	<b>27</b>	-3 9	24	-10 -7
7112	8306	4	52	52	52	3	15	0
7112 7112	8307 8308	4 2	5 10	7	7		0	7
7112	8309	12	140	110	109	-6 6	9 26	-7 9
7112	8310	15	232	206	205	11	14	6
7112	8311	12	153	152	150	13	37	9
7112 7112	8312 8401	<b>4</b> 1	17 1	11	10	55	1 <del>69</del>	10
7112	8402	16	214	190	190	4	9	7
7112	8403	7	67	53	52	-8	43	-2
7112 7112	8404 8405	30 10	3 <b>4</b> 3 101	315 92	315 92	3 0	9 7	5 1
7112	8406	24	330	285	284	5	8	4
7112	8407	8	98	<b>7</b> 6	<i>7</i> 5	8	13	2
7112 7112	8408 8409	10 9	129 111	95 99	94 99	7 5	17	1
7112	8410	4	31	22	22	6	9 9	2 -2
7112	8808	16	238	217	216	2	6	-2
7112	8809 8810	51	833	580	580	4	11	-1
7112 7112	9009	5 2	78 17	6 <b>4</b> 17	6 <b>4</b> 17	-14 -8	25 10	-2
7112	9010	23	336	336	332	10	16	
7114	7909 7010	22	272	271	271	-2	12	0
7114 7114	7910 7911	43 38	601 516	578 502	576 502	-1 0	13 16	0 0
7114	7912	28	428	427	427	-5	14	-3
7114	8001	11	1 <i>7</i> 5	173	173	-2	9	0
7114 7114	8002 8003	25 31	428 367	4 <i>2</i> 7 339	4 <i>27</i> 338	-3 -2	9 7	-4 -1
7114	8004	14	173	158	157	-5	8	
7114	8005	8	85	84	84	-2	8	-4 -2
7114 7114	8006 8007	1 2	5 10	5 8	5 8	0 -1	3 6	-10 <b>4</b>
7114	8008	15	149	107	107	1	10	1
7114	8009	16	163	15 <del>9</del>	158	-4	27	-1
7114 7114	8010 8011	11 32	128 498	114 493	114 492	-3 -1	12 12	-2 1
7114	8012	18	218	217	216	3	28	3
7114	8101	4	59	59	<del>59</del>	4	11	3 5
7114 7114	8108 8109	5 <b>24</b>	<b>4</b> 3 237	43 232	43 232	-3 0	12 8	-7 1
7114	8211	17	82 82	82 82	232 81	2	12	1
7114	8212	20	162	162	162	5	8	1
7114	8301 7900	28	232	232	225	2	11	4
7115 7115	7909 7910	1 23	4 326	4 320	4 320	-27 -3	31 13	-23 -12
7115	<b>7</b> 911	44	653	644	642	-8	17	-19
7115	<i>7</i> 912	31	380	379 307	<b>37</b> 9	-8	15	-17
7115 7115	8001 8002	24 21	297 279	297 279	297 279	-3 -1	13 8	-16 -14
7115	8003	20	267	261	261	-1 -2	8	-14
7115	8004	15	210	210	210	5	11	-11
7115 7115	8005 8006	14 23	146 221	146 220	144 220	-4 1	12	-18
7115 7115	8007	1	221 20	220 20	220 20	1 0	12 5	-12 -13
	<del>- ·</del>	-		<del></del>	<del></del>	-	<u>-</u>	

Station		No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
						(CIII)	(CIII)	(CIII)
			150	132	132	-8	11	-18
7115 7115	8008 8009	13 16	158 213	213	213	-1	8	-13
7115 7115	8010	20	255	255	255	-1	7	-12
7115	8011	33	294	291	291	-1	9	-11 -10
<i>7</i> 115	8012	14	128	128	128 <i>7</i> 5	2 -3	11 8	-10 -15
7115	8101	7 2	<i>7</i> 5 34	<i>7</i> 5 34	34	-14	19	-19
7115 7115	8102 8103	42	5 <b>88</b>	588	587	0	17	-12
7115	8104	18	230	229	228	2	11	-8
7120	8007	3	30	30	30 30′	0 4	8 11	8 7
7120	8008	21	297 341	297 341	296 340	2	9	6
7120 7120	8009 8010	19 <b>27</b>	289	283	283	5	12	7
7120 7120	8011	26	309	301	300	4	14	5
7120	8012	14	117	116	116	1	11 <b>26</b>	6 <b>4</b>
7120	8101	9	57	57 353	56 253	9 -2	26 16	3
7120	8102	20 32	253 400	253 400	400	2	10	5
7120 7120	8103 8104	22	229	226	225	4	15	4
7120	8105	13	86	86	85	-4	8	1
7120	8106	33	371	365	365 256	1 -4	9 13	1 2
7120	8107	21 24	261 391	25 <del>9</del> 391	256 387	0	9	0
7120 7120	8108 8109	2 <del>4</del> 29	466	463	461	1	10	2
7120	8110	30	<b>54</b> 6	546	546	-2	8	1
7120	8111	17	3 <u>09</u>	309	308	2 -8	9 13	7 -6
7120	8112	<b>4</b> 8	<i>7</i> 7 159	<i>7</i> 7 15 <del>9</del>	77 159	-2	13	-2
7120 7121	8201 8307	5	54	54	54	6	15	5
7121	8308	16	186	172	156	-6	22	5 2 3 5
7121	8309	6	106	106	106	0 2	5 7	<i>3</i> 5
7121	8310	14 9	176 74	173 74	173 74	2	7	5
7121 7121	8311 8312	13	136	131	131	-2	15	-1
7121	8401	1	<b>2</b> 1	21	21	4	7	7 10
7121	8402	11	83	79	73 143	3 13	18 17	14
7121	8403	12 16	148 192	144 158	157	2	14	2
7121 7121	8404 8405	15	142	137	136	0	8	4
7121	8406	14	170	148	144	-2	8	1
7121	8407	14	160	150	149 <i>7</i> 9	-1 -3	7 7	1 0
7121	8408	7 6	81 73	80 66	66	3	7	5
7121 7121	8409 8410	10	113	93	93	4	8	-1
7121	8411	19	<b>22</b> 5	206	205	-3	8	1
7121	8412	14	163	136	135 8	-5 5	12 6	5
7121	8501 8502	1 15	8 1 <b>4</b> 5	8 133	132	5	8	1 5 7 1
7121 7121	8503	15	142	137	118	-3 -5 5 5 -4 -65	205	1
7121	8504	8	49	49	32	-65	347	7
7121	8505	1	1 24	16	16	-1	10	-4
7121 7121	8506 8509	2	24 25	21	20	-15	22 25	3
7121	8510	3 2 9 7	25 7	7	7	21 -8 2 -6	25	13
7121 7121	8511	9	78 97	₩	<del>69</del> 87	-8 2	17 8	5
7121	8512	7 3	9/ 50	87 49	49	-6	8	-3
7121 7121	8601 8602	11	52 96	88	88	-12	15	-7
7121	8603	9 13	<i>7</i> 4	40	40	1	13	5
7121	8604	13	1 <i>7</i> 7	152	151 <i>8</i> 7	-10 2 -4	14 8	-4 3 13 5 -3 -7 5 -8 1
7122 7122	8305 8306	7 11	102 184	87 172	6/ 1 <b>72</b>	4	14	1
7122 7122	8307	8	88	81	<i>7</i> 5	-14	20	0
7122	8308	4	63	54	54	-3	8	-4
7122	8309	4	<i>₩</i>	<i>⊕</i>	63	-5 =	19 11	-3 n
7122	8310	20 16	275 259	273 258	273 258	-3 -5 -5 -4	8	2
7122 7122	8311 8312	16 7	259 98	236 97	258 97	-2	9	3
7122	8401	24	429	406	402	0	9	0 -4 -3 0 2 3 4
7122	8402	38	627	591	5 <b>7</b> 5	10	15	17

Station	Dete	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Engr. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
						(CIII)	(CIII)	(CIII)
7122	8403	15	266	250	250	6	14	11
7122	8406	11	143	143	142	0	5	6
7122	8408	12	155	153	149	3	13	5
7122	8409	1 <b>4</b>	185	179	179	-2	13	2 4
7122 7122	8410 8411	25 27	382 520	380 520	378 520	1 0	7 7	4
7122	8412	18	289	289	284	3	13	5 7
7122	8501	14	248	247	247	-1	5	2
7122	8502	17	293	292	292	i	6	4
7122	8503	22	382	378	378	-1	11	7
7122	8504	25	414	414	414	2	8	4
7122	8505 8506	26	503	502	501	0	5	4
7122 7122	8506 8507	19 10	327 131	327 131	326 131	0 <b>4</b>	6	4
7122	8508	24	32 <b>4</b>	322	322	-1	13 8	<b>4</b> 1
7122	8509	22	328	328	328	-1 -1	11	3
7122	8510	<u>25</u>	458	457	456	- <b>1</b>	9	2
7122	8511	24	397	397	397	6	10	3
7122	8512	15	213	95	95	3	6	2
7122	8512			118	102	-5	13	4
7122	8601	21	372	372	371	0	7	2
7122	8602	30 35	502 225	502 224	502	-5	8	-1
7122 7122	8603 8604	25 23	335 350	334 349	334 348	1 - <b>4</b>	12 7	4 -1
7122	8605	15	206	163	162	-2	7	-1
7122	8606	14	268	203	203	4	7	-1
7122	8607	14	181	141	140	-8	10	•
7122	8608	12	126	63	63	7	9	8
7122	8609	18	266	265	265	-2	7	
7122	8610	20	378	378	378	1	5	-1
7122 7122	8611 8612	13	255	237	237	-1	8	,
7122	8701	9 13	121 180	88 177	88 177	0 -6	5 13	6
7122	8702	27	480	480	480	-0 -2	9	1 <b>4</b>
7122	8703	<u></u>	324	277	277	Õ	ģ	3
7122	8704	12	196	190	190	-8	15	-1
7122	8705	1	10	10	10	-1	3	0
7122	8706	19	318	317	316	-3	6	1
7122 7122	8707 8708	13	150	145	144	-5 10	9	-1
7122	8709	6 10	<del>69</del> 157	30 138	20 136	-13 -5	18 9	-18
7122	8710	22	381	368	368	-5 0	5	-1 2
7122	8711	26	426	404	404	-6	8	-2
7122	8712	15	254	95	95	-3	10	ō
7122	8801	23	322	256	256	-2	7	2
7122	8802	26	<b>42</b> 0	228	211	-5	13	0
7122	8803	17	250	202	202	-2	6	1
7122 7122	8804 8805	11 2	154 14	138	138 1	-3 <b>27</b>	5	0
7122	8806	3	8	5 4	4	27 -1	34 1	13 4
7122	8807	2	21	21	17	-15	24	-2
7122	8808	3	35	21	21	-6	6	0
7122	8808			3	3	-5	6	-5
7122	8809	9	88	<i>7</i> 1	71	2	5	0
7122	8810	34	404	354	333	-4	9	-1
7122	8811	14	188	148	146	-6	12	-1
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7123 8808 7 7 79 66 66 66 -8 21 7123 8808 8 84 62 62 -2 5 7123 8809 1 155 7123 8906 7 99 99 99 -101 107 7123 8906 12 197 197 196 -101 108 7123 8906 12 197 197 196 -101 108 7123 8907 16 215 215 215 -84 101 7123 8908 10 166 154 153 -100 107 7123 8908 10 166 154 153 -100 107 7123 9004 15 180 162 162 -2 14 7123 9005 10 135 134 134 -2 8 7123 9006 3 53 53 53 53 3 16 7123 9006 3 53 53 53 53 3 16 7123 9007 10 121 121 109 46 115 7123 9008 2 28 28 28 28 -8 11 7125 8505 10 138 138 138 131 2 90 7125 8506 16 248 223 219 -6 50 7125 8507 9 127 127 119 2 55 7125 8507 9 127 127 119 2 55 71210 7905 2 3 1 1 1 799 0 7210 7907 4 4 4 2 0 102 146 7210 7908 3 3 3 7210 7907 4 4 4 2 0 102 146 7210 7908 3 3 3 7 1 0 53 0 7210 8001 2 3 1 1 0 53 0 7210 8001 2 3 1 1 0 53 0	3
7123       8806       8       84       62       62       -2       5         7123       8809       1       15       99       99       -101       107         7123       8905       7       99       99       -101       107         7123       8906       12       197       197       196       -101       108         7123       8908       10       166       154       153       -100       107         7123       8908       10       166       154       153       -100       107         7123       9004       15       180       162       162       -2       14         7123       9005       10       135       134       134       -2       8         7123       9006       3       53       53       53       3       3       16         7123       9007       10       121       121       109       46       115         7123       9007       10       121       121       109       46       115         7123       9008       2       28       28       28       28       8       11	0
7123         8809         1         15         99         99         -101         107           7123         8905         7         99         99         99         -101         108           7123         8906         12         197         197         196         -101         108           7123         8907         16         215         215         215         -84         101           7123         8908         10         166         154         153         -100         107           7123         9004         15         180         162         162         -2         14           7123         9005         10         135         134         134         -2         8           7123         9006         3         53         53         53         3         16           7123         9007         10         121         121         109         46         115           7123         9007         10         121         121         109         46         115           7123         9008         2         28         28         28         8         11	1
7123         8906         12         197         197         196         -101         108           7123         8907         16         215         215         215         84         101           7123         8908         10         166         154         153         -100         107           7123         9004         15         180         162         162         -2         14           7123         9005         10         135         134         134         -2         8           7123         9006         3         53         53         53         3         16           7123         9007         10         121         121         109         46         115           7123         9008         2         28         28         -8         11           7123         9008         2         28         28         28         -8         11           7123         9008         2         28         28         28         -8         11           7125         8505         10         138         138         131         2         90           7125 <td>-1</td>	-1
7123         8906         12         17         215         215         -84         101           7123         8908         10         166         154         153         -100         107           7123         9004         15         180         162         162         -2         14           7123         9005         10         135         134         134         -2         8           7123         9006         3         53         53         53         3         16           7123         9007         10         121         121         109         46         115           7123         9008         2         28         28         28         8         11           7123         9008         2         28         28         28         8         11           7125         8505         10         138         138         131         2         90           7125         8506         16         248         223         219         -6         50           7210         7905         2         3         1         1         -79         0	-1 -2
7123         8908         10         166         154         153         -100         107           7123         9004         15         180         162         162         -2         14           7123         9005         10         135         134         134         -2         8           7123         9006         3         53         53         53         3         16           7123         9007         10         121         121         109         46         115           7123         9008         2         28         28         28         8         11           7125         8505         10         138         138         131         2         90           7125         8506         16         248         223         219         -6         50           7125         8507         9         127         127         119         2         55           7210         7905         2         3         1         1         -79         0           7210         7907         4         4         4         2         0         102         146	4
7123         9004         15         180         162         162         -2         14           7123         9005         10         135         134         134         -2         8           7123         9006         3         53         53         53         3         16           7123         9007         10         121         121         109         46         115           7123         9008         2         28         28         28         8         11           7125         8505         10         138         138         131         2         90           7125         8506         16         248         223         219         -6         50           7125         8507         9         127         127         119         2         55           7210         7905         2         3         1         1         -79         0           7210         7907         4         4         2         0         102         146           7210         7912         7         21         7         721         7         721         7         721 <td>-12</td>	-12
7123         9005         10         135         134         134         -2         3           7123         9006         3         53         53         53         3         16           7123         9007         10         121         121         109         46         115           7123         9008         2         28         28         28         -8         11           7125         8505         10         138         138         131         2         90           7125         8506         16         248         223         219         -6         50           7125         8507         9         127         127         119         2         55           7210         7905         2         3         1         1         -79         0           7210         7907         4         4         2         0         102         146           7210         7908         3         3         3         -         -         -         -         -         -         -         -         -         -         -         -         -         -         -	0 3
7123 9007 10 121 121 109 46 115 7123 9008 2 28 28 28 8 11 7125 8505 10 138 138 131 2 90 7125 8506 16 248 223 219 -6 50 7125 8507 9 127 127 119 2 55 7210 7905 2 3 1 1 1 -79 0 7210 7907 4 4 2 0 102 146 7210 7908 3 3 3 7210 7908 3 3 3 7210 7911 4 4 4 4 4 0 142 681 7210 7912 7 21 7210 8001 2 3 1 0 53 0 7210 8004 5 15 7210 8005 2 2 1 0 53 0	-2
7123 9008 2 28 28 8 11 7125 8505 10 138 138 131 2 90 7125 8506 16 248 223 219 -6 50 7125 8507 9 127 127 119 2 55 7210 7905 2 3 1 1 1 -79 0 7210 7907 4 4 2 2 0 102 146 7210 7908 3 3 7210 7911 4 4 4 4 0 142 681 7210 7912 7 21 7210 8001 2 3 1 0 53 0 7210 8004 5 15 7210 8004 5 15 7210 8006 2 2 1 0 660 0 7210 8100 7 7 79 79 79 0	_
7125 8506 16 248 223 219 -6 50 7125 8507 9 127 127 119 2 55 7210 7905 2 3 1 1 1 -79 0 7210 7907 4 4 2 2 0 102 146 7210 7908 3 3 7210 7911 4 4 4 4 0 142 681 7210 7912 7 21 7210 8001 2 3 1 0 53 0 7210 8004 5 15 7210 8005 2 2 1 0 -660 0 7210 8109 7 79 79 79 0 16	_
7125     8506     16     248     223     219     -6     33       7125     8507     9     127     127     119     2     55       7210     7905     2     3     1     1     -79     0       7210     7907     4     4     2     0     102     146       7210     7908     3     <	2 -4
7110 7905 2 3 1 1 -79 0 7210 7907 4 4 2 2 0 102 146 7210 7908 3 3 7210 7911 4 4 4 4 0 142 681 7210 7912 7 21 7210 8001 2 3 1 0 53 0 7210 8004 5 15 7210 8005 2 2 1 0 660 0 7210 8109 7 79 79 79 0 16	- <del>4</del> -1
7210 7907 4 4 2 0 102 146 7210 7908 3 3 3 7210 7911 4 4 4 4 0 142 681 7210 7912 7 21 7210 8001 2 3 1 0 53 0 7210 8004 5 15 7210 8005 2 2 1 0 660 0 7210 8109 7 79 79 79 0 16	-87
7210     7908     3     3       7210     7911     4     4     4     4     0     142     681       7210     7912     7     21     7210     8001     2     3     1     0     53     0       7210     8004     5     15       7210     8005     2     2     1     0     -660     0       7210     8109     7     79     79     79     0     16	-1
7210 7911 7 21 7 21 7 21 7 21 7 21 7 21 7 21	-1
7210 8001 2 3 1 0 53 0 7210 8004 5 15 7210 8005 2 2 1 0 -660 0 7210 8109 7 79 79 79 0 16	-1
7210 8004 5 15 7210 8005 2 2 1 0 -660 0 7210 8109 7 79 79 79 0 16	-1
7210 8005 2 2 1 0 -660 0 7210 8100 7 79 79 79 0 16	
7210 8109 7 79 79 79 10 10 10 10 10 10 10 10 10 10 10 10 10	-1 4
	8
7210 8111 19 284 284 284 -1 8	5
7210 8112 14 187 187 187 -1 11	5 2 -4
7210 8201 6 83 83 83 -3	6
7210 8202 9 130	7
7210 8203 9 133 19	-1
	3
7210 8206 25 409 329 329 -1 2	3
7210 8207 25 390 388 388 -2 6 7210 8208 10 148 146 146 -10 16	0
7210 8209 11 150 150 4 10	-3
7210 8210 19 235 235 235 6 12	-3 9 2
7210 8211 7 83 83 83 1	0
7210 6212 21 361 460 460 1 5	3
7210 8301 32 488 488 488 -1 8	1
7210 8303 31 569 569 568 1 7	6 3
7210 8304 23 402 402 402 0 10	3 4 3 7 4
7210 8305 32 595 582 582 2	3
7210 8307 18 276 276 276 1 11	7
/210 000/ 10 2/0	4
7210 8309 34 460 454 454 0	5
7210 8310 30 400 396 396	A
7210 8311 26 382 381 381 0 4	5 <b>4</b> 6

Station Number	Date	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	eng r. East	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
	· · · · · · ·					()	(4.1.)	(4111)
7210	8312	37	513	512	512	0	6	2
7210	8401	27	374	374	373	1	7	6
7210 7210	8403 8404	2 35	18 401	18 22	18 22	-7 - <b>4</b>	8 12	-2 15
7210	8404	2	401	378	378	2	8	7
7210	8405	52	600	563	563	3	7	7
7210 7210	8406 8407	45 23	616 302	606 301	605 301	1 2	6 7	6
7210	8408	2	266	264	264	0	8	5 5
7210	8409	33	436	435	435	-1	9	3
7210 7210	8410	26 17	390 363	389	389	-1	6	3 2
7210 7210	8411 8412	17 16	262 200	261 200	261 198	0 -1	9 14	5 2
7210	8501	12	154	153	153	-3	6	0
7210	8502	3	25	25	25	-1	11	-2
7210 7210	8503 8504	7 23	35 235	31 232	30 230	-25 -10	143	5
7210	8505	13	147	138	112	-10 9	74 16	-8 10
7210	8506	29	344	340	340	0	6	4
7210 7210	8507	24	335	330	330	-1	11	4
7210 7210	8508 8509	31 23	430 353	426 353	423 353	1 -2	12 11	5 <b>4</b>
7210	8510	25	346	346	346	-1	9	4
7210	8511	20	279	278	277	1	10	4
<i>7</i> 210 <i>7</i> 210	8512 8601	21 21	301 330	298 330	297 330	0 2	6 7	4 4
7210	8602	24	317	317	317	3	10	6
7210	8603	18	297	296	296	-3	7	1
7210 7210	8604 8605	6 10	85 152	85 136	85 126	4	13	5
<b>72</b> 10	8606	11	140	125	136 125	4 2	10 5	9
<b>72</b> 10	8607	18	232	163	163	-1	8	
<i>7</i> 210 <i>7</i> 210	8608 8609	15 10	159 98	145 96	145	-1	9	8
7210 7210	8610	14	220	218	96 218	1 2	5 <b>4</b>	3
7210	8611	11	107	105	105	2	7	3
7210 7210	8612	6	53	.52 177	52 177	4	8	5
7210 7210	8701 8702	17 17	184 197	176 196	176 182	7 3	20 19	6
7210	8703	12	137	73	73	-8	10	2 2
7210 7210	8704	22	288	154	154	1	6	5
7210 7210	8705 8706	28 25	416 321	332 282	332 277	<b>4</b> 0	8 7	7 6
7210	8707	19	267	36	36	1	8	7
7210	8707	•	•••	198	198	3	6	7
7210 7210	8708 8709	16 2	239 15	197	192	-3	8	0
7210	<b>871</b> 0	22	311	249	249	-1	6	2
7210	8711	16	209	161	161	-7	9	-1
7210 7210	8712 8801	9 <b>2</b> 5	122 331	121 183	121	-2	6	4
7210	8802	28 28	385	120	183 120	-3 4	7 6	2 4
7210	8803	13	136	48	48	2	7	5
7210 7210	8804 8805	23 22	246 250	194 223	194 223	-2 -3	4	1
7210	8806	13	163	142	141	-3 -5	5 6	2 0
7210	8807	37	480	392	360	-5	13	2
7210 7210	8808 8809	37 16	448	317	317	-4	5	1
7210 7210	8810	19 31	220 382	122 173	122 168	-3 -4	5 9	3 0
7210	8811	8	107	21	20	-3	14	3
7210	8812	13	173	110	107	-3	10	0
7210 7210	8901 8902	8 11	141 147	54 96	47 96	-16 -5	18 16	-8 1
<b>72</b> 10	8903	10	151	96 137	96 137	-5 -5	16 7	-1 2
<b>7210</b>	8904	7	106	92	92	-6	8	0
7210 7210	8905	11	355 25	135	135	-5	7	1
7210 7210	8906 8907	3 18	35 258	29 72	29 68	-26 13	27 27	-10 11
7210	8908	12	226	112	103	-11	22	-9
						- <del>-</del>	<del>_</del>	-

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate (cm)
						(cm)	(cm)	(cm)
7010	8909	11	179	179	179	-1	5	2
7210 7210	8910	5	59	77	77	-7	9	-4
7210	8911	16	222	182	177	1	9	8 6
7210	8912	11	152	139	139	0	6	6 21
<b>72</b> 10	9001	1	12	12	12 70	1 -7	15 9	-21 -3 -2
7210	9002	10	105	70 206	70 206	-/ -1	9	- <b>2</b>
7210	9003	21 14	229 143	108	108	-6	14	-4
7210	9004 9005	12	196	123	123	2 -5	16	-1
7210 7210	9006	15	209	151	145	-5	11	3
7210	9007	13	128	128	128	2	11	
7210	9008	14	188	188	188	4	9	
7210	9009	16	198	198	198	-3 -3	8 8	
7210	9010	22	290	290	290 120	-3 -1	11	
7210	9011	9	120	120 164	161	7	16	
7210	9012	12 33	164 408	399	396	Ö	10	3
7220 7220	830 <del>9</del> 8310	39	465	463	452	2	20	2
7220 7220	8311	5	36	35	35	-5 ·	11	0
7265	8401	22	276	276	276	1	6	1 3
7265	8402	21	267	266	266	-5	10 9	<i>3</i> 5
7265	8403	8	86	86	86 102	1 -2	4	1
7288	8803	12	143	102	119	0	3	i
7288	8804	10 20	125 450	119 409	409	- <b>2</b>	4	1
7288	8805 8806	28 15	211	206	206	ō	14	1
7288 7288	8902	11	156	156	156	-14	18	<b>-4</b>
7288 7288	8903	4	54	54	54	-16	24	-7
7288	8904	13	186	186	186	-4	5	0 17
7288	8910	1	2	10	10	14	15 10	4
7288	8911	24	369	3 <del>69</del>	3 <del>69</del> 3 <b>4</b> 3	-2 -2	11	3
7288	8912	18	343 127	343 137	343 137	- <u>-2</u> -11	16	- <del>7</del>
7288	9001	7 14	137 224	22 <b>4</b>	224	-5	12	
7288 7288	9011 9012	12	193	193	193	-4	10	_
7295	8803	3	21	20	20	20	21	2 -3
7295	8804	19	236	227	227	7	9	-3 -2
7295	8805	2	14	11	11	6	8 12	-2 -2
7295	8806	14	163	155	153 138	10 10	14	0
7295	8807	14	160 83	138 83	83	3	20	14
7307	8809 8403	7 8	80 90	89 89	89	-3	8	1
7400 7400	8404	25	256	244	244	1	7	-3
7400	8405	10	120	120	120	-3	8	-4
7401	8405	13	180	177	177	1	7 9	- <del>0</del>
7401	8406	40	180 613 5	585	581	-1 141	158	-8 -9 -1
7401	9002	1	300	5 398	0 92	65	110	9
7401	9003	25 14	398 251	251	251	6	26	9 7 7 7
7401 7401	9004 9005	20	3 <b>4</b> 1	341	341	7	18	7
7401 7401	9006	2	23	23	23	-12	37	7
7401	9012	2 29	382	382	375	6	20	
7403	9007	26	450					
7403	9008	21	388					
7403	9009	24	413 193					
7403	9010	12 30	193 387	302	298	-3	15	
7510 7510	8606 8607	30 30	305	213	213	-3 2	17	_
7510 7510	8608	20	<del>-</del>					-6
7510	8610						21	-4 -8 -5 -5 1 -2 2
<b>7510</b>	8706	13	100	79	79 405	6	21 15	-0 -5
7510	8707	63	571 540	496	495 462	5 5	13 14	-5 -5
7510	8708	55 12	540 80	462 80	402 80	10	22	1
7510 7510	8910	13 <b>43</b>	625	626	623	10 7	103	-2
7510 7510	8911 8912	13	250	249	249	7	25	2
7510 7512	8609	8	80	<i>7</i> 7	<i>7</i> 7	7 -5	11	
7512 7512	8610	5Ŏ	705	670	665	-2	16	
7512	8702				44		<b>1</b> 5	- <b>4</b> 1
7512	8703	6	49	42	42	9	15	ı

Station		No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual	Residual	Estimate
						(cm)	(cm)	(cm)
7512	8704	46	498	354	354	2	15	-3
7512	8705	9	119	105	105	-7	<b>2</b> 0	-6
7512	8910	58	808	803	<b>78</b> 6	-6	16	-6
7515 7515	8608	42	603	532	532	3 -9	63	
7515 7515	8609 8612	5	80	74	74	-9	72	-4
7515 7515	8702							-1
7515	8707	11	139	<i>7</i> 8	78	-4	41	- <b>ż</b>
7515	8708	48	604	426	426	19	63	-1
7515	8709	56	749	436	436	-1	50	-1
7515 7515	8710	40	488	383 13	383 13	4	63 29	-3
7515 7515	8912 9001	2 45	13 599	599	599	12 20	<i>6</i> 7	2 4
7517	8606	12	158	125	123	-1	16	•
7517	8607	23	225	131	130	7	17	
7517	8608	33	301	228	227	1	11	-2
7517	8609	8	81	80	78	8	15	_
7517 7517	8610							-1 -3
7517 7517	8612 8702							-3 -1
7517 7517	8707	16	261	261	261	11	16	1
7517	8708	42	532	450	450	10	16	-1
7517	8710	8	104	46	46	9	17	4
7517	8711	33	514	390	390	7	15	-2
7517 7517	8712	15 22	218	1 <i>69</i>	1 <del>69</del>	19	25 14	4
7517 7517	8905 8906	32 18	385 298	312 260	312 260	5 -9	14 39	-2 4 -3 -5 4
7520	8604	37	5 <b>4</b> 1	518	511	ó	7	4
7520	8605	9	130	119	117	3	7	
7520	8606	_					_	7
7520 7520	8906	9	103	90	90	-16	31 ~	-41
7520 7520	8907 8908	38 4	451 45	449 45	449 45	5 -11	26 36	4 16
7525	8609	22	252	175	175	13	25	10
7525	8609			56	56	18	29 32	
7525	8610	3	26	26	26	-2	32	
7525 7525	8702							0
7525 7525	8702 8704							0 1
7525 7525	8709	4	50	50	50	16	26	5
7525	8710	29	444	370	370	17	32	3
7525	8711	21	293	220	220	18	30	3
7525	8712	13	203	141	141	16	<u> 36</u>	6
7525 7525	8911 8912	5 9	34 94	31 92	30 92	9	77 24	1
7525 7525	9001	37	474	474	467	5 18	36 75	2 -2
7530	8607	2	16	16	14	-22	24	~
7530	8608	1	6	5	4	18	22	
7530	8609	6	72	60	<del>59</del>	15	17	_
7530 7530	8610	8	103	84	84	0	8	-5
7530 7530	8611 8612	13 11	167 137	137 81	137 75	-2 10	8 13	-5
7530	8701	8	101	89	89	-2	11	-5 3
7530	8702	10	90	55	55	<u>-</u> 4	15	3
7530	8703	2	24	22	22	8	12	10
7530	8704	10	114	98	<b>%</b>	-6	16	-2
7530 7530	8705 8706	4 8	53 158	20	20	2	19	3
7530 7530	8707	12	158 171	64 126	64 126	1 0	8 7	-2 2
7530 7530	8708	4	54	26	26	-4	11	2 -5
7530	8709	14	253	142	142	2	16	5
7530	8710	10	130	81	81	-1	10	1
7530	8711	12	162	148	141	-1	12	2
7530 7530	8909	2	26	26	9	-478 0	2174	6
7530 7530	9001	1	16 <b>28</b>	16 21	16 21	9	12 22	-3 10
7530 7530	9002 9003	4 11	28 131	21 131	21 130	-11 -9	19	-10 -8
		11	113	82	79	- <del>22</del>	26	-0 -7
7530	9000							
7530 7541 7541	9006 8601 8602	34 21	449 226	430 76	418 76	1 3	6	-1 -3

7541 8603 6 50 7543 9011 1 17 7543 9012 25 368 7544 8709 17 163 7544 8710 43 417 7544 8711 16 125 7544 8712 11 83 7544 8903 1 14 7544 8904 1 7 7544 8904 1 7 7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8801 3 19 7545 8802 34 318 7545 8803 21 170	49 17 368 314 85 62 14 7 530 11 319 116 18 271 140 284 72 189 1	49 17 368 308 85 62 14 7 530 11 319 113 18 270 140 284 72 189	(cm)  1 -11 -5  16 9 13 14 45 14 10 1 4 3 3 3 16 1	(cm)  6 19 15 22 22 28 16 49 21 22 7 7 6 7 21 15	-2  1 0 6 5 6 1 2 -2 1 0 -2 -1 2
7543 9011 1 17 7543 9012 25 368 7544 8709 17 163 7544 8710 43 417 7544 8711 16 125 7544 8712 11 83 7544 8903 1 14 7544 8904 1 7 7544 8905 41 533 7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	17 368 314 85 62 14 7 530 11 319 116 18 271 140 284 72 189 1	17 368 308 85 62 14 7 530 11 319 113 18 270 140 284 72 189	-11 -5 16 9 13 14 45 14 10 1 4 3 3 3 16 1	19 15 22 22 28 16 49 21 22 7 7 7 7 6 7	1 0 6 5 6 1 2 -2 1 0 -2 -1 2
7543 9011 1 17 7543 9012 25 368 7544 8709 17 163 7544 8710 43 417 7544 8711 16 125 7544 8712 11 83 7544 8903 1 14 7544 8904 1 7 7544 8905 41 533 7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	17 368 314 85 62 14 7 530 11 319 116 18 271 140 284 72 189 1	17 368 308 85 62 14 7 530 11 319 113 18 270 140 284 72 189	-11 -5 16 9 13 14 45 14 10 1 4 3 3 3 16 1	19 15 22 22 28 16 49 21 22 7 7 7 7 6 7	1 0 6 5 6 1 2 -2 1 0 -2 -1 2
7543 9012 25 368 7544 8709 17 163 7544 8710 43 417 7544 8711 16 125 7544 8712 11 83 7544 8903 1 14 7544 8904 1 7 7544 8905 41 533 7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	368 314 85 62 14 7 530 11 319 116 18 271 140 284 72 189 1 39	368 308 85 62 14 7 530 11 319 113 18 270 140 284 72 189	-5 16 9 13 14 45 14 10 1 4 3 3 3 16	22 22 28 16 49 21 22 7 7 7 6 7	0 6 5 6 1 2 -2 1 0 -2 -1 2
7544     8709     17     163       7544     8710     43     417       7544     8711     16     125       7544     8712     11     83       7544     8903     1     14       7544     8904     1     7       7544     8905     41     533       7544     8906     1     11       7545     8511     22     333       7545     8512     6     117       7545     8801     3     19       7545     8802     34     318	85 62 14 7 530 11 319 116 18 271 140 284 72 189 1	85 62 14 7 530 11 319 113 18 270 140 284 72 189	9 13 14 45 14 10 1 4 3 3 3 16	22 28 16 49 21 22 7 7 7 6 7	0 6 5 6 1 2 -2 1 0 -2 -1 2
7544 8711 16 125 7544 8712 11 83 7544 8903 1 144 7544 8904 1 7 7544 8905 41 533 7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	85 62 14 7 530 11 319 116 18 271 140 284 72 189 1	85 62 14 7 530 11 319 113 18 270 140 284 72 189	9 13 14 45 14 10 1 4 3 3 3 16	22 28 16 49 21 22 7 7 7 6 7	0 6 5 6 1 2 -2 1 0 -2 -1 2
7544 8712 11 83 7544 8903 1 14 7544 8904 1 7 7544 8905 41 533 7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	62 14 7 530 11 319 116 18 271 140 284 72 189 1	62 14 7 530 11 319 113 18 270 140 284 72 189	13 14 45 14 10 1 4 3 3 3 3	28 16 49 21 22 7 7 7 6 7 21	6 5 6 1 2 -2 1 0 -2 -1 2
7544 8903 1 14 7544 8904 1 7 7544 8905 41 533 7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	14 7 530 11 319 116 18 271 140 284 72 189 1	14 7 530 11 319 113 18 270 140 284 72 189	14 45 14 10 1 4 3 3 3 16	49 21 22 7 7 7 6 7 21	6 1 2 -2 1 0 -2 -1 2
7544 8904 1 7 7544 8905 41 533 7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	530 11 319 116 18 271 140 284 72 189 1	530 11 319 113 18 270 140 284 72 189	14 10 1 4 3 3 3 3 16	21 22 7 7 7 6 7 21	1 2 -2 1 0 -2 -1 2
7544 8906 1 11 7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	11 319 116 18 271 140 284 72 189 1	11 319 113 18 270 140 284 72 189	10 1 4 3 3 3 16 1	22 7 7 7 6 7 21	2 -2 1 0 -2 -1 2
7545 8511 22 333 7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	319 116 18 271 140 284 72 189 1	319 113 18 270 140 284 72 189	1 4 3 3 3 16 1	7 7 7 6 7 21	-2 1 0 -2 -1 2
7545 8512 6 117 7545 8801 3 19 7545 8802 34 318	116 18 271 140 284 72 189 1	18 270 140 284 72 189	3 3 3 16 1	7 6 7 21	0 -2 -1 2
7545 8801 3 19 7545 8802 34 318	271 140 284 72 189 1 39	270 140 284 72 189	3 3 16 1	6 7 21	-2 -1 2
	140 284 72 189 1 39	140 284 72 189	3 16 1	<i>7</i> 21	-1 2
	284 72 189 1 39	284 72 189	16 1		2
7545 8803 21 170 7545 9002 24 303	72 189 1 39	189		15	
7545 9003 7 72	1 39				-4 -1
7545 9004 18 201	39	1	-11 5	19 0	-1 9
7546 8804 1 1 7546 8805 7 41	-	1 39	4	12	4
7546 8805 7 41 7546 8806 4 37	37	37	7	22	6
7550 8604 5 44	44	44	0 -2	11 <b>2</b> 0	16
7550 8605 24 256	247	247	-2	20	14
7550 8606 7550 8906 15 59	58	58	-7	19	13
7550 8907 5 28	28	28	-26	37	3
7575 8704 5 <b>44</b>	37	37 209	29 14	33 18	2 -1
7575 8705 27 261 7575 8909 60 918	209 914	914	18	22	5
7575 8909 60 918 7580 8704 27 322	241	241	12	21	1
7580 8705 16 220	206	206	10	14 42	-3 0
7580 8910 32 430 7580 8911 18 243	451 243	449 243	7 4	42 19	0
7580 8911 18 243 7585 8706 27 251	225	225	10	17	11
7585 8707 10 65	14	14	7	28	4
7585 8908 45 478	456 173	456 1 <i>7</i> 2	-8 21	33 41	-10 19
7585 8909 12 175 7587 8706 34 457	172 397	397	-3	7	-2
7587 8706 34 457 7587 8707 9 133	114	114	-1	6	-1
7587 8907 1 10	10	10 220	7 -3	9 28	2 2
7587 8908 20 245 7587 8909 16 183	220 177	1 <b>77</b>	0	12	-1
7587 8909 16 183 7587 8910 14 196	195	195	3	22	4
7590 8509 19 351	345	332	8 -2	13 10	4 -2
7590 8510 26 548	531 <b>37</b>	509 19	-2 198	222	107
7596 8503 4 37 7596 8504 1 6	3/		.,,		
7602 9009 20 270	270	270	-1	10 53	-12
7805 8009 6 66	20 18	20 18	- <b>43</b> -55	33 79	-12 -2
7805 8010 5 72 7805 8011 8 89	65	65	-158	197	-108
7805 8012 7 71	43	43	-127	193	-80 277
	<i>6</i> 7	<i>6</i> 7 229	225 253	268 322	276 310
7805 8104 20 232 7805 8105 4 4	232 4	3	464	643	466
7805 8108 1 15	15	15	332	351	384
7805 8109 4 50	50	46	208	297 124	231 341
7805 8110 3 24	2 41	2 41	<i>7</i> 3 140	191	195
7805 8111 3 41 7805 8203 2 26	26	26	66	211	100
7805 8205 1 1				227	
7805 8208 6 74	<i>7</i> 4	73 141	-2 <b>4</b> -81	221 141	5
7805 8209 11 143	143	141	-01	1771	-25
7805 8210 5 63 7805 8211 7 94	90	90	-84	162	
7805 8212 3 38	28	26	-79	173	-40 -45
7805 8301	94	83	-193	1155	-43 -62
7805 8303 11 94 7805 8304 3 24	94 24	24	-86	181	-36
7003 0001 0	-				

Number	132+0	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
	Date	Passes	Acquired	Engr. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
7805	8311	2	16	16	13	-170	273	-63
7805 7805	8312 8403	3 13	30 196	30 43	30 43	-103 -20	190 78	-71 17
7805	8404	3	31	4	4	20	88 88	-121
7805	8405	9	54	5	4	132	256	87
7805 7805	8408 8409	8 7	109 117	20 8	20 8	-30 -34	61 39	4 14
7805	8410	11	136	6	6	-33	42 42	25
7805	8411	1	18	_	_		_	
7805 7805	8603 8612	5 5	56 15	5	5	-61	70	1
7805	8705	6	32	2	2	-27	40	-8
7805	8809	3	18					_
7805 7805	8904 8905	3 1	20 5	20 5	20 5	-64 -71	116 156	-3 -150
7805 7805	8910	1	4	4	2	350	2303	-130
7805	8912	3	30	25	25	-99	110	-54
7805 7810	9003 8405	7 1	<b>47</b> 9	47 9	<b>4</b> 7 8	-30 11	56 16	-9 6
7810	8406	5	64	64	64	-3	8	-1
7810	8407	14	177	170	169	-1	12	3
7810 7810	8408 8409	18 10	263 134	256 100	256 100	-3 3	12 9	2 0
7810 7810	8410	12	117	100	100	-6	11	-1
7810	8411	4	65	65	64	4	12	4
7810 7810	8509 8510	1 <b>4</b> 22	173 238	154 223	154 223	12 0	17 11	<b>4</b> -3
<b>7810</b>	8511	2	236 22	20	20 20	-7	19	-3 -1
7810	8512	7	78	69	69	7	11	3
7810 7810	8603 8604	14 3	140 30	137 27	137 <i>2</i> 7	1 -4	6 14	3 -5
<b>7810</b>	8605	4	41	34	34	6	9	-5
7810	8606							-2
7810 7810	8609 8610	2 1	13 11	13 11	13 11	0 -4	12 11	
7810	8611	12	182	172	171	Ô	10	
7810 7810	8612	7	81	71	71	-2	10	
7810 7810	8702 8703	2	29	23	19	-5	18	-4 -12
7810	8704	22	298	195	191	10	16	1
7810 7810	8705 8706	11	136	131 34	131	0	7	-1
7810 7810	8707	3 5	37 42	34 40	32 36	1 9	11 14	-4 4
7810	8708	14	174	166	151	7	13	3
7810 7810	8709 8710	25 11	347 112	327 109	325 101	4 4	12 13	1 -2
7810	8711	14	139	84	84	4	9	-2 -2
7810	8803	2	23	23	18	-8	13	-2 -2 2
7810 7810	8804 8805	6 2	73 21	73 21	70 17	-8 -6	10 11	2
7810	8806	14	192	107	107	0	8	5
7810	8807	16	190	170	170	3	11	4
7810 7810	8808 8809	30 33	418 449	377 238	338 227	5 2	10 10	5 4
7810	8810	4	57	38	30	-10	15	-6
7810 7810	8811	30 20	444	342	336	2	11	5
7810 7810	8812 8901	20 44	308 637	157 455	150 444	8 8	13 12	5 5
7810	8902	41	562	499	499	11	14	11
7810 7810	8903 8904	7 9	75 87	72 56	72 55	<i>7</i> 15	13 19	9 12
7810 7810	8904 8905	16	8/ 2 <b>4</b> 2	207	207	3	19 12	12 3
7810	8906	9	119	103	103	4	12	-1
7810 7810	8907 8908	4	29 8	18	18	15 5	16 7	1
7810 7810	8908 8909	2 1	8 4	3 3	3 3	5 <b>3</b>	7 12	-1 -2
7810	8910	9	100	80	80	-10	14	0
7810	8911	12	176	117	117	-4	11	2
7810	8912	14	19 <del>9</del>	109	109	14	26	19

Station		No. of	Observ.	Obs. after	Obs. after	Mean	RMS of Residual	Bias Estimate
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual (cm)	(cm)	(cm)
		· · · · · · · · · · · · · · · · · · ·				<del></del>		
7810	9002	29	414	340	324	-3	16	1 7
7810	9003	34	480	321	321	-11 -26	15 31	-7 -5
7810	9004	9 24	114 290	67 237	50 237	-20 -6	11	-1
7810 7810	9005 9006	9	101	<i>237</i> 71	70	-9	16	-3
7810 7810	9007	<b>3</b> 0	415	415	414	<b>-4</b>	10	
7810	9008	26	359	359	359	0 1	7 9	
7810	9010	19	248 105	248 105	248 105	5	16	
7810 7811	9011 8805	8 2	19	10	10	17	<i>7</i> 1	-24
7811	8806	3	21	11	11	-16	20	-8 21
7811	8807	5	<u>49</u>	7	7	21 <b>43</b>	26 77	-31 -4
7811	8808	<i>7</i> 14	<i>7</i> 9 117	17 93	17 61	103	177	Ō
7811 7811	880 <del>9</del> 8811	1	5	5	5	-8	60	1
7811	8905	11	136	134	134	98	141	11
7811	8906	2	23	23	23 16	90 34	117 <i>7</i> 5	-10 16
7811	9001	2 2 5 5	16 50	16 50	50	99	139	20
7811 7811	9002 9003	5	37	37	37	171	182	31
7811	9004	5	57	57	<b>57</b>	137	150	22 20
7811	9005	21	150	150	150 37	172 180	179 186	30 21
7811	9006	<b>4</b> 8	37 92	37 92	37 92	143	167	
7811 7811	9007 9008	9	92 94	94	85	166	182	
7811 7811	9010	23	286	286	286	153	178	
<i>7</i> 811	9011	5	54	54 ~~	54 27	127 164	159 197	
7811	9012	2 1	27 6	27 6	27 6	-45	68	104
7831 7831	8310 8311	4	39	3 <b>9</b>	39	3	106	81
7831	8706	3	17	7	7	-32	36 77	14
7831	8707	30	276	101	101 139	-3 8	27 56	3 5
7831 7831	8708 8709	28 22	215 257	139 128	128	-18	44	3 7
7831 7831	8906	12	92	92	92	19	72	7
7831	8907	16	129	124	1 <b>24</b>	5	64	-6 0
7831	8908	9	81 ~~	81 25	81 25	61 33	70 41	-19
7831 7831	8909 8910	3 12	25 133	25 133	133	-106	121	-2 3
7831 7831	9006	9	75	<i>7</i> 5	<i>7</i> 5	-71	106	3
7831	9007	24	488	247	247	-90 94	109 101	
7831	9008	6 7	58 90	58 74	58 74	-86 26	37	14
7833 7833	7904 7905	10	134	109	109	20	25	19
7833	7906	11	120	117 84	117	20 15 1	29 24	19
7833	7907	8	85	84	84	1	24	20
7833	7908 7909	11 8 5 8	60 66	56	56	33	36	27
7833 7833	7910 7910	22	234	183	183	12 33	22	27 23 24
7833	7911	22 3 6	234 22 73 21 18 5	183 13	13	33	41	24
7833	7912	6	73 21	<b>44</b> 13	<b>44</b> 13	12 12	24 15	22 17
7833 7833	8002 8003	6 2	18	13	13	12 33	39	28 63
7833 7833	8004	3	5	1	1	61	0	63
7833 7833	8005	2	29 24	29	29 20	23 -28	26 35	33 -29
7833	8008	2 6	24 99	20 89	20 89	-40 -9	35 19	-4
7833 7833	8009 8010	4	64	5 <del>9</del>	59	-9 -15	39	-11
7833	8204	8	76	56	56	-10	17	5
7833 7833	8205	6	<i>6</i> 9	64	64 77	<del>-4</del> -2	18 30	3
7833	8206 8207	9	112	77	//	-4	3.0	7
7833 7833	8207 8209	8	86	66	66	6	31	
7833 7833	8210	8	103	42	42	11	27 20	18
7833 7833	8211	6	84	27	27 67	0	20 26	12 -4
7833	8212	7 2	105 28	67 27	& 27	1 2	23	-4 5
7833 7833	8301 8302	10	163	163	163	-1 <b>7</b>	28	-13 3 -16
7833 7833	8303	3 2	<b>4</b> 5 17	45 17	45 17	-17 7 -13	21 61	3
,000	8304							

Station	<b>.</b>	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng r. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
			180			(5557)		(/
7833	8305	2	26	26	26	-2	24	30
7833 7833	8309 8310	3 8	30 76	30 30	30 30	-8 3	21 22	-2 11
7833	8403	4	37	33	33	3 5	16	6
7833	8404	25	301	234	234	-5 17	14	-1 20
7833 7833	8405 8406	10 7	1 <b>27</b> 68	104 45	104 <b>4</b> 5	17 <b>4</b>	20 12	20 12
7833	8407	5	47	42	42	9	15	9
7833 7833	8408 8410	6 3	83 41	56 33	56 33	1 3	14 14	3 9
7833	8411	4	56	39 39	39	- <b>1</b>	16	0
7833	8502		••	**	**			-6
7834 7834	7807 7808	4 13	30 106	30 106	30 106	-1 <b>7</b> 8	31 15	3 4
7834	7809	2	14	14	14	-1	29	17
7834	7810 7902	9	62 7	62 7	62	-2 -10	29 29	-11 -80
7834 7834	7902 7903	3 2	9	9	7 9	-10 -16	20	-00 -26
7834	7904	1	3	3	3	13	15	-29
7834 7834	7905 7906	8 19	56 158	55 157	55 157	-18 -2	25 20	-39 -17
7834	7907	2	11	11	11	-19	22	-27
7834	8001	2	9	9	9	7	8	1
7834 7834	8002 8003	13 5	58 41	56 40	55 40	16 <b>2</b> 0	23 21	19 18
7834	8010	1	8	8	8	13	15	-12
7834 7834	8103 8104	8 14	<b>4</b> 7 112	47 112	47 111	7 -1	23 17	5 -1
7834 7834	8106	6	. 28	28	28	-1 -6	8	-1 -17
7834	8107	2	8	8	8	-6	13	-5
7834 7834	8109 8203	7 5	29 21	29 21	29 21	5 5	12 12	0 13
7834	8204	23	154	123	123	3	10	9
7834 7834	8205 8206	19 5	121 32	93 12	93 12	-3 -7	9 12	0
7834	8207	17	128	128	128	4	8	-6
7834	8208	18	117	117	117	3	10	-1
7834 7834	8209 8210	27 20	261 142	256 138	256 138	3 2	10 10	3 3
7834	8211	11	110	110	109	ō	12	-2
7834 7834	8212 8302	9	85	85	85	3	7	-6 -5
7834 7834	8303	5	32	32	32	3	10	-3 -3
7834	8304	3	27	27	27	-3	9	-8
7834 7834	8305 8308	3 1	20 4	20 4	20 4	-1 -1	5 2	- <b>4</b> 0
7834	8309	5	36	36	36	-2	8	-3
7834 7834	8310 8311	20 23	236 275	236 275	236 275	1 -1	6 5	-4 2
7834	8312	13	155	155	155	3	6	-5 -5
7834	8401	8	93 256	91 252	91	0	8	-3 -4 -3 -5 -7 -2
7834 7834	8402 8403	32 42	356 419	353 363	353 363	1 6	8 9	-2 - <b>4</b>
7834	8404	26	299	250	247	7	10	0
7834	8405	30 31	328	316	316	7	8	0
7834 7834	8406 8407	21 28	227 323	197 308	197 308	5 2	7 8	-1 1
7834	8408	31	383	350	350	5	10	1
7834 7834	8409 8410	20 21	175 202	156 1 <b>7</b> 9	156 178	6 3	10 9	-1 -1
7834	8411	24	291	283	283	3 7	9	3
7834	8412	4	49	31	31	10	12	11
7834 7834	8502 8503	3 2	21 <i>2</i> 7	15 27	15 27	11 -9	12 12	-1 -3
7834	8504	10	113	111	111	5	6	-3
7834	8505	6	56	55	55	-3	6	-6
7834 7834	8506 8507	11 27	120 432	113 430	113 430	-3 1	10 7	-7 -5
7834	8508	24	298	295	295	4	11	-3
7834	8509	37	490	489	489	4	11	-3

Station		No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual	Residual	Estimate
1 ( a mi b c i						(cm)	(cm)	(cm)
							_	
7834	8510	40	497	486	486	3 5	10 11	-2 2
7834	8511	5	.55 120	55 128	55 1 <b>28</b>	0	5	-2
7834	8512	1 <b>1</b> 7	129 <i>7</i> 1	71	71	1	7	-1
7834 7834	8601 8602	18	205	196	196	5	10	3
7834 7834	8603	19	217	216	216	3	9	1 -4
7834	8604	17	213	213	213	2 0	6 8	-4
7834	8605	10	124	95 22	94 23	1	9	-4
7834	8606	3 2	23 18	23 18	16	-12	17	
7834	8607 8608	2	10	10				-12
7834 7834	8609	2	22	22	22	-4	6	2
7834	8610	13	164	151	151	6	8 8	-3
7834	8611	16	203	194	194 174	7 -2	° 7	
7834	8612	15	181	1 <b>74</b> 11	11	16	17	4
7834	8701	1 6	11 50	46	46	-3	3	0
7834 7834	8702 8703	8	64	61	61	11	13	2
7834 7834	8704	5	39	38	38	0	6 m	-4 4
7834	8705	9	98	98	81	20 1	22 8	-1
7834	8706	8	71	63 204	63 306	8	10	i
7834	8707	29 20	309 206	306 206	206	7	8	0
7834	8708 8709	20 25	206 221	215	215	6	8	-1
7834 7834	8710	29	321	298	298	4	7	<b>-4</b> 0
7834	8711	19	205	186	186	8	12 12	3
7834	8712	6	34	34	34 56	11 5	6	3
7834	8801	5	56 27	56 34	36 34	8	11	1
7834	8802 8803	5 1	37 5	5	5	11	13	-1
7834 7834	8804	5	4 <u>9</u>	34	34	4	6	-1
7834	8805	3	29	29	29	0	5 7	-5 - <b>4</b>
7834	8806	2	16	16	16 81	<b>2</b> 5	11	-2
7834	8807	11	1 <b>2</b> 0 1 <b>4</b> 0	81 138	138	2	5	-2 -3
7834 7934	8808 8809	10 12	146	93	93	0	5	-4
7834 7834	8810	12	130	112	109	2	7	-4 -4
7834	8811	16	166	113	112	1	10 7	1
7834	8901	<b>2</b> 0	235	235 109	235 109	6 8	ý	5
7834	8902	11 13	112 143	118	118	ĭ	7	5 -2
7834 7834	8903 8904	16	176	143	143	5	8	-1
7834 7834	8905	9	88	86	86	3	6	-2 -2
7834	8906	9	94	65	65 20	1 -2	10 12	-2 -7
7834	8907	2	20 8	20 8	20 0	-2 -48	53	-1
7834	8908	1 10	114	103	89	- <b>48</b> 5	13	-5
7834 7834	8910 8911	9	102	67	<b>67</b>	8	11	6
7834	8912	4	58 42	58	58	-6	8 16	-6 -2
7834	9001	3	42	41	35 90	9 0	11	-1
7834	9002	13	132 347	90 286	90 286	3	9	-1 -5 6 -6 -2 -1 -3 -9 -2 -3
7834 7834	9003 9004	31 13	138	33	30	-1	16	-9
7834 7834	9004	20	189	113	113	2	13 5	-2
7834	9006	5	30	8	8	-3 15	5 240	-3
7834	9007	20	202	202	201 304	15 -2	240 21	
7834	9008	26 22 22 5	305 265	305 265	265	1	21 8	
7834 7834	9009 9010	<i>∠</i> ∠ 27	205 198	198	198	5	10	
7834 7834	9010	5	198 58	58	58	-7	15	
7834	9012	4	43	43	43	-3 16	9 21	19
7835	7907	1	6	6	6	16	∠1	17
7835 7835	7908	7	43	57	57	29	33	16
7835	7909	6	73 27	20	20 20	34	39	23 -12
7835 7835	7911 7912	2 2	27 23	23	23	-12	15	-12
7835 7835	8009	10	105	55	55	1	24	-4
7835	8010	22	305	298	292	13	30 26	9 18
7835 7835	8011	1 1	12	12	12 8	22 -26	26 29	-4 9 18 -30
7835	8109	1	8	8	o	-20	_	

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
		1 23000			_ j	(cm)	(cm)	(cm)
7835	8110	2	20	20	20	-15	18	-18
7835	8205	2 5	<i>6</i> 7	<i>6</i> 7	<del>59</del>	-12	25	-20
7835	8206	9	122	96	90	-23	29	
7835	8207	7	58	46	46	-30	53	-22
7835 7835	8208 8209	9 16	145 296	131 296	123 275	-21 -56	44 99	-27 -22
7835	8210	10	250	290	2/3	-50	77	-22 -56
7835	8312	1	6	6	6	17	19	11
7835	8403	3	22					
7835	8404	11	89					
7835 7835	8405 8406	3 14	45 146					
7835 7835	8407	26	314					
7835	8408	8	86					
7835	8409	13	115					
7835	8410	21	264	135	135	2	5	1
7835	8411	11	129	128	125	7	11	4
7835 7835	8412 8501	14 7	214 70	207 70	204 <i>6</i> 9	6 <b>4</b>	9 7	3 2
7835	8502	7	118	118	113	4	8	4
7835	8503	8	130	130	127	4	10	i
7835	8504	17	250	234	231	1	9	0
7835	8505	7	99	99	99	-1	5	-1
7835	8506	17 ~7	293	278	273	2	13	1
7835 7835	8507 8508	27 30	4 <del>69</del> 577	434 576	433 566	1 3	8 10	-4 -3
7835	8509	32	652	652	638	<del>-6</del>	13	-7
7835	8510	32	609					-7 -6
7835	8511	15	238					-5 -5
7835	8512	18	265	11	••	•	10	-5
7835 7835	8601 8602	4 1	61 16	11 16	11 16	-1 2	10 8	-9 -5
7835	8603	5	62	43	42	-6	11	-3 -4
7835	8604	7	68	31	31	-6	9	-11
7835	8605	6	60	6	6	-9	10	
7835	8606	1	11	11	8	-4	6 ~	-14
7835 7835	8607 8608	13 4	141 <i>6</i> 6	17 13	16 13	0 -1	22 8	-5
7835	8609	7	115	68	66	8	10	-5
7835	8610	10	104	32	29	14	20	5
7835	8611	20	288	132	120	6	10	
7835	8612	28	611	561	471	4	10	3
7835 7835	8701 8702	10 24	209 443	209 393	175 340	7 5	14 13	2 3
7835	8703	19	321	240	222	1	6	0
7835	8704	28	522	317	301	10	13	4
7835	8705	23	372	331	301	16	19	7
7835	8706	14	210	185	176	7	10	2
7835 7835	8707 8708	6	100	100	94	11	12	3 -1
7835	8711	25	430	399	381	6	10	-1
7835	8712	48	812	656	614	-2	10	-5
7835	8801	36	752	532	471	6	16	-1
7835 7835	8802 8803	37 67	624	393	393	3	8	4
7835 7835	8804	3	1212 38	718 38	718 38	<b>4</b> 6	7 10	1 1
7835	8805	22	350	290	273	6	8	1
7835	8806	41	677	618	5 <b>7</b> 8	5	11	1
7835	8807	<u>55</u>	1021	887	<i>7</i> 97	7	12	0
7835 7835	8808 8809	71 71	1239 1292	11 <i>7</i> 7 1252	1062	4	6	-1 0
7835 7835	8810	71 60	924	924	11 <b>2</b> 5 869	7 5	16 17	0 2
7835	8811	60	1170	1170	1012	5	14	4
7835	8812	60	1152	817	717	7	10	2
7835	8901	82	1603	1603	1434	4	13	2
7835	8902	<i>6</i> 7	1240	1240	1088	5	12	4
7835 7835	8903 8904	73 18	1292	1287	1181	3 7	14	0
7835 7835	890 <del>4</del> 8905	18 58	268 865	268 865	251 825	6	13 14	3 2
, ~~	8906	51	699	699	660	~	24	2

Number	Date	Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Residual	Residual	Estimate
			<u>.</u>			(cm)	(cm)	(cm)
	-			<b>604</b>	<b>(50</b>	1	23	-6
7835	8907	51 27	684 508	684 502	658 485	1 -3	24	-1
7835	8908 8909	37 45	592	592	568	8	16	5
7835 7835	8910	71	1331	1342	1240	5	10	0
7835	8911	38	<i>7</i> 31	731	667	6	11 <b>2</b> 0	3 10
7835	8912	27	486	476	446 1120	15 <b>483</b>	130 <b>47</b>	1
7835	9001	71 42	1257 <i>7</i> 74	1257 774	1120 719	-2	16	3
7835	9002 9003	42 41	631	631	604	5	16	0
7835 7835	9004	34	608	608	561	7	25	7
7835	9005	53	863	863	818	3	17 14	3 4
7835	9006	<u>64</u>	965	965	928 1262	3 0	23	*
7835	9007	75 69	1334 1139	1334 1139	1089	3	9	
7835	9008 9009	59	1017	1017	947	6	12	
7835 7835	9010	28	432	432	411	6	14	
7835	9011	57	953	953	898	9	56 10	
7835	9012	41	616	616	586	2 -35	19 39	-52
7837	8311	3	19 17	6 15	6 15	-33 4	19	4
7837	8312 8402	7 1	5	5	5	43	49	31
7837 7837	8406	1	2	2	2	17	26	40
7837	8407	i	1		_		~	21
7837	8408	6	18	15	15	-14 29	29 46	-21 -23
7837	8409	1	3	2 102	2 102	-1	16	-15
7837	8410	14 4	144 <i>2</i> 7	15	15	-2	22	-19
7837 7837	8411 8703	3	32	14	14	-18	23	-27
7837	8704	1	9	9	9	-24	26	-47 22
7837	8705	3	25	11	11	-27	30	-33
7837	8711	3	18					
7837	8712 8801	12 1	77 6					
7837 7837	8804	1	3	3	3	-10	14	<b>-4</b> 1
7837	8805	i	15				40	21
7837	8806	4	28	14	14	-6	13 5	-21 -18
7837	8809	7	46 45	29 34	29 34	0 <b>2</b> 5	34	4
7837	8810 8811	6 11	%5 86	86	86	-25	36	-28
7837 7837	8812	6	34	37	34	-64	1097	-15
7837	8910	2	7	7	7	1	34 12	-28 -9
7837	8911	10	82	82 67	82 66	2 -14	56	-21
7837	8912	10	67 233		232	-9	65	
7837 7838	9012 8204	19 15	233 131	233 131 32	131 32	6	15	7 5
<b>7838</b>	8205	15 5	32	32	32	-1	10	5
7838	8206	1	131 32 3 7	-	7	-7	13	
7838	8208	2	7	7	,	-/	13	18
7838 7838	8209 8210	5	33	23	22	8	41	
7838	8211	2	3 86	23 3	22 3	-11	18	16
7838	8212	15	86	86	86	-3 8	10	-165 14
7838	8301	12	73 99	73 76	<b>70</b> 55	8 28	16 <b>4</b> 8	7
7838	8302 8303	13 11	99	76 94	94	13	22	18
7838 7838	8304	1	5	5	5 7	14	17	35
7838	8305	3	94 5 7 7	7	7_	14 -5 -6	18	-4 4
7838 7838	8306	3	7	7	7 3	-6 1=	10 20	23
7838 7838	8307	1	3 66	3 66	65	15 13 19 3	16	14
7838 7838	8308 8309	11 3	900 17	17	17	19	21	27 13
7838 7838	8310	23	17 168	168	168	3	11	13
7838	8311	24	203	201	201 290	4	8	12 7 15
7838	8312	33	290	290	290	5	9 13	/ 15
7838	8401	11	72 110	<i>69</i> 96	68 96	9 7	13 14	21
7838	8402	18 30	110 2 <del>69</del>	214	212	-7	16	-4
/838 7838	8403 8404	30 11	71	<i>7</i> 1	70	-5	14	5
7838 7838 7838 7838 7838 7838 7838	8405	16	101 64	96	96	-5 2 5	6	21 -4 5 9
7829	8407	9	64	62	62	5	12	9

Station	D-1-	No. of	Observ.	Obs. after	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
Number	Date	Passes	Acquired	Eng r. East	Dynam. Edit	(cm)	(cm)	(cm)
						·····		
7838	8408	28	202	189	188	2	11	12
7838 7838	8409 8410	21 23	251 329	243 312	243 309	2 -2	11 9	8 4
7838 7838	8411	23 29	325 335	315	315	1	9	9
7838	8412	25	261	179	179	3	12	11
7838	8501	29	279	277	277	4	8	11
7838	8502	13	127	125	124	-1 -6	11 7	8 4
7838 7838	8503 8504	4 20	35 252	31 243	31 2 <b>4</b> 3	-6 1	8	6
7838	8505	21	277	256	256	-2	7	5
7838	8506	3	45	44	44	-10	13	3
7838	8507	20	260 520	238	237	4	8	4 5
7838 7838	8508 8509	39 25	539 <b>422</b>	500 402	498 400	-2 -8	12 13	0
7838	8510	22	321	304	303	-5 -5	17	i
7838	8511	48	731	683	682	0	10	6
7838	8512	52	805	<b>741</b>	726	-2	8	5
7838 7838	8601 8602	43 35	619 511	584 466	576 465	-1 0	9 9	<b>4</b> 5
7838	8603	28	506	463	462	-4	10	š
7838	8604	21	322	306	306	-4	9	2
7838	8605	13	216	172	172	-3	6	
7838 7838	8606 8607	5 1	74 18	44 15	<b>44</b> 10	-7 -25	14 28	4
7838	8608	11	107	61	61	-23 -7	13	5
7838	8609	11	113	101	97	0	11	
7838	8610	14	161	151	151	-3	9	16
7838 7838	8611 8612	15 30	188 501	161 394	161 3 <b>7</b> 9	-4 2	9 9	2
7838	8701	18	306	267	267	-1	8	5
7838	8702	26	343	335	334	-4	15	5
7838	8703	14	194	<b>7</b> 0	<b>7</b> 0	2	8	7
7838 7838	8704 8705	4 6	5 <del>9</del> 57	35 26	35 26	-4 -9	7 11	6 6
7838	8706	10	87	63	62	1	8	8
7838	8707	7	85	76	<i>7</i> 3	6	11	9
7838	8708	12	119	97 122	97	1	6	8
7838 7838	8709 8710	13 14	174 177	133 138	128 136	4 4	9 8	9 8
7838	8711	5	56	48	46	ż	14	7
7838	8712	30	496	383	382	-4	8	5
7838	8801	17	189	<i>7</i> 3 94	63 94	-7	15 5	8 10
7838 7838	8802 8803	18 4	191 57	43	<del>94</del> 41	1 8	10	8
7838	8804	6	91	70	÷	7	10	10
7838	8805	4	67	58	55	4	8	8
7838	8806	4	<b>47</b> 85	42	42 52	5	7 21	10
7838 7838	8807 8808	6 8	93	62 71	62 62	9 -4	21 9	7 3
7838	8809	8	115	60	51	<u>.</u> ق	17	1
7838	8810	10	168	86	68	3	15	12
7838 7838	8811 8812	11 9	183 134	119	113 <i>6</i> 7	-1 -	12 9	3 7
7838	8901	9	155	68 116	113	5 -6	11	-2
7838	8902	10	139	98	98	-2	9	-2 6 7
7838	8903	9	113	82	82	3	8	
7838	8905	7	135	63 57	63	0	11 17	8
7838 7838	8906 8907	7 3	135 39	57 31	57 31	-7 -6	17 8	4 9
7838	8908	5	64	31	31	-3	15	13
7838	8910	7	<i>7</i> 7	<i>7</i> 7	<i>7</i> 3	4	11	9
7838	8911	11	142	142	112	10	16	15
7838 7838	8912 9001	14 10	240 137	184 <i>7</i> 6	174 <i>7</i> 6	5 3	13 10	11 8
7838	9001	6	93	80 80	76 80	6	14	0 11
7839	8309	6	74	<i>7</i> 4	74	ő	9	-1
7839	8310	26	313	313	273	-6	19	0
7839	8311	14 14	170	170	170 156	-4 1	6	-2 1
7839 7839	8312 8401	14 24	156 229	156 226	156 226	-1 2	5 6	-1 -1
7007	OTOI	27	<i></i> /	220	220	<b>-</b>	J	-1

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
					•	(cm)	(cm)	(cm)
7920	8402	11	148	148	148	0	3	1
7839 7839	8403	12	132	132	132	8	9	-1
7839	8404	11	137	137	137	0	4	-1
7839	8405	8	100	100	100	2 -2	5 5	-1 -3
7839	8406	11	142 201	142 201	142 201	-2 -1	6	ő
7839 7839	8407 8408	19 10	201 93	93	93	2	10	2
7839	8409	13	128	128	128	1	7	-1
7839	8410	4	32	32	32	8	11	0
7839	8411	1	11	11	11 7	-8 -3	9 <b>4</b>	-3 5
7839	8501 8502	1 7	7 75	<i>7</i> <i>7</i> 5	<i>7</i> 5	3	9	5 2
7839 7839	8503	4	33	31	31	-5	6	0
7839	8504	10	135	135	135	2	8	-1
7839	8505	8	92	92 24	92 21	-3 12	5 13	-1 -5
7839	8506	3	31 323	31 323	31 323	-12 5	11	1
7839 7839	8508 8509	26 28	323 331	329	329	1	10	1
7839 7839	8510	1	14	14	14	-19	20	-15
7839	8601	19	233	233	233	-1	5	0
7839	8602	10	103	103	103	4 4	9 8	0 0
7839	8603	10 17	130 222	130 222	130 222	1	7	-1
7839 7839	8604 8605	17 10	137	130	130	i	4	
7839 7839	8606	4	31	29	29	-4	11	-1
7839	8607	1	8	8	8	-8	11	-8
7839	8608		50	50	50	-2	4	-0
7839	8609	4 13	50 140	50 134	134	2	6	-1
7839 7839	8610 8611	15 15	215	201	201	2	5	
7839	8612	21	252	228	228	0	10	•
7839	8701	15	188	186	186	-2 -3	8 14	<i>-</i> 2 -1
7839	8702	32 35	362 251	361 225	361 225	-3 -6	12	-3
7839 7839	8703 8704	25 22	351 235	198	198	6	10	-2
7839 7839	8705	17	207	185	185	-7	11	-4
7839	8706	12	125	119	119	2	6	-1 1
7839	8707	29	319	319 201	319 201	<b>4</b> 3	6 <b>4</b>	0
7839 7839	8708 8709	14 25	201 327	325	325	2	5	0
7839 7839	8710	10	143	129	129	3	6	-2 -2
7839	8711	15	165	161	161	2	7	-2 0
7839	8712	11	150	133	133	0 3	6 10	5
7839	8801	14	229 80	63	216 63	5	10	1
7839 7839	8802 8803	6 5	82 52	52	63 52	5 -2 0	7 2	1
7839	8804	3	35	35	35	0	2	1
7839	8805	1	12	47	<i>A</i> 1	-4	5	-3
7839	8806	5 13	53 180	41 1 <b>7</b> 1	41 163	4	11	0
7839 7839	8807 8808	13 21	341	300	300	0	4	-1
7839	8809	17	274	271	213	0	15 12	-1 2
7839 7839	8810	21	343	259	216 122	-4 1	13 8	-2 2 0
7839	8811	15 31	<b>25</b> 5 550	122 408	122 408	3	8	ō
7839 7839	8812 8901	14	230 230	230	222	-3	10	0
7839 7839	8902	22	333	333	333	-5	12	1
7839	8903	16	218	218	218	-1	11	0 -2
7839	8904	13	156	156	156 168	-2 1	8 7	0
7839	8905 8006	10 1	168 9	168 9	168 9	17	19	-18
7839 7839	8906 8907	1	8	8	8	-3	3	-12
7839 7839	8910	17	251	191	191	1	6	0
7839	8911	15	214	149	149	-1	7 9	2 -1
7839	8912	15	265	210	210 183	-4 2	10	-1 -2
7839 7830	9001	14 21	183 338	183 315	315	2 6	12	-2 3 0
7839 7839	9002 9003	17	204	192	192	2	9	0
,,		1	9	9	9	20 -7	24	9 -3
7839	9004	15	250	242	242	-	13	•

Station	<b>5</b>	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
		<del></del>				(CIII)	(CIII)	(CIII)
7839	9006	1	4	4	4	13	15	13
7839	9007	7	87	87	87	-4	7	
7839 7830	9008	25	400	400	400 m	-3	6	
7839 7839	9009 9010	11 <b>23</b>	83 259	83 259	83 259	0 - <b>4</b>	6 12	
7839	9011	14	173	173	173	2	11	
7839	9012	16	261	261	256	-2	14	
7840	8304	5	56	56	56	-3	9	-6
7840 7840	8306 8310	3 <b>2</b> 0	34 198	34 197	34 197	- <b>4</b> -1	13 7	-4
7840	8311	14	161	160	159	0	8	1 2
7840	8312	14	187	187	187	š	š	4
7840	8401	16	184	184	181	6	10	3
7840 7840	8402	30	360	353	353	-1	7	2
7840 7840	8403 8404	17 36	172 374	172 3 <del>69</del>	172 3 <del>69</del>	3 3	8 7	-1 3
78 <b>4</b> 0	8405	10	96	94	94	3	7	1
7840	8406	26	268	254	254	1	5	i
7840	8407	50	611	586	585	1	9	1
7840 7840	8408 8409	30 34	399	390	390	3	8	2
7840 7840	8410	34 40	416 550	377 546	377 545	3 1	8 8	2 1
78 <b>4</b> 0	8411	38 38	489	483	483	-1	8	2
7840	8412	43	556	536	536	<u>-2</u>	9	ō
7840	8501	36	506	506	506	1	7	0
7840 7840	8502 8503	43 29	541 295	527 266	526	0	8	-1
7840	8504	17	205	200 179	266 179	-2 -1	8 5	-1 -3
7840	8505	<u></u>	138	133	133	- <b>i</b>	6	<b>-</b> 4
7840	8506	15	153	142	142	-3	9	-1
7840 7840	8507	49 ~~	598	597	597	-4	8	-4
7840 7840	8508 8509	30 52	356 728	356 709	356 709	3 -3	11 12	-3 0
7840	8510	39	539	531	531	0	9	-2
<b>784</b> 0	8511	37	498	492	492	-3	8	-2
7840	8512	18	253	251	251	-2	7	-2
7840 7840	8601 8602	49 36	737 503	732 482	732 483	0 -1	7	0
7840	8603	36 43	595	402 570	482 570	-1 -1	7 7	0 -1
7840	8604	45	486	465	465	i	8	-1
7840	8605	38	432	331	331	0	6	
7840 7840	8606	37 38	360	253	248	-1	8	-5
7840 7840	8607 8608	38 46	378 568	200 510	200 510	4 1	9	4
7840	8609	49	562	503	510 503	3	5 <b>6</b>	-6
<b>784</b> 0	8610	43	5 <b>17</b>	477	477	2	6	-2
7840 7840	8611	34 50	510	447	447	2	5	_
7840 7840	8612 8701	50 22	715 260	597 235	597 235	2 -4	7 8	-1 -4
7840	8702	46	651	638	635	2	16	-1
7840	8703	38	565	499	49 <del>9</del>	ō	5	- <b>i</b>
7840 7840	8704	50	616	449	449	6	10	-1
7840 7840	8705 8706	54 28	762 353	6 <b>43</b> 311	643 311	1	7	-2
7840	8707	49	5 <b>79</b>	306	306	0 1	7 6	-2 -1
7840	8708	39	527	461	461	3	6	1
7840	8709	37	468	396	396	1	6	-1
7840 7840	8710 8711	32 29	365 409	283	283	0	5	-4
7840 7840	8712	28	368	264 246	264 244	2 1	7 8	-2 -1
7840	8801	35	485	354	354	1	5	-1 -1
7840	8802	58	823	705	705	-1	5 7	-2
7840	8803	35	430	367	367	1	5	0
7840 7840	8804 8805	40 25	487	342 236	337 236	-1	5	-1
7840 7840	8806	22	283 240	236	236 206	0 1	4 6	-1 0
7840 7840	8807	34 34	365	192	192	2	7 7	-1
7840	8808	49	563	358	358	1	4	0
7840	8809	36	433	291	291	-3	6	-2
7840	8810	61	<i>7</i> 34	425	<b>42</b> 0	4	9	4

Number         Date           7840         8811           7840         8912           7840         8902           7840         8903           7840         8904           7840         8905           7840         8908           7840         8908           7840         8909           7840         8910           7840         8911           7840         8912           7840         9001           7840         9002           7840         9005           7840         9006           7840         9007           7840         9009           7840         9009           7840         9009           7840         9009           7840         9009           7840         9001           7840         9009           7840         9001           7843         8505           7843         8506           7843         8507           7843         8601           7843         8602           7843         8604           7843<	Passes		T	Damam Edit	Residual	Residual	Estimate
7840         8812           7840         8901           7840         8902           7840         8903           7840         8906           7840         8906           7840         8908           7840         8909           7840         8910           7840         8911           7840         8912           7840         9001           7840         9005           7840         9005           7840         9006           7840         9006           7840         9007           7840         9006           7840         9007           7840         9009           7840         9009           7840         9001           7840         9001           7840         9001           7840         9001           7840         9001           7840         9010           7843         8505           7843         8506           7843         8507           7843         8501           7843         8601           7843 <th>1 45565</th> <th>Acquired</th> <th>Engr. East</th> <th>Dynam. Edit</th> <th>(cm)</th> <th>(cm)</th> <th>(cm)</th>	1 45565	Acquired	Engr. East	Dynam. Edit	(cm)	(cm)	(cm)
7840         8812           7840         8901           7840         8902           7840         8903           7840         8906           7840         8906           7840         8908           7840         8909           7840         8910           7840         8911           7840         8912           7840         9001           7840         9005           7840         9005           7840         9006           7840         9006           7840         9007           7840         9006           7840         9007           7840         9009           7840         9009           7840         9001           7840         9001           7840         9001           7840         9001           7840         9001           7840         9010           7843         8505           7843         8506           7843         8507           7843         8501           7843         8601           7843 <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>							
7840 8901 7840 8902 7840 8903 7840 8904 7840 8904 7840 8905 7840 8906 7840 8906 7840 8909 7840 8910 7840 8911 7840 8912 7840 9011 7840 9002 7840 9005 7840 9005 7840 9006 7840 9006 7840 9007 7840 9006 7840 9011 7840 9010 7840 9011 7843 8505 7843 8506 7843 8506 7843 8511 7843 8511 7843 8511 7843 8512 7843 8601 7843 8601 7843 8601 7843 8606 7843 8606 7843 8607 7843 8606 7843 8606 7843 8607 7843 8606 7843 8607 7843 8606 7843 8607 7843 8606 7843 8607 7843 8607 7843 8606 7843 8607 7843 8607 7843 8608 7843 8607 7843 8608 7843 8609 7843 8611 7843 8611 7843 8612 7843 8705 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8903 7843 8903 7843 8903 7843 8905 7843 8903 7843 8905 7843 8906 7843 8906 7843 8907	64	935	746	724	2	10 6	4
7840 8902 7840 8903 7840 8904 7840 8905 7840 8906 7840 8907 7840 8908 7840 8909 7840 8910 7840 8911 7840 8912 7840 9001 7840 9001 7840 9005 7840 9005 7840 9006 7840 9006 7840 9007 7840 9008 7840 9007 7840 9008 7840 9011 7843 8505 7843 8506 7843 8507 7843 8511 7843 8511 7843 8601 7843 8601 7843 8601 7843 8602 7843 8601 7843 8606 7843 8607 7843 8606 7843 8607 7843 8606 7843 8607 7843 8606 7843 8607 7843 8606 7843 8607 7843 8607 7843 8606 7843 8607 7843 8607 7843 8608 7843 8607 7843 8608 7843 8607 7843 8608 7843 8607 7843 8608 7843 8609 7843 8609 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8600 7843 8700 7843 8700 7843 8700 7843 8700 7843 8700 7843 8700 7843 8700 7843 8700 7843 8700 7843 8700 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8800 7843 8905 7843 8905 7843 8905 7843 8905 7843 8905 7843 8905 7843 8906 7843 8905	28	396	277	277 388	3 2	6	2 2
7840         8903           7840         8904           7840         8904           7840         8906           7840         8908           7840         8909           7840         8910           7840         8911           7840         8912           7840         9001           7840         9005           7840         9006           7840         9006           7840         9008           7840         9009           7840         9010           7840         9011           7843         8505           7843         8505           7843         8507           7843         8509           7843         8501           7843         8601           7843         8602           7843         8603           7843         8604           7843         8605           7843         8606           7843         8606           7843         8606           7843         8606           7843         8606           7843 <td>40</td> <td>527 470</td> <td>388 331</td> <td>331</td> <td>1</td> <td>5</td> <td>3</td>	40	527 470	388 331	331	1	5	3
7840         8904           7840         8905           7840         8906           7840         8908           7840         8909           7840         8910           7840         8911           7840         8912           7840         9001           7840         9005           7840         9005           7840         9006           7840         9008           7840         9009           7840         9010           7840         9011           7843         8505           7843         8506           7843         8506           7843         8511           7843         8601           7843         8602           7843         8603           7843         8604           7843         8605           7843         8606           7843         8606           7843         8607           7843         8606           7843         8607           7843         8606           7843         8607           7843 <td>40 34</td> <td>470 435</td> <td>285</td> <td>285</td> <td>i</td> <td>8</td> <td>0</td>	40 34	470 435	285	285	i	8	0
7840 8905 7840 8906 7840 8906 7840 8907 7840 8908 7840 8909 7840 8910 7840 8911 7840 8912 7840 9001 7840 9002 7840 9005 7840 9006 7840 9006 7840 9006 7840 9010 7840 9010 7840 9011 7843 8505 7843 8505 7843 8506 7843 8511 7843 8511 7843 8512 7843 8601 7843 8602 7843 8605 7843 8606 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8607 7843 8608 7843 8607 7843 8609 7843 8611 7843 8611 7843 8611 7843 8611 7843 8610 7843 8610 7843 8610 7843 8701 7843 8702 7843 8703 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8707 7843 8706 7843 8707 7843 8706 7843 8707 7843 8708 7843 8709 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8901 7843 8903 7843 8903 7843 8903 7843 8903 7843 8903 7843 8905 7843 8906 7843 8906 7843 8906 7843 8906	28	313	210	210	2	6	1
7840         8906           7840         8907           7840         8908           7840         8909           7840         8910           7840         8911           7840         901           7840         9002           7840         9005           7840         9006           7840         9006           7840         9009           7840         9010           7840         9011           7843         8505           7843         8506           7843         8507           7843         8509           7843         8511           7843         8601           7843         8602           7843         8603           7843         8604           7843         8605           7843         8606           7843         8606           7843         8607           7843         8608           7843         8609           7843         8601           7843         8607           7843         8608           7843 <td>68</td> <td>715</td> <td>531</td> <td>531</td> <td>0</td> <td>6</td> <td>-1</td>	68	715	531	531	0	6	-1
7840 8907 7840 8908 7840 8908 7840 8909 7840 8910 7840 8911 7840 8911 7840 9001 7840 9001 7840 9003 7840 9005 7840 9006 7840 9006 7840 9007 7840 9010 7840 9011 7843 8505 7843 8506 7843 8506 7843 8511 7843 8511 7843 8511 7843 8601 7843 8602 7843 8603 7843 8606 7843 8607 7843 8606 7843 8607 7843 8601 7843 8601 7843 8601 7843 8601 7843 8601 7843 8601 7843 8602 7843 8601 7843 8606 7843 8607 7843 8606 7843 8607 7843 8608 7843 8607 7843 8608 7843 8607 7843 8608 7843 8607 7843 8608 7843 8609 7843 8611 7843 8611 7843 8612 7843 8702 7843 8703 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8706 7843 8709 7843 8706 7843 8808 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8905 7843 8905 7843 8905 7843 8905 7843 8906 7843 8905	59	647	327	327	-1	8	.9 - <b>4</b>
7840         8908           7840         8909           7840         8910           7840         8911           7840         901           7840         9001           7840         9005           7840         9006           7840         9006           7840         9009           7840         9010           7840         9011           7843         8505           7843         8506           7843         8509           7843         8510           7843         8601           7843         8601           7843         8603           7843         8604           7843         8605           7843         8606           7843         8606           7843         8606           7843         8607           7843         8608           7843         8610           7843         8611           7843         8701           7843         8702           7843         8704           7843         8705           7843 <td><i>7</i>5</td> <td><b>76</b>1</td> <td>410</td> <td>410</td> <td>0 -3</td> <td>6 9</td> <td>-1</td>	<i>7</i> 5	<b>76</b> 1	410	410	0 -3	6 9	-1
7840         8910           7840         8911           7840         8912           7840         9001           7840         9003           7840         9006           7840         9006           7840         9008           7840         9010           7840         9011           7843         8505           7843         8506           7843         8507           7843         8509           7843         8510           7843         8601           7843         8602           7843         8603           7843         8602           7843         8603           7843         8604           7843         8605           7843         8606           7843         8606           7843         8606           7843         8607           7843         8609           7843         8701           7843         8704           7843         8705           7843         8706           7843         8706           7843 <td>61</td> <td>631</td> <td>205</td> <td>204</td> <td>ა 0</td> <td>6</td> <td>2</td>	61	631	205	204	ა 0	6	2
7840         8911           7840         8912           7840         9001           7840         9003           7840         9005           7840         9006           7840         9008           7840         9009           7840         9010           7840         9011           7843         8505           7843         8505           7843         8507           7843         8509           7843         8510           7843         8601           7843         8601           7843         8602           7843         8603           7843         8604           7843         8605           7843         8606           7843         8606           7843         8607           7843         8609           7843         8610           7843         8610           7843         8701           7843         8704           7843         8706           7843         8706           7843         8706           7843 <td>36</td> <td>330</td> <td>255 30</td> <td>2<b>4</b>5 17</td> <td>-2</td> <td>2Ŏ</td> <td>2</td>	36	330	255 30	2 <b>4</b> 5 17	-2	2Ŏ	2
7840         8912           7840         9001           7840         9002           7840         9005           7840         9006           7840         9008           7840         9009           7840         9010           7840         9011           7843         8505           7843         8506           7843         8509           7843         8510           7843         8511           7843         8601           7843         8601           7843         8602           7843         8603           7843         8604           7843         8605           7843         8606           7843         8606           7843         8606           7843         8607           7843         8610           7843         8611           7843         8701           7843         8702           7843         8705           7843         8706           7843         8706           7843         8706           7843 <td>40 57</td> <td>381 745</td> <td>662</td> <td>656</td> <td>ī</td> <td>7</td> <td>1</td>	40 57	381 745	662	656	ī	7	1
7840         9001           7840         9002           7840         9003           7840         9006           7840         9006           7840         9008           7840         9010           7840         9011           7843         8505           7843         8506           7843         8509           7843         8510           7843         8511           7843         8601           7843         8602           7843         8603           7843         8604           7843         8605           7843         8606           7843         8606           7843         8607           7843         8608           7843         8610           7843         8611           7843         8701           7843         8702           7843         8706           7843         8706           7843         8706           7843         8706           7843         8706           7843         8706           7843 <td>5/ 9</td> <td>745 86</td> <td>56</td> <td>56</td> <td>6</td> <td>10</td> <td>8</td>	5/ 9	745 86	56	56	6	10	8
7840 9002 7840 9003 7840 9005 7840 9006 7840 9006 7840 9007 7840 9009 7840 9010 7840 9011 7843 8505 7843 8506 7843 8507 7843 8510 7843 8511 7843 8512 7843 8601 7843 8602 7843 8606 7843 8606 7843 8606 7843 8606 7843 8606 7843 8606 7843 8607 7843 8606 7843 8607 7843 8607 7843 8607 7843 8608 7843 8607 7843 8607 7843 8608 7843 8607 7843 8608 7843 8610 7843 8611 7843 8611 7843 8702 7843 8703 7843 8706 7843 8706 7843 8707 7843 8706 7843 8706 7843 8707 7843 8706 7843 8706 7843 8707 7843 8706 7843 8706 7843 8707 7843 8706 7843 8707 7843 8706 7843 8707 7843 8708 7843 8709 7843 8808 7843 8809	17	150	111	111	7	10	2
7840 9003 7840 9005 7840 9006 7840 9006 7840 9007 7840 9008 7840 9010 7840 9011 7843 8505 7843 8506 7843 8507 7843 8511 7843 8512 7843 8601 7843 8601 7843 8602 7843 8603 7843 8606 7843 8606 7843 8606 7843 8606 7843 8607 7843 8606 7843 8607 7843 8607 7843 8607 7843 8607 7843 8608 7843 8611 7843 8611 7843 8612 7843 8701 7843 8702 7843 8703 7843 8702 7843 8703 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8709 7843 8700 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8808 7843 8809 7843 8809 7843 8809 7843 8809 7843 8810 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809	40	450	277	277	-4	12	4
7840 9005 7840 9006 7840 9006 7840 9008 7840 9009 7840 9010 7840 9011 7843 8505 7843 8506 7843 8507 7843 8510 7843 8511 7843 8512 7843 8601 7843 8602 7843 8602 7843 8603 7843 8606 7843 8606 7843 8606 7843 8606 7843 8607 7843 8606 7843 8607 7843 8607 7843 8608 7843 8607 7843 8608 7843 8610 7843 8611 7843 8611 7843 8612 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8700 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8709 7843 8808 7843 8809 7843 8810 7843 8810 7843 8810 7843 8810 7843 8811 7843 8811 7843 8809 7843 8810 7843 8810 7843 8809 7843 8810 7843 8809 7843 8810 7843 8809 7843 8810 7843 8809 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810	26	327	285	285	1	8	2
7840 9006 7840 9007 7840 9008 7840 9009 7840 9010 7840 9011 7843 8505 7843 8506 7843 8507 7843 8510 7843 8511 7843 8512 7843 8601 7843 8601 7843 8602 7843 8603 7843 8604 7843 8605 7843 8606 7843 8606 7843 8607 7843 8606 7843 8607 7843 8607 7843 8608 7843 8607 7843 8609 7843 8610 7843 8610 7843 8701 7843 8701 7843 8701 7843 8701 7843 8702 7843 8701 7843 8702 7843 8701 7843 8705 7843 8706 7843 8707 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8809 7843 8809 7843 8810 7843 8809 7843 8809 7843 8809 7843 8810 7843 8809	64	820	637	637	1	13	1 0
7840 9007 7840 9008 7840 9009 7840 9010 7840 9011 7843 8505 7843 8506 7843 8507 7843 8510 7843 8511 7843 8511 7843 8601 7843 8602 7843 8602 7843 8603 7843 8603 7843 8606 7843 8606 7843 8606 7843 8607 7843 8608 7843 8610 7843 8611 7843 8611 7843 8612 7843 8701 7843 8702 7843 8701 7843 8702 7843 8701 7843 8702 7843 8701 7843 8702 7843 8701 7843 8702 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8809	30	346	240	237	-5 1	12 8	U
7840         9009           7840         9010           7840         9011           7843         8505           7843         8506           7843         8509           7843         8510           7843         8511           7843         8601           7843         8601           7843         8602           7843         8603           7843         8606           7843         8606           7843         8606           7843         8609           7843         8610           7843         8611           7843         8701           7843         8701           7843         8702           7843         8703           7843         8706           7843         8706           7843         8706           7843         8700           7843         8808           7843         8809           7843         8901           7843         8902           7843         8906           7843         8906           7843 <td>69</td> <td>874</td> <td>874</td> <td>874 771</td> <td>-1 -2</td> <td>7</td> <td></td>	69	874	874	874 771	-1 -2	7	
7840 9010 7840 9011 7843 8505 7843 8506 7843 8507 7843 8509 7843 8510 7843 8511 7843 8511 7843 8601 7843 8602 7843 8602 7843 8603 7843 8606 7843 8606 7843 8606 7843 8606 7843 8607 7843 8610 7843 8611 7843 8611 7843 8611 7843 8702 7843 8701 7843 8702 7843 8703 7843 8706 7843 8706 7843 8707 7843 8706 7843 8706 7843 8707 7843 8706 7843 8706 7843 8707 7843 8706 7843 8707 7843 8706 7843 8707 7843 8706 7843 8707 7843 8706 7843 8707 7843 8706 7843 8707 7843 8706 7843 8707 7843 8707 7843 8708 7843 8808 7843 8809 7843 8809 7843 8810 7843 8809 7843 8810 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809	56	732	732 470	731 466	0	11	
7840 9011 7843 8505 7843 8506 7843 8507 7843 8509 7843 8510 7843 8511 7843 8511 7843 8611 7843 8602 7843 8603 7843 8604 7843 8605 7843 8606 7843 8606 7843 8606 7843 8607 7843 8608 7843 8611 7843 8611 7843 8611 7843 8702 7843 8701 7843 8702 7843 8703 7843 8703 7843 8706 7843 8706 7843 8707 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8808 7843 8809 7843 8811 7843 8809 7843 8811 7843 8811 7843 8809	47	470 3	470 3	0	-111	230	
7843 8505 7843 8506 7843 8507 7843 8509 7843 8510 7843 8511 7843 8511 7843 8601 7843 8602 7843 8603 7843 8603 7843 8605 7843 8606 7843 8606 7843 8606 7843 8607 7843 8608 7843 8611 7843 8611 7843 8612 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8707 7843 8708 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8709 7843 8808 7843 8809 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8809 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8809 7843 8809 7843 8810 7843 8809 7843 8810 7843 8810 7843 8810 7843 8810 7843 8905 7843 8903 7843 8905 7843 8905	1 33	309	309	303	-17	126	
7843         8506           7843         8507           7843         8509           7843         8510           7843         8511           7843         8601           7843         8602           7843         8603           7843         8604           7843         8605           7843         8606           7843         8608           7843         8609           7843         8610           7843         8611           7843         8701           7843         8702           7843         8704           7843         8704           7843         8705           7843         8706           7843         8709           7843         8709           7843         8808           7843         8809           7843         8901           7843         8901           7843         8902           7843         8905           7843         8906           7843         8906           7843         8906           7843 <td>30</td> <td>434</td> <td>359</td> <td>358</td> <td>-3</td> <td>8</td> <td>7</td>	30	434	359	358	-3	8	7
7843 8507 7843 8509 7843 8510 7843 8511 7843 8511 7843 8601 7843 8602 7843 8603 7843 8604 7843 8605 7843 8606 7843 8606 7843 8609 7843 8609 7843 8610 7843 8610 7843 8611 7843 8611 7843 8701 7843 8702 7843 8702 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8709 7843 8809	<u>52</u>	628	596	596	-4	9	6
7843 8509 7843 8510 7843 8511 7843 8511 7843 8512 7843 8601 7843 8602 7843 8602 7843 8604 7843 8605 7843 8606 7843 8606 7843 8609 7843 8610 7843 8610 7843 8611 7843 8611 7843 8701 7843 8702 7843 8704 7843 8705 7843 8706 7843 8706 7843 8706 7843 8706 7843 8707 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8809 7843 8810 7843 8809 7843 8810 7843 8809 7843 8810 7843 8809 7843 8903 7843 8903 7843 8903	28	454	410	410	-3	11	8
7843 8510 7843 8511 7843 8511 7843 8512 7843 8601 7843 8602 7843 8602 7843 8605 7843 8606 7843 8606 7843 8607 7843 8609 7843 8610 7843 8610 7843 8611 7843 8611 7843 8701 7843 8702 7843 8704 7843 8705 7843 8706 7843 8706 7843 8706 7843 8706 7843 8707 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8808 7843 8809 7843 8809 7843 8810 7843 8809 7843 8811 7843 8811 7843 8809 7843 8905 7843 8903 7843 8905 7843 8906 7843 8906	15	198	176	176	-3	15	13 15
7843 8511 7843 8512 7843 8601 7843 8602 7843 8603 7843 8604 7843 8605 7843 8606 7843 8606 7843 8609 7843 8610 7843 8610 7843 8611 7843 8611 7843 8701 7843 8702 7843 8702 7843 8703 7843 8705 7843 8706 7843 8706 7843 8706 7843 8706 7843 8707 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8809 7843 8809 7843 8810 7843 8809 7843 8810 7843 8811 7843 8811 7843 8809 7843 8810 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8810 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8903 7843 8903 7843 8903	14	240					12
7843 8601 7843 8602 7843 8603 7843 8604 7843 8605 7843 8606 7843 8606 7843 8607 7843 8608 7843 8610 7843 8611 7843 8612 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8709 7843 8808 7843 8809 7843 8810	15	203					10
7843 8602 7843 8603 7843 8604 7843 8605 7843 8606 7843 8607 7843 8609 7843 8610 7843 8611 7843 8611 7843 8612 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8810 7843 8809 7843 8810 7843 8809 7843 8905 7843 8903 7843 8905 7843 8906	16	249 700	346	324	6	18	22
7843 8603 7843 8604 7843 8605 7843 8606 7843 8607 7843 8608 7843 8609 7843 8610 7843 8611 7843 8611 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8810 7843 8809 7843 8810 7843 8811 7843 8811 7843 8809 7843 8810 7843 8809 7843 8903 7843 8903 7843 8903	47 29	703 383	296	291	11	15	30
7843 8604 7843 8605 7843 8606 7843 8607 7843 8608 7843 8609 7843 8610 7843 8611 7843 8612 7843 8701 7843 8702 7843 8702 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8707 7843 8708 7843 8709 7843 8709 7843 8809 7843 8810 7843 8810 7843 8811 7843 8811 7843 8901 7843 8902 7843 8903 7843 8903 7843 8903 7843 8906 7843 8906 7843 8906	23	310	237	237	8	12	24
7843 8605 7843 8606 7843 8606 7843 8608 7843 8609 7843 8610 7843 8611 7843 8611 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8810 7843 8810 7843 8811 7843 8811 7843 8811 7843 8810 7843 8809 7843 8810 7843 8810 7843 8809 7843 8810 7843 8809 7843 8809 7843 8810 7843 8809 7843 8809 7843 8809 7843 8903 7843 8902 7843 8903 7843 8903	33	501	481	477	0	13	11
7843 8606 7843 8607 7843 8608 7843 8610 7843 8611 7843 8611 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8705 7843 8706 7843 8707 7843 8706 7843 8707 7843 8709 7843 8709 7843 8710 7843 8808 7843 8811 7843 8811 7843 8810 7843 8901 7843 8901 7843 8901 7843 8903 7843 8905 7843 8906 7843 8906 7843 8906 7843 8906	21	331	152	152	1	9	
7843 8607 7843 8608 7843 8609 7843 8610 7843 8611 7843 8611 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8707 7843 8708 7843 8709 7843 8710 7843 8808 7843 8809 7843 8811 7843 8811 7843 8811 7843 8811 7843 8810 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8809 7843 8901 7843 8901 7843 8901 7843 8902 7843 8903 7843 8903	46	704	212	206	3	13	13
7843 8609 7843 8610 7843 8611 7843 8611 7843 8612 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8709 7843 8710 7843 8809 7843 8811 7843 8812 7843 8812 7843 8901 7843 8901 7843 8902 7843 8903 7843 8903 7843 8905 7843 8906 7843 8906	39	662	261	261	-1 <b>4</b>	9 8	14
7843 8610 7843 8611 7843 8611 7843 8612 7843 8701 7843 8702 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8709 7843 8809 7843 8809 7843 8810 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8903 7843 8903 7843 8906 7843 8906	34	763	327 305	327 381	7	11	1-1
7843 8611 7843 8612 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8709 7843 8709 7843 8709 7843 8809 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8903 7843 8903 7843 8903	30 13	4 <del>69</del> 221	395 190	175	10	13	14
7843 8612 7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8709 7843 8709 7843 8808 7843 8809 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8902 7843 8903 7843 8903 7843 8903	13 3	49	43	43	5	7	
7843 8701 7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8706 7843 8707 7843 8708 7843 8709 7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8903 7843 8903 7843 8903	3	•	_				18
7843 8702 7843 8703 7843 8704 7843 8705 7843 8706 7843 8706 7843 8708 7843 8709 7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8903 7843 8903	17	25 <del>9</del>	247	247	-2	13	15
7843 8703 7843 8704 7843 8705 7843 8706 7843 8706 7843 8708 7843 8710 7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8906	15	198	197	197	9	15	18 22
7843 8705 7843 8706 7843 8707 7843 8708 7843 8709 7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8906	18	253	188	187	11 <b>4</b>	12 19	18
7843 8706 7843 8707 7843 8708 7843 8709 7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8906	13	195	57 111	52 111	4	8	16
7843 8707 7843 8708 7843 8709 7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8907	10	147	111	111	-		18
7843 8708 7843 8709 7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8906	12	195	163	163	5	9	19
7843 8709 7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8906	24	402	61	61	5 4	9	14
7843 8710 7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8907	30	480	480	480	16	29 45	26 35
7843 8808 7843 8809 7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8906 7843 8907	12 7	173	173	172	17	65 7	35 11
7843 8810 7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8907	7	73 426	73 20	73 32	<u>-4</u> 2	12	14
7843 8811 7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8907	33	436 604	32 539	32 539	-13	28	2
7843 8812 7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8907	<b>4</b> 5 <b>2</b> 0	254	247	247	-3	28 27	2
7843 8901 7843 8902 7843 8903 7843 8905 7843 8906 7843 8907	22	275		<del></del>			
7843 8902 7843 8903 7843 8905 7843 8906 7843 8907	40	637	498	493	-8 -4	33	-1 8 5 1
7843 8903 7843 8905 7843 8906 7843 8907	37	542	522	517	4	15	8
7843 8905 7843 8906 7843 8907	13	201	151	150	-8 16	16	5
7843 8906 7843 8907	3	31	31	31 ~7	-16	17 61	
7843 8907	3	41	27 126	27 125	-11 -12	34	10 -2 8 0
-0.10 00000	9	126	126 166	163	11	21	8
7843 8908	13 7	166 90	90	88 88	-10	17	Õ
7843 8909 7843 8910	2	90 40	54	54	-14	15	6 1
7843 8910 7843 8911	21	519	519	515	-10	17	1
7843 8912	17	416	416	416	-5	21	3 -6
7843 9001	19	177	1 <b>77</b>	177	-17	28	-6

Station	ъ.	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Engr. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
<u>, , , , , , , , , , , , , , , , , , , </u>	·					(CIII)	(CIII)	(CIII)
7843	9003	12	170	170	168	-6	15	-5
7843	9004	24	277	277	276	-19	31	2
7843	9005	56	75 <del>9</del>	75 <del>9</del>	756	-12	25	4
7843 7843	9006	22	296	296	294	-5	17	7
7843 7843	9007 9008	7 6	59 71	59 71	59 71	-5 -9	15 18	
7843	9009	<u>2</u> 2	275	275	271	-7	14	
7843	9010	36	441	441	437	-14	24	
7843	9011	19	274	274	269	-23	30	_
7844 7844	8802 8803	8 3	51 <b>4</b> 1	33 15	33 15	0 22	27 29	7 9
7853	8810	48	738	457	457	4	9	5
7853	8811	12	231	209	209	4	25	4
7882	8402	8	88	86	85	-3	9	16
7882	8403	8	66	59	59	8	13	22
7882 7882	8805 8806	12 34	165 454	165 454	156 453	25 -5	<i>77</i> 0 255	-1 -3
7882	8807	6	66	66	433 66	-18	235 39	-3 -1
7883	8905	9	116	116	116	28	29	7
7883	8906	15	210	210	210	24	32	7
7883	8907	4	53	21	21	-7	12	-8
7883 7883	8907 8908	5	40	32 40	32 40	22 31	27 34	3
7883	8909	1	10	10	40 10	19	20 20	1 8
7885	8207	1	4	4	4	Ő	4	J
7885	8208	25	235	224	224	1	6	-10
7885 7885	8209	7 3	57 7	57 7	55	4	14	-1
7885 7885	8210 8211	3	7	/	7	-4	12	3 4
7886	8308	18	128	128	127	-3	9	3
7886	8407	4	49	48	48	3	5	6
7886	8408	37	583	577	577	-1	8	-3
7886 7886	8409 8409	28	387	274 113	271	-1 <b>7</b>	51 12	-1 0
7886	8410	19	198	194	113 194	1	5	1
7887	8302	3	10	10	10	3	22	85
7888	8202	13	104	104	104	0	11	-14
7888	8203	10	125	125	125	0	13	-12
7888 7890	8204 8103	8 2	80 25	80 25	80 25	-2 1	14 14	-16 61
7891	8106	11	141	141	141	-4	11	-7
7891	8107	28	278	256	256	-2	11	-5
7892	8105	11	109	106	105	-3	11	2
7892 7892	8106	26	335	322	321	-4	9	-11
7892	8206 8207	10 22	95 172	95 172	95 169	3 2	6 12	4
7892	8208		.,_	.,_	107	-	12	3
7894	8303	3	11	9	9	1	9	10
7894	8304	15	101	101	100	-2	11	-4
7894 7894	8305 8306	3 25	13 146	13 144	13 144	-7 -3	15 <b>2</b> 0	6 3
7894	8307	5	23	23	22	-3 11	25 25	6
7896	8010	6	55	55	55	3	11	4
7896	8011	35	324	315	312	1	13	-6
7896 7899	8012 8008	30	370	354	349	- <b>4</b>	9	-10
7899	8009	1 25	1 219	1 191	1 191	-13 -2	0 10	-27 -12
7899	8010	7	45	45	42	-3	21	-7
7907	7602							-19
7907	7603							31
7907 7907	7604 7605	22	242	147	146	10	49	27
7907 7907	7605 7605	44	Z- <b>4</b> Z	14/	140	-10	49	3 28
7907	7606	23	335	186	185	-15	55	-10
7907	7607	17	216	134	133	-14	43	3
7907	7608 7600	11	166	78 15	78 15	3	45	-1
7907 7907	760 <del>9</del> 7610	2 31	24 528	15 <b>461</b>	15 461	0 2	46 40	
7907 7907	7611	31	526 549	461 464	461 461	6	40 52	
7907	7612	20	336	287	287	-5	46	

Station		No. of	Observ.	Obs. after	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
Number	Date	Passes	Acquired	eng r. Eun	Dynam. Eun	(cm)	(cm)	(cm)
7907	<b>77</b> 01	15	211	154	153	-10	51	-8 6
7907	7702	9	1 <b>27</b>	.97	97	-6 33	42 58	40
7907	7704	22	356	272 316	272 316	-10	50	-2 9
7907	7705	24 51	391 886	742	742	Ö	43	9
7907	7706 7707	51 56	1007	713	712	-1	43	5
7907 7907	7708	31	511	348	348	-9	48 45	-4 -45
7907	7709	31	572	280	280	-15 10	45 41	0
7907	<i>7</i> 710	24	410 383	307 328	307 328	-1	45	0
7907	7711 7712	21 21	405	343	343	7	48	2
7907 7907	7712 7804	17	300	250	250	27	49	3 3
7907	7805	29	512	408	408	22 15	51 50	7
7907	7806	28	451	380 875	380 874	-1	34	-10
7907	7807	50 42	1013 <b>792</b>	750	748	- <b>i</b>	34	-13
7907	7808 7809	42 41	688	688	681	-2	48	-9
7907 7907	7810	25	403	392	387	5	65 F	-4 -8
7907	7811	12	158	158	156	11	53 31	-0 -4
7907	7812	17	194	182 87	182 87	0 -7	44	-19
7907	7901	11	101 21 <b>4</b>	87 184	184	-4	32	-8
7907 7907	7902 7903	18 11	91	79	79	-1	31	10
7907 7907	7904	31	370	302	297	-2	36 32	<i>-7</i> -5
7907	7905	43	527	438	437 594	3 2	32 32	-1
7907	7906	43	683 344	605 229	225	-4	30	-12
7907	7907	36 23	253	206	206	2	21	-2
7907 7907	7908 7909	23	256	209	201	6	26	-3 22
7907 7907	7910	7	55	38	<b>38</b>	-10	26 27	-23 -4
7907	7911	20	194	151	151 163	-1 3	23	4
7907	7912	20	219 247	163 178	174	-5	22	-10
7907	8001 8002	<b>20</b> 11	65	36	30	7	38	3 -3 -7 -7
7907 7907	8003	7	71	42	40	5	24 25	-3 7
7907	8004	29	367	336	330	-5 -3	25 25	-7 -7
7907	8005	39	547 645	<b>49</b> 0 5 <b>76</b>	490 570	-3 -2	25	
7907	8006	47 36	465	405	395	0	24	-5
7907 7907	8007 8008	51	698	639	621	4	27	0
7907	8009	35	457	358	348	<b>4</b> -5	25 22	-1 -9
7907	8010	16	216	208 208	203 203	2	23	-7
7907	8011	23 24	219 250	208	203	-8	33	-13
7907 7907	8012 8101	<b>24</b> 5	28	28	26	-14	35	-22
7 <del>9</del> 07	8103	12	28 95	28 95	95	9 3	33 42	-2 0
7907	8104	18	199	178	168 2 <b>7</b> 9	1	23	-5
7907	8105	28 42	325 551	287 497	491	-3	23	-22 -2 0 -5 -6 -9 -7 -4
7907 7907	8106 8107	53	842	801	792	-2	22	-9
7907 7907	8108	39	677	656	590	-3	22 23	-/ .A
7907	8109	41	700	636	518 274	-1 -1	23	4
7907	8110	24	363 191	342 120	274 113	1	20	-1
7907	8111 8112	23 5 4	25	15	14	-9	30	-13 -5
7907 7907	8112 8201	4	36	33	32	4	20	-5 -10
7907	8202	7	55 1 <b>2</b> 6	55	55 116	-5 7	33 36	0
7907	8203	14	126	126	116 61	-17	23	-25
7907	8204	4	66 876	64 802	619	0	18	-25 <i>-</i> 7
7907 7007	8205 8206	39 47	966	<i>77</i> 8	631	0	11	
7907 7907	820 <del>7</del>	64	1350	1323	1045	1	9	-5 -7 -8
7907	8208	42	822	784	667	-2 -4	13 14	-/ -8
7907	8209	32	587	587 383	488 307	-4 -9	20	-10
7907	8210	23	390 216	383 207	307 175	-6	26	-12
7907 7907	8211 8212	16 28	418	418	395	-6 -2 -4	10	-8 -12
7907 7907	8301	29	448	448	420		12	-12 12
7907	8302	28 22	446 272	<b>44</b> 6 272	423 266	-4 -6	14 17	-12 -7
	8303							

Station Number	Date	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
						(CIII)	(CIII)	(CIII)
7907	8304	35	506	486	458	-2	17	-6
7907	8305	56	1029	981	782	-2	19	-6
7907	8306	61	1226	1226	996	-3	22	-6 -5 -8 -6 -5 -5 -8
7907 7007	8307	<i>7</i> 6	1550	1550	1249	-1	12	-5
7907 7907	8308 8309	57 48	1103 1016	1103 1016	887 762	-2 -3	9 9	-8
7907 7907	8310	45	1038	985	787	-3 -1	12	-0
7907	8311	43	931	914	777	-1 -1	11	-5 -5
7907	8312	30	512	500	457	-3	11	-8
7907	8401	1	16	16	16	2	7	-4
7907	8402	1	17	17	16	-3	8	-10
7907	8403	2	30	28	28	8	15	-6
7907 7907	8404 8405	25 38	414 646	403 612	366 538	-3	27	-8
7907 7907	8406	37	601	581	528 572	-1 0	14 9	-5
7907	8407	53	909	871	863	1	12	-5 -5
7907	8408	48	763	743	742	-1	9	-8 -5 -5 -5 -5
7907	8409	51	841	831	829	Ō	10	-4
7907	8410	26	361	321	309	-1	19	-6
7907	8411	18	235	210	206	-1	11	-6
7907 7907	8412 8501	19 13	264 139	244 139	224	-6	19	-9
7907 7907	8502	6	13 <del>9</del> 59	139 59	138 59	2 -2	17 10	-3 -7
7907	8503	10	109	93	93	-2 -6	10 14	-/ -8
7907	8504	20	190	134	134	-3	12	-7
7907	8505	40	552	490	487	0	9	-5
7907	8506	44	690	655	655	1	9	-4
7907 7007	8507	51 45	792 707	777	771	1	13	-4
7907 7907	8508 8509	45 24	707 393	<b>684</b> 371	683 367	-1 2	14	-9
7907	8510	29	440	427	367 410	-2 -3	18 19	- <del>6</del> -10
7907	8511	8	75	64	52	-3 - <b>2</b>	26	-10 -11
7907	8512	3	32	29	29	- <del>6</del>	11	-9
7907	8601	4	41	35	35	-3	9	-12
7907	8602	5	<b>⊕</b>	63	63	-6	12	-10
7907 7907	8603 8604	9	107	91 120	91 120	7	14	-2
7907 7907	8605	21 31	225 459	129 234	128 233	-5 -3	14	-11
7907	8606	33	588	226	223	-3 8	8 13	-4
7907	8607	33	572	209	207	-5	11	-4
7907	8608	23	332	219	219	-6	10	7
7907	8609	20	306	251	250	2	10	
7907	8610	29	506	411	409	2	10	-8
7907 7907	8611 8612	27 19	387	262 170	262	0	8	_
7907 7907	8701	7	287 99	170 80	154 80	3 1	14 11	-5
7907	8702	<b>2</b> 6	370	328	328	3	9	-3 1
7907	8703	20	245	139	139	2	<b>8</b>	-1
7907	8704	23	314	194	194	3	11	-2
7907	8705	13	163	88	84	1	13	-1
7907	8706	9	89	41	40	3	8	2
7907 7907	8707 8708	22 31	376 520	235 230	235 229	2	9	-1
7907 7907	8709	36	614	230 271	265	3 5	7 9	-3 0
7907	8710	29	542	151	140	2	11	-2
7907	8711	23	389	177	177	ī	7	-1
7907	8712	21	290	156	156	4	9	-3
7907	8801	6	80	42	34	5	18	-4
7907 7007	8802	3	51 250	20	20	0	10	-4
7907 7907	8803 8804	14 16	250 271	158	150	2	8	-2
7 <del>9</del> 07 <b>79</b> 07	8805	32	495	223 291	218 284	<b>4</b> 3	8 7	-2 1
7907	8806	31	509	159	264 120	3 7	7 15	-1 -1
7907	8806	V-	300	155	154	4	7	-1 1
7907	8807	33	530	311	300	5	14	3
7907	8808	30	498	241	231	5	8	1
7907	8809	25	413	<i>7</i> 8	72	5	11	1
7907	8810	22	385	169	145	6	16	0
7907 7907	8811 8812	11	188	56	52	8	15	-1
7507	0012	1	13					
7907	8812	1	13					-

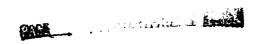
Station	<b>D</b> :	No. of	Observ.	Obs. after	Obs. after Dynam. Edit	Mean Residual	RMS of Residual	Bias Estimate
Number	Date	Passes	Acquired	Eng r. Euit	Jynam. Buit	(cm)	(cm)	(cm)
							.,	
7907	8901	1	12	12	6	-3 -1	24 21	-10 -5
7907	8902	5	76 103	76 103	72 98	-1 9	15	1
7907 7907	8903 8904	<i>7</i> 14	217	217	209	7	17	3
7907 7907	8905	31	481	481	456	4	20	1
7907	8906	28	457	457	439	5	32 11	8 0
7907	8907	31	511 245	109	109 74	4 11	32	0
7907	8908	16 17	245 249	91 249	155	-5	18	-2
7907 7907	8909 8910	17	219	219	151	4	<b>78</b>	-3
7907	8911	26	393	382	309	3	20 22	1 2
7907	8912	18	289	251	209	9 1	32 10	4
7907	9001	5	62 133	38 41	38 38	2	19	-13
7907 7907	9002 9003	9 3	135 <b>47</b>	29	29	3	12	0
7907 7907	9006	6	72	44	42	14	19	2
7907	9007	15	281	281	252	5 4	16 16	
7907	9008	14	251 274	251 274	226 237	5	19	
7907	9009 9010	16 16	274 205	205	198	-51	730	
7907 7907	9011	1	13	13	12	1	24	
7918	8812	1	10				100	
7918	9004	14	185	185	63 151	-157 5	198 14	
7918	9005	10 21	154 276	154 276	151 2 <b>6</b> 7	4	12	
7918 7918	9006 9007	21 10	106	106	106	5	7	
7918	9008	6	<i>7</i> 4	74	74	1	3	
7918	9009	19	288					
7920	8811	6	96 253					
7920	8812 8908	21 1	13					
7920 7920	8909	2	18					
7920	8910	8	101					
7920	9009	17	197					
7920	9010	1	19					27
7921 7921	7602 7603							-6 5
7921	7604						***	5
7921	7605	36	587	386	384	11	50	24 57
7921	7605	40	730	451	446	4	56	16
7921 7921	7606 7607	48 3	750 25	17	16	-28	84	11
7921	7608	7	102	54	54	-7	64	1
7921	7609	27	334	194	194	23 20	<i>7</i> 3	
7921	7610	35	405 598	242 379	242 378	19	52 57	
7921 7921 7921	7611 7612	46 32	475	307	306	-1	50	
7921 7921	7701	12	166	101	101	20	58	82
7921	<i>7</i> 702	34	580	438	438	23 0 -15 5	46 38	30 -12
7921	7703	31	592	414	414 206	-15	38	-51
7921 7921	7704 7705	16 4	247 60	206 48	48	-13 5	41	-34
7921 7921	7706	2	32	24	24	-10	52	-23
7921	7707	1	32 15	15	15	-62	73 97	-76 93
7921	7708	8	112	70 124	65 134	68 20	87 46	21
7921 7021	7709 7710	20 24	293 443	134 341	341	20 6	40	17
7921 7921	7710 7711	33	578	466	466		48	35 -8
7921	<i>7</i> 712	36	613	522	521	2	45 77	-8 21
7921 7921	<b>7</b> 801	<b>2</b> 0	307	307	306 	-6 -4	<i>7</i> 7 <b>4</b> 6	-21 -3
7921	7802	3 32	61 <b>44</b> 5	61 331	61 331	- <b>1</b> -7	46 45	-14
7921 7921	7804 7805	32 28	445 478	379	378	-7 -3	47	-23
7921 7921	7806	40	697	541	541	0 -6	49	-12
7921	7807	10	54	48	48	-6 20	34	-26 -40
7921	7808	2	19	19	19 <b>7</b> 3	-39 -9	49 36	- <del>4</del> 0 -8
7921 7921	7809 7810	11 15	91 186	73 157	156	-9 -30	50 52	-30
7921 7921	7810 7811	15 10	77	76	<b>7</b> 6	-35	55	-11 -25
7921	7812	11	84	82	82	-22	41	-25
<b></b>								

Station	Dat-	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng r. East	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
		÷				(CIII)	(ent)	(CIII)
7921	<b>7</b> 901	5	35	32	32	-11	26	-34
7921	7902	8	58	47	47	-5	36	-21
7921	7903 7004	8	<b>4</b> 7	38 52	38	-5 13	33 20	-21 20
7921 7921	7904 7905	14 9	70 65	53 61	52 61	-12 -13	29 31	-28 -18
7921 7921	8112	1	15	8	8	-13 -9	19	-10 - <b>4</b> 0
7921	8201	1	16	8	8	-23	28	-10
7921	8202	8	105	105	92	-23	217	-30
7921	8203	2	27	27	27	-12	32	-19
7929 7929	7602 7603							-5 <b>36</b>
7929	7604							16
7929	7605	15	15 <del>9</del>	104	104	-14	57	9
7929	7605							70
7929	7606	25	363	278	275	-11	55	-18
7929 7929	7607 7608	10 12	142 138	98 70	98 69	14 22	4 <u>2</u> 63	2 31
7929 7929	7609	10	117	58	58	<b>4</b> 5	86	31
7929	7610	12	173	123	123	3	49	
7929	7611	16	225	140	138	23	65	
7929	7612	12	176	124	122	46	₩	
7929 7929	<i>7</i> 701 <i>7</i> 702	5 5	33 55	29 33	28 33	25 34	72 64	-16 37
7929 7929	7703	10	130	33 74	33 73	50 50	66	50
7929	7704	3	22	16	16	29	65	52
7929	<i>7</i> 705	9	88	60	60	-24	90	-12
7929	7706	10	94	39	39	-1	72	13
7929 7929	7707 7708	9 13	<i>7</i> 7 134	47 94	<b>4</b> 3 87	22 23	79 95	6 -3
7929 7929	7709	13 4	51	40	38	29	105	-30 -30
7929	7710	9	78	45	32	72	133	-11
7929	<i>7</i> 711	11	118	80	70	33	113	3
7929	7801	16	172	172	170	10	81	39
7929 7929	7802 7807	1 2	15 17	15 14	15 1 <b>4</b>	52 -17	87 62	143 -48
7929	7808	4	42	39	38	-10	37	- <del>2</del> 6
7929	7809	5	51	35	35	7	73	0
7929	<b>7</b> 810	11	101	79	78	7	64	-13
7929 7929	7811 7812	10	87 23	64	64	-5	53	-13
7929 7929	7901	2 6	31	17 26	14 26	-3 2	108 26	-9 -33
7929	7902	ž	50	49	49	-22	30	-35 -37
7929	7903	3	13	9	9	15	25	22
7929	7904	2	19	15	15	7	26	-34
7929 7929	7905 7004	1	4	4	4	-10	29 35	<b>-4</b> 5
7929 7929	7906 7908	2 5	13 15	8 10	8 10	-15 -14	35 <b>29</b>	-29 -9
7929	7910	2	8	4	4	9	15	-21
7929	7911	4	15	7	7	-37	46	-43
7929	7912	2	18	6	6	-20	27	-43
7929 7929	8001 8002	1 3	4	<b>4</b> 7	2	<b>-49</b>	83 20	-72 27
7929 7929	8003	4	10 25	7	5 7	-7 4	39 25	-27 12
7929	8004	6	46	32 32	30	-12	38	-16
7929	8005	4	18	14	12	-1	73	-46
7929	8006	4	11	9	9	-5	29	-19
7929	8007	3	17	3	3	-32	<b>42</b>	-52
7929 7929	8008 8009	8 4	50 19	33 16	30 16	4 2	38 17	-15 -11
7929	8010	6	33	32	31	4	24	-11 -15
7929	8011	12	81	78	<i>7</i> 5	-6	26	-16
7929	8012	7	37	36	34	-5	33	-14
7929	8101	9	47	47	45	7	30	-14
7929 7929	8102	8	33 14	33 14	30 14	-18	42 27	-18
7929 7929	8103 8104	3 2	14 18	14 18	14 17	4 8	27 32	48 -8
7929 7929	8106	8	93	93	83	-4	32 35	-8 -16
7929	8107	19	1 <b>7</b> 5	164	155	- <del>7</del>	33	-23
7929	8108	15	140	136	136	-4	26	-23
7929	8109	17	146	138	133	-9	25	-23

Station		No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng'r. Edit	Dynam. Edit	Residual	Residual	Estimate
						(cm)	(cm)	(cm)
			_	_		0	26	-21
7929	8110	1 19	7 378	7 378	7 300	4	20 11	-7
7939 7939	8309 8310	25	455	401	325	-7	13	-10
7939 7939	8311	12	226	115	96	-4	10	-5 <b>7</b>
7939	8312	16	309	302	237	-2 -3	11 9	-7 -6
7939	8401	30	635	610 152	511 114	-3 -12	21	-8
7939	8402 8403	9 14	164 211	200	181	-4	10	-8 -8
7939 7939	8404	24	435	415	352	1	15	-3
7939	8405	32	602	544	466	0	8	-3 -2
7939	8406	38	<del>699</del>	6 <del>69</del>	604	-1 -1	8 9	- <u>-</u> 2 1
7939	8407	50	830	768 679	<i>7</i> 35 651	1	10	i
7939	8408 8409	43 35	724 643	599	573	i	8	0
7939 7939	8410	25	413	375	361	0	9	-1
7939	8411	13	219	190	185	1	9	0 -2
7939	8412	25	418	339	291 77	-3 5	13 15	2
7939	8501	11	148	123 106	97 99	-1	11	1
7939	8502 8503	9 10	129 178	88	85	- <b>3</b>	9	-1
7939 7939	8504	19	298	286	250	-1	64	-3
7939	8505	22	392	283	270	-1	8 9	-3 -4
7939	8506	26	430	327	306 762	1 1	10	-3
7939	8507	49 58	1007 1137	862 1024	926	-1	10	-3 -2
7939 7939	8508 8509	26 78	1577	1338	1192	-1	13	-2
7939	8510	70	1354	1237	1108	1	12	-1 -1
7939	8511	43	753	676	610 <del>669</del>	-2 0	10 <b>7</b>	-1 -1
7939	8512	44	854 704	745 640	568	0	8	Ô
7939 7939	8601 8602	41 26	444	351	333	-1	8	0
7939 7939	8603	15	210	170	154	0	7	0 0
7939	8604	30	575	496	445 226	3 1	10 8	U
7939	8605	19	338 248	256 169	236 158	-7	14	-1
7939 7939	8606 8607	16 15	246 215	117	112	-5	13	
7939 7939	8608	10	128	86	68	0	11	-2
7939	8609	16	292	236	199	2 0	10 7	-4
7939	8610	20	420 195	384 149	337 142	1	6	•
7939 7939	8611 8612	11 28	538	421	391	-2 -5	9	1
7939 7939	8701	9	195	149	139	-5	9	-3
<b>7</b> 939	8702	18	<b>34</b> 5	288	265	5	12 6	-1 -2
7939	8703	23	397	193 436	182 408	1 2	8	
7939	8704 8705	41 37	788 648	392	362	ō	7	-2 -3 -2
7939 7939	8706	37	590	412	405	2	6	-2
7939	8707	57	830	615	607	2	6 6	-1 -4
7939	8708	44	728	528 580	518 <b>54</b> 6	0 -101	807	-3
7939 7939	8709 8710	44 28	816 453	324	317	0	6	-4
7939 7939	8711	16	281	206	197	2 0	7	-3
7939	8712	17	267	131	131		8 15	-2 0
7939	8801	12	212	104	88 107	3 1	9	-1
7939 7939	8802 8803	17 14	260 253	109 127	118	-3	9	-1
7939 7939	8804	16	259	128	127	0	7	-3
7939	8805	18	304	217	194	-2	6	-3 -4 -3 -2 0 -1 -1 -3 -5 -7 -6 4 -5 -2 -3 -4 -5 -2 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1 -1
7939 7939	8806	25	496	350	287 170	-1 -3	10 8	-5 -7
7939	8807	31	483 776	1 <i>7</i> 2 329	170 318	-3 -4	8 7	-6
7939 7939	8808 8809	46 27	402	68	68	-4 -2	4	-4
7939 7939	8810	35	555	189	172	-1	9	-5
7939 7939	8901	22	318	163	160	-1	6 10	-2 _2
7939 7939	8902	31	458	243	242 225	-5 -4	10 8	-3 -4
7939	8903	25 17	377 211	225 121	225 121	-2	8 7	- <b>5</b>
7939 7939	8904 8905	23	309	183	183	0	9	-1
7939	8906	10	154	62	62 104	-7	15 7	-4 -6
7939 7939	8907	11	1 <b>7</b> 1	110	104	-1	7	- <b>6</b>

Station	D-1-	No. of	Observ.	Obs. after	Obs. after	Mean	RMS of	Bias
Number	Date	Passes	Acquired	Eng r. East	Dynam. Edit	Residual (cm)	Residual (cm)	Estimate (cm)
							<u> </u>	· · ·
7939	8908	2	29	23	9	-34	43	-4
7939 7939	8909 8910	1 5	14 56	10 55	10 <b>46</b>	6 -3	9 <b>16</b>	10 -5
7939	8911	18	286	156	154	0	8	2
7939	8912	18	2 <del>69</del>	129	127	€	746	3
7939 7939	9001 9002	23 46	378 876	246 297	244 283	-2 2	7 7	-6 0
7939 7939	9003	40 40	711	297 71	200 66	2	10	-2
7939	9004	2	<b>37</b>	36	<b>2</b> 0	-37	42	-14
7939	9005	22	359 300	291	287	-12	16	-4
7939 7939	9006 9007	24 18	300 219	102 219	97 213	-6 -3	13 173	-3
7939	9008	8	120	120	118	0	8	
7939	9010	26 20	377	377	365	-71 7	901	
7939 7939	9011 9012	<b>20</b> 11	347 201	347 201	333 186	-7 -6	188 18	
7940	7601	1	16	201	100	Ū	10	
7940	8406	6	42					_
7943 7943	7605 7606							9 -27
7943	7607							-27 -41
7943	7608							-41
7943 7943	7609 7610	3	47	43 109	43	6	35	
7943 7943	7611	8 8	121 109	104	109 104	18 -6	44 53	
7943	7612	22	340	298	298	-11	40	
7943	7701	21	322	278	278	2	40	-32
7943 7943	7702 7703	25 25	404 372	340 291	340 291	-3 -5	36 38	-15 <i>-7</i>
7943	7704	59	883	767	<i>7</i> 53	ŏ	39	Ó
7943	7705	37	538	435	435	13	45	-6
7943 7943	7706 7707	40 62	5 <del>99</del> 1251	494 1056	465 938	16 8	53 36	-11 -11
7943	7708	62	1097	1023	898	-2	33	-11 -27
7943	7709	15	279	97	.88	-1	44	-38
7943 7943	<i>7</i> 710 <i>7</i> 711	39 21	843 427	757 412	682 370	-16 -1 <b>4</b>	36 30	- <b>4</b> 1
7943	7712	15	276	267	248	-14 -8	39 40	-40 -27
7943	7801	3	65	65	57	0	51	-21
7943 7943	7802 7804	1 15	13 300	13 271	13 <b>24</b> 9	28 -9	43 20	65 30
7943	780 <del>1</del>	15	355	313	288	-9 -18	39 51	-29 -26
7943	7806	6	133	131	119	-29	56	-35
7943 7943	7809 7810	6	120 474	117	103	-8 10	40	-31 26
7943 7943	7810 7811	38 27	674 419	579 401	507 378	-10 -5	47 39	-26 -25
7943	7812	14	209	185	174	-5	44	-2
7943	7901	20	279	194	179	2	43	17
7943 7943	7902 7903	24 23	442 392	325 250	302 223	1 4	30 33	-8 8
7943	7904	9	1 <b>2</b> 6	88	84	-3	35	-29
7943	7905	12	193	188	176	-5	22	-31
7943 7943	7906 7907	20 23	286 388	2 <del>69</del> 356	254 341	-5 2	25 19	-20 -30
7943	7908	14	221	193	193	3	15	-30 -20
7943	7909	5	65	53	52	-2	24	-18
7943 7943	7910 7911	2 3	22 41	20 39	19 39	0 -3	27 22	-12 25
7943 7943	7912	3 7	134	111	39 111	-3 -7	23 19	-25 -32
7943	8001	5	72	68	68	-2	16	-24
7943 7943	8002 8003	10 <b>26</b>	160 <b>47</b> 3	145 434	132 401	-1 -5	21	-24
7943 7943	8004	26 33	473 568	434 549	401 494	-5 -5	18 22	-27 -25
7943	8005	22	271	245	222	1	26	-17
7943	8006	40	651 586	597	553	-3	24	-27
7943 7943	8007 8008	44 67	586 930	526 825	475 744	2 -3	26 24	-21 -22
7943 7943	8009	67 44	662	632	570	-3 -2	24 21	-22 -23
	8010	40	624	580	529	- <b>4</b>	24	-25
7943 7943	8011	30	<b>47</b> 0	465	425	-8	27	-27

Station Number	Date	No. of Passes	Observ. Acquired	Obs. after Eng'r. Edit	Obs. after Dynam. Edit	Mean Residual (cm)	RMS of Residual (cm)	Bias Estimate (cm)
-				216	205	-3	23	-27
7943	8012	15	224	216	244	-1	24	-20
7943	8101	20	265	265	131	-1 -4	24	-34
7943	8102	10	141	141	80	4	30	-18
7943	8103	7	84	84	138	-1	28	-32
7943	8104	12	165	149	93	0	30	-29
7943	8105	11	137	102	93 94	2	39	-23
7943	8106	10	121	108		-3	25	-26
7943	8107	24	376	347	326		27	-22
7943	8108	16	189	160	147	0	26 26	-24
7943	8109	21	268	227	206	-2	27 27	-31
7943	8110	13	117	90	77	-5		-33
7943	8111	6	55	34	32	-4	21 22	-35 -35
7943	8112	9	<i>7</i> 1	61	57	-2	22	-33 -30
7943	8201	14	98	89	<i>7</i> 5	3	33	
7943	8202	27	247	247	221	-8	37	-33
8833	8404	4	23	23	23	-1	5	10
8833	8405	8	130	130	130	3	7	2
8833	8412	7	97	93	93	-1	11	-6
8833	8501	6	40	40	40	1	7	•
8833	8502	4	38	38	38	8	10	0
8833	8806	2	7	7	7	3	7	6
8833	8807	7	67	49	49	-2	9	-1
	8808	<b>2</b> 0	206	206	206	-2	8	0
8833	8809	24 24	284	284	283	-4	12	1
8833		35	383	383	382	0	7	
8833	9007	30	303	•				



## LAGEOS Geodetic Analysis - SL7.1

## Appendix 3

Monthly LAGEOS Orbital Fits and Estimates of Force Model Parameters

Modified	No. of	RMS Orbital	Solar	Along-Track
Julian Date	Observations	Fits (cm)	Radiation	Acceleration (pms <sup>-2</sup> )
42930	<i>7</i> 78	36	1.2119	-4.5464
42945			1.2014	-3.5817
42960	956	31.1	1.1641	-6.0025
42975			1.0805	-4.0346
42991	247	28.8	1.8377	-2.6459
43006			1.8037	-7.44
43022	223	35.4	.9913	-5.1794
43037			1.1277	-4.1021
43052	325	33.9	1.1043	-3.1988
43067			1.1774	-3.5388
43083	1030	28.3	1.1555	-3.3535
43098			1.1602	-3.1257
43113	1904	34.9	1.1324	-1.7707
43128	1701	02.5	1.1282	-1.6933
43144	1199	34.4	1.0556	-3.9379
43159	11//	<b>73.3</b>	1.1664	1657
43175	560	31.9	1.1484	-1.215
43190	<b>500</b>	51.7	1.0997	753
43203	1125	30.7	1.124	753 -4.5884
43218	1125	30.7		
43234	942	30.9	1.0861	-4.3162 2.5306
43249	942	30.9	1.135	-3.5306
43264	1467	25.2	1.1401	-4.2003
432 <del>7</del> 9	1467	35.2	1.1456	-5.4863
	073	22.4	1.1066	-2.1732
43295	873	32.4	1.1288	-3.9015
43310	1070	20.4	1.1381	-3.0441
43325	1270	29.4	1.1079	-3.8855
43340	17700	21.6	1.1129	-3.0339
43356	1708	31.6	1.1392	-2.8198
43371	1407	04.77	1.1129	-3.9677
43387	1436	34.7	1.0875	-3.0219
43402	eer	20.0	1.1897	-1.1776
43417	555	30.2	1.1198	-2.4546
43432	1530	27.5	1.1517	-2.8093
43448	1528	36.5	1.1015	9143
43463	1007	22	1.1104	-1.8421
43478	1296	37	1.0996	-2.1358
43493	1140	<b>40.4</b>	1.1835	-3.5831
43509	1142	63.4	1.2333	-5.1484
43524	540	22.2	1.0237	-3.6518
43540	543	32.3	.6026	3.032
43555	21-	1	1.1763	-1.2907
43568	215	11.7	1.1102	-3.0922
43583		20.7	.9828	-2.0284
43599	593	30.7	.9743	-3.369
43614			1.0965	-2.1473
43629	1072	38.4	1.0848	-3.1293
43644			1.0875	-2.2875
43660	1074	41.3	1.0568	-1.921
43675			1.135	-3.8121
43690	1049	28.6	1.0932	-1.2848
43705			1.1285	7446
43721	1122	24.7	1.1236	952
43736			1.1267	-1.4589

Modified	No. of	RMS Orbital	Solar	Along-Track
Julian Date	Observations	Fits (cm)	Radiation	Acceleration (pms-2)
	1446	35.1	1.1232	-1.236
43752	1440	33.1	1.1312	-3.1879
43767	1196	44.1	1.1207	-2.9339
43782	1190	74.1	1.136	-4.2142
43797	1100	36.9	1.2028	-3.961
43813	1190	30.9	1.174	-3.7485
43828	(0)	20.0	1.1488	-2.5765
43843	696	28.8	1.2632	-5.5891
43858		20.2	1.2194	-3.492
43874	<b>5</b> 05	22.3	1.0833	-4.6632
43889		10.4		-6.3809
43905	342	19.4	1.1381	-3.4201
43920		4=0	1.0676	-3.7948
43933	825	17.3	1.1329	-3.7 <del>94</del> 0 -4.8523
43948			1.1395	
43964	880	15.6	1.134	-7.2594 4.6535
43979			1.1489	-4.6535 5.5039
43994	1352	18.9	1.1471	-5.5038
44009			1.1054	-5.6283
44025	1304	22.4	1.1304	-5.1828
44040			1.1432	-3.7562
44055	1130	17.7	1.1072	-3.1239
44070			1.1573	-4.5634
44086	910	15.3	1.148	-3.9493
44101			1.2023	-5.5878
44117	546	11.1	1.1852	-4.3884 4.5539
44132			1.1866	-4.5538 2.0152
44147	1082	10.2	1.1967	-3.9152 4.2024
44162			1.172	-4.3924 -4.2313
44178	2371	15.3	1.1484	
44193			1.1515	-3.8966 -3.852
44208	2574	13.7	1.1453	-3.1536
44223		40.0	1.1325	-2.5083
44239	2665	10.2	1.1302	-1.7162
44254		0.0	1.1145	-1.5172
44270	1712	9.3	1.13 1.1217	8456
44285		0.0	1.1277	7127
44299	2543	9.3	1.1331	9707
44314	0001	10.0	1.1389	-2.8289
44330	2991	13.3	1.1378	-3.6897
44345	0740	16.1	1.1443	-3.7941
44360	2642	10.1	1.1447	-3.4406
44375	1745	17.4	1.1495	-3.3603
44391	1 <b>74</b> 5	17.4	1.132	-2.8682
44406	0117	14.6	1.1116	-2.8943
44421	2117	14.0	1.1346	-3.1474
44436	20/1	14.8	1.123	-3.037
44452	2061	14.0	1.1251	-3.0056
44467	2406	11.7	1.1179	-3.1242
44483	3496	11./	1.1316	-2.7381
44498	2775	11.8	1.1310	-3.1648
44513	3 <b>77</b> 5	11.0	1.1279	-3.1147
44528	2702	12.8	1.1286	-2.3152
44544	3783	14.0	1.1268	-1.7136
44559			1.1200	2

Modified Julian Date	No. of Observations	RMS Orbital Fits (cm)	Solar Radiation	Along-Track Acceleration (pms <sup>-2</sup> )
·				
44574	3172	12.6	1.1207	-2.1829
44589	40=0	4.	1.1249	-2.4563
44605	1850	12.6	1.1215	-2.3513
44620			1.1221	-2.8965
44636	970	9.6	1.1201	-3.3725
44651			1.1104	-3.786
44664	1453	13.6	1.1248	-3.2154
44679			1.089	-3.729
44695	3298	12.7	1.0805	-3.422
44710			1.0767	-3.7933
44725	2560	11.4	1.0932	-3.8521
44740			1.1414	-3.4747
44756	2086	12.7	1.1012	-3.6846
<b>4477</b> 1			1.1222	-3.7148
44786	2238	14.2	1.1141	-3.9384
44801			1.1174	-3.0089
44817	3147	12.7	1.115	-2.1925
44832			1.1274	-1.9959
44848	2453	11.3	1.1228	-2.0094
44863			1.1324	-2.5319
44878	3387	8.8	1.1311	-2.9519
44893			1.1396	-4.2817
44909	3078	8.5	1.1398	-4.1678
44924			1.1376	-3.879
44939	2113	8.6	1.1736	-3.8434
44954			1.1727	-3.6026
44970	1722	8.3	1.2628	-3.9571
44985			1.0822	-3.8012
45001	1630	14.9	1.1044	-4.2307
45016			1.1376	-3.7779
45029	2041	11	1.1136	-4.6042
45044			1.1543	-3.8364
45060	1768	6	1.1397	-5.3286
45075			1.1267	-6.0256
45090	1324	9.6	1.1377	-6.8851
45105			1.1281	-5.202
45121	2566	7.1	1.134	-6.0658
45136			1.1304	-4.9549
45151	2335	6.2	1.1229	-5.0825
45166			1.1208	-4.0258
45182	3502	7.7	1.1173	-3.8776
45197			1.1244	-4.2585
45213	2314	8.8	1.1222	-4.2335
45228			1.1565	-4.3635
45243	3030	6.5	1.1835	-4.2287
45258			1.1661	-3.8493
45274	3909	6.9	1.1627	-3.426
45289			1.1553	-3.8944
45304	2183	6.6	1.1429	-3.7925
45319			1.1332	-3.2881
45335	2178	7.1	1.1203	-3.2176
45350			1.1265	-2.2157
45366	2446	8.1	1.1095	-2.0806
45381			1.1101	-1.191 <i>7</i>

				. a man y
Modified	No. of	RMS Orbital	Solar	Along-Track
Julian Date	Observations	Fits (cm)	Radiation	Acceleration (pms <sup>-2</sup> )
45394	1869	11.1	1.1265	602
45409	1007	11.1	1.125	271
45425	2205	8.4	1.1393	2655
	2200	0.1	1.1428	.1857
45440 45455	2537	7.6	1.1574	5038
45455 45470	2557	7.0	1.1575	-3.1332
45470 45486	2589	9	1.1611	-2.9613
45486 45501	2507	,	1.161	-3.4197
	2672	5.6	1.1527	-3.092
45516 45521	20/2	3.0	1.1545	-3.0632
45531 45547	2480	5.1	1.1441	-3.3554
45547	2400	5.1	1.137	-3.2343
45562 45570	2318	5.6	1.1271	-3.214
45578	2310	5.0	1.1349	-3.1989
45593	3587	6.1	1.1258	-3.4637
45608 45603	3307	0.1	1.1351	-3.2198
45623	4936	5.5	1.1292	-3.6929
45639	4930	5.5	1.125	-3.4116
45654	3841	7.3	1.1281	-3.5824
45669	3041	7.5	1.1163	-3.4547
45684	3142	4.9	1.1226	-3.3891
45700	3142	4.7	1.1232	-3.6416
45715	2715	6.5	1.1177	-3.5093
45731	3715	6.3	1.1283	-3.9162
45746	2450	( )	1.1187	-4.2225
45760	3450	6.4	1.12	-3.5713
45775	0000	( )	1.1264	-3.6294
45791	2833	6.2	1.0832	-3.5639
45806	45702	4.5	1.0232	-3.5384
45821	4793	4.5	1.129	-3.6068
45836	F.7700	-	1.1146	-3.6033
45852	5702	5	1.1238	-3.7565
45867	E07.4	4.0	1.1145	-3.8422
45882	5864	4.8	1.1172	-3.7066
45897	E010	4.0	1.172	-3.1624
45913	5818	4.8	1.1127	-2.6732
45928	(101		1.1203	-2.353
45944	6424	5.5	1.1193	-2.0985
45959	(004	4.6	1.1193	-2.4637
45974	6234	4.6	1.1216	-2.4499
45989	F1F0	4.6	1.1212	-4.0118
46005	5159	4.6	1.1212	-3.7948
46020	4040	. <b>.</b>	1.1203	-3.9216
46035	4012	6.7	1.1256	-4.0359
46050		5.4	1.128	-3.8881
46066	3314	5.4	1.0876	-3.6712
46081	2000	4.7	1.1231	-4.1745
46097	2800	4.6	1.1423	-3.686
46112		7.1		-3.8633
46125	2574	7.1	1.1296	-3.8913
46140		2.4	1.1245	-3.728
46156	3315	6.1	1.1274	-3.728 -4.5108
46171			1.1282	-4.5106 -5.5091
46186	4654	4.6	1.1255	
46201			1.1217	-6.3306

N.C. 1101 . 1	<b>N</b> 7 (	D. (0.01)		
Modified Julian Date	No. of Observations	RMS Orbital	Solar	Along-Track
Julian Date	Observations	Fits (cm)	Radiation	Acceleration (pms <sup>-2</sup> )
46217	5001	5.3	1.1214	-5.911
46232			1.1158	-5.5183
46247	6437	4.9	1.1186	-4.8522
46262			1.1142	-4.9711
46278	7075	6.1	1.1108	-3.9831
46293			1.1096	-4.0532
46309	<b>67</b> 16	9.1	1.1098	-3.7499
46324			1.1107	-4.3427
46339	7913	10.4	1.1191	-3.7191
46354			1.1558	-4.097
46370	5991	5.5	1.1482	-3.4171
46385			1.147	-3.7849
46400	5054	4.7	1.1368	-3.2954
46415			1.1343	-3.3324
46431	4659	5.4	1.1223	-2.895
46446			1.122	-3.1987
46462	5852	5.1	1.1186	-3.0303
46477			1.1174	-2.5206
<b>464</b> 90	4551	6.1	1.1155	-2.0623
46505			1.122	-1.3313
46521	4883	7.1	1.1265	<i>-</i> 1.4788
46536			1.1276	<b>4</b> 626
46551	5362	3.9	1.1312	4773
46566			1.132	6038
46582	3385	3.3	1.1337	8318
46597			1.1409	-3.3955
46612	3446	3.5	1.137	-3.9451
46627			1.1397	-3.8253
46643	2954	2.9	1.1423	-3.7748
46658			1.144	-3.9511
46674	3310	3.1	1.1352	-3.92
46689			1.1361	-3.6052
46704	3818	3.4	1.1277	-3.5587
46719			1.1297	-3.9735
46735	5120	3.3	1.1267	-3.9104
46750			1.1243	-4.218
46765	4231	3.4	1.1203	-4.5314
46780	20/5		1.1212	-4.3632
46796	3967	3.2	1.1165	-4.3669
46811	2100		1.1165	-4.2098
46827	3122	4.6	1.1105	-4.0998
46842	4000	2.0	1.1058	-3.9666
46855	4923	2.9	1.1135	-4.635
46870	2500	•	1.1138	-4.1636
46886	3580	3	1.1171	-4.1359
46901	4701	2	1.101	-4.0771
46916	4691	3	1.0956	-3.7686
46931	AEQ.4	2	1.0537	-4.1248
46947	4584	3	1.1804	-3.7953
46962 46077	4500	2.0	1.1482	-3.8995
46977	4509	3.2	1.1345	-3.8833
46992	(000	2	1.1284	-4.1012
47008 47003	6099	3	1.1335	-3.9268
47023			1.1261	-3.8328

Modified Julian Date	No. of Observations	RMS Orbital Fits (cm)	Solar Radiation	Along-Track Acceleration (pms <sup>-2</sup> )
47039	5961	3.5	1.1271	-2.7571
47054	3901	5.0	1.1272	-1.8035
	5353	3.6	1.1283	-1.2671
47069	3333	5.0	1.1323	-1.4784
47084	5627	3.2	1.1295	-1.9348
47100	3027	3.2	1.1214	-2.7165
47115	4609	2.8	1.1217	-3.649
47130	4009	2.0	1.1154	-3.7019
47145	2474	3	1.1169	-3.5981
47161	3474	3	1.1126	-3.5492
47176	0047	2.6	1.0893	-3.6347
47192	2947	2.0	1.079	-3.7639
47207	0644	2.4	1.1305	-3.837
47221	3644	2.6	1.1282	-4.24
47236	440	2.0	1.1332	-3.7016
47252	4187	2.8	1.1272	-4.0004
47267		2.5	1.1312	-4.2891
47282	2916	2.5		-5.4043
47297		• •	1.1242	-5.2901
47313	3459	2.4	1.125	-5.4717
47328			1.1266	-5.2868
47343	4104	2.8	1.1255	
47358			1.1214	-5.2904 5.2267
47374	4217	2.6	1.1194	-5.2367 5.0375
47389			1.1157	-5.0275
47405	5257	2.1	1.1091	-3.9358
47420			1.111	-3.9656
47435	5714	3.5	1.1183	-4.3256
47450			1.1276	-4.6788
47466	6376	3.3	1.1222	-3.8629
47481			1.1498	-4.3328
47496	4897	3.1	1.149	-4.174
47511			1.1513	-4.0852
47527	3374	3.2	1.147	-3.8852
47542			1.1321	-3.8618
47558	5 <b>7</b> 95	3.3	1.1279	-3.5565
47573			1.1293	-4.016
47586	5874	2.9	1.1128	-4.187
47601			1.1207	-3.2773
47617	4702	4	1.1242	-2.9768
47632			1.127	-1.8453
47647	3865	2.9	1.1292	-1.2332
47662			1.1256	5245
47678	5315	2.8	1.1352	0379
47693	<del></del>		1.1459	.1708
47708	3602	3	1.1447	-3.6613
47723	200-		1.1532	-4.1793
47739	3562	3	1.1628	-3.4679
47754	2002	-	1.1754	-4.7764

## LAGEOS Geodetic Analysis - SL7.1

Appendix 4

Polar Motion and Earth Rotation Values

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
760506	029	.26394	.414	.44757	14.693	.00000	
760506 760508.5	~.029	.20394	.414	.44/3/	14.093	.00000	3.186
760511	.002	.22072	.416	.27852	14.709	.02148	
760513.5 760516	.030	.13069	.417	.25166	14.725	.02327	3.166
760518 760518.5	.050	.13009	.417	.23100	14.723	.02327	3.140
760521	.057	.09514	.417	.11739	14.741	.02276	
760523.5 760526	.085	.09642	.415	.12225	14.756	.02302	3.040
760528.5	.005	.07042	.415	.12223	14.750	.02302	2.872
760531	.111	.08593	.408	.16036	14. <i>77</i> 0	.02302	2 (10
760533.5 760605	.131	.10716	.401	.13708	14.783	.00000	2.648
760607.5							2.446
760610 760613 E	.145	.09284	.396	.13708	14.796	.00818	2.284
760612.5 760615	.156	.09437	.394	.14271	14.807	.00767	2.204
760617.5							2.190
760620 760622.5	.164	.08056	.390	.13171	14.818	.00818	2.182
760625	.173	.08721	.382	.12864	14.829	.00844	2.102
760627.5 760620	1770	15/07	260	17000	14 040	00001	2.214
760630 760632.5	.179	.15627	.368	.17008	14.840	.00921	2.342
760705	.176	.19719	.353	.68056	14.852	.00000	
760707.5 760710	.174	9.09620	.340	3.96040	14.864	.00000	2.474
760710 760712.5	.174	7.07020	.540	3.90040	14.004	.00000	2.552
760715	.179	.60435	.331	.52813	14.877	.03146	0.557
760717.5 760720	.198	.45166	.328	.35473	14.890	.02634	2.576
760722.5							2.584
760725 760727.5	.219	.34246	.325	.23095	14.903	.02327	2.548
760727.5 760730	.225	1.11990	.312	.39591	14.915	.00000	2.340
760732.5							2.516
760804 760806.5	.214	.55473	.279	.25166	14.928	.00000	2.526
760809	.189	.45166	.223	.27852	14.941	.01637	
760811.5 760814	.154	.00000	.158	.00000	14.954	.00000	2.580
760814 760816.5	.134	.0000	.130	.00000	14.534	.00000	2.644
760819	.130	1.31820	.112	1.84400	14.967	.00000	
760821.5 760824	.135	.33632	.107	.31560	14.980	.02762	2.668
760826.5							2.580
760829	.181	.29079	.154	.32583	14.993	.03402	2.25/
760831.5 760903	.248	.45575	.220	.19258	15.004	.00000	2.256
760905.5							2.182
760908 760910.5	.289	.31560	.244	.17008	15.015	.02916	2.492
760910.3 760913	.290	.88082	.234	.37340	15.028	.00000	2.492
760915.5	250		20/	(0000	45.040	~~	2.950
760918 760920.5	.258	1.47900	.206	.60230	15.042	.07494	3.306
760923	.214	.32174	.176	.19258	15.059	.04271	
760925.5 760928	190	.08900	.157	.07724	15 075	.03785	3.304
760928 760930.5	.180	.00900	.13/	.07724	15.075	.03/65	3.160
761003	.167	.09182	.146	.10742	15.091	.00000	
761005.5 761008	.164	.12020	.137	.06471	15.107	.00716	3.130
76100 <del>6</del> 761010.5	.104	.12020	.13/	.004/1	13.107	.007.10	3.252
761013	.161	.09719	.125	.06522	15.123	.00895	
761015.5 761018	.154	.09335	.112	.07084	15.140	.00895	3.342
761018 761020.5	.134	,07000	.112	.0/004	13.140	.00093	3.374
761023	.142	.10205	.100	.07826	15.157	.00870	
761025.5 761028	.131	.07826	.089	.06522	15.174	.00895	3.372
761028 761030.5	.131	.07020	.007	.00322	13.174	.0093	3.334

		v oi		y sigma	A1-UT1R	A1-UT1R	ΔLOD
Date	X (#)	x sigma (")	y (")	y sigita (")	(s)	sigma (s)	(ms)
YYMMDD	(")						(12.0)
761102 761104.5	.117	.07673	.082	.06471	15.190	.00000	3.224
761104.3 761107	.102	.05780	.080	.04450	15.206	.00486	3.066
761109.5 761112	.085	.07263	.080	.04962	15.222	.00537	
761114.5						WE88	2.946
761117	.068	.07366	.080	.04527	15.236	.00588	2.958
761119.5 761122	.052	.07519	.079	.05831	15.251	.00563	3.056
761124.5	.037	.09821	.075	.07954	15.267	.00588	3.036
761127 761129.5						~~~	3.114
761202 761204 5	.023	.06343	.069	.04629	15.282	.00000	3.102
761204.5 761207	.005	.09182	.065	.06547	15.298	.00614	2 004
761209.5	014	.06752	.062	.05371	15.313	.00486	3.034
761212 761214.5	014					20512	2.968
761217	029	.09003	.060	.06854	15.328	.00512	2.804
761219.5 761222	044	.09540	.056	.07647	15.342	.00691	2710
761224.5	059	.24143	.050	.10026	15.355	.01458	2.710
761227 761229.5	039	.24143					2.730
770101	077	.32788	.048	.56522	15.369	.00000	2.818
770103.5 770106	099	.17391	.054	.11841	15.383	.03018	2.024
770108.5	100	.23939	.070	.12532	15.398	.03120	2.934
<i>77</i> 0111 <i>77</i> 0113.5	123	.23737	.070				3.040
<i>77</i> 0116	144	.14783	.095	.09693	15.413	.02839	3.020
<i>77</i> 0118.5 <i>77</i> 0121	159	.10563	.118	.09233	15.428	.02813	
770123.5	1/0	12420	.132	.11176	15. <del>44</del> 2	.02839	2.870
770126 770128.5	169	.12430	.132				2.700
<i>77</i> 0131	180	.14834	.143	.11867	15.456	.00000	2.654
<i>77</i> 0133.5 <i>77</i> 0205	196	.10921	.154	.09667	15.469	.01023	
770207.5	21/	.10972	.169	.05217	15.483	.01100	2.754
770210 770212.5	216	.10972	.107				2.928
770215	229	.11535	.186	.05703	15.497	.01202	2.952
770217.5 770220	238	.17008	.207	.07954	15.512	.01304	2.020
770222.5	238	.16164	.226	.09054	15.526	.01432	2.838
770225 770227.5	230						2.748
770302 770304 5	232	.17826	.243	.09258	15.540	.00000	2.812
770304.5 770307	223	.38977	.259	.19974	15.554	.02046	2.986
770309.5 770312	214	.12711	.275	.05933	15.569	.01151	
<i>7</i> 70314.5					15 505	.01177	3.106
770317 770319.5	207	.09744	.294	.04987	15.585		3.196
770322	202	.07724	.312	.05933	15.601	.01125	3.244
770324.5 770327	199	.12481	.331	.13069	15.617	.01330	
770329.5				.08056	15.633	.00000	3.216
770401 770403.5	195	.10384	.350	OCUOU.			3.228
770406	187	.06445	.369	.04962	15.649	.00793	3.298
770408.5 770411	175	.07008	.386	.06343	15.666	.00895	
770413.5			400	.05575	15.682	.00844	3.356
<i>77</i> 0416 <i>77</i> 0418.5	163	.07059	.402	.03373			3.308
770421	152	.06931	.418	.05422	15.699	.00793	3.212
770423.5 770426	139	.07724	.434	.07570	15.715	.00895	
770428.5							3.102

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
770501	125	.07442	.446	.05985	15.730	.00000	·
770503.5 770506	104	.07212	.452	.06010	15.746	.00563	3.022
770508.5 770511	082	.09335	.457	.07826	15.760	.00665	2.972
770513.5 770516	060	1.18590	.461	1.63150	15.775	.00000	2.914
770518.5 770521	040	.18645	.469	.27647	15.789	.01253	2.844
770523.5 770526	026	.11662	.480	.14501	15.803	.01100	2.730 2.502
770528.5 770531 770533.5	014	.14348	.493	.12916	15.815	.00000	2.356
770605 770607.5	.003	.13836	.503	.08900	15.827	.00895	2.324
770610 770612.5	.025	.07775	.506	.05678	15.839	.00972	2.324
770612.5 770615 770617.5	.048	.06266	.504	.06010	15.850	.01023	2.190
770620 770622.5	.072	.11151	.501	.07519	15.861	.00997	2.016
770625 770625 770627.5	.091	.06445	.499	.05601	15.871	.00972	1.820
770630 770632.5	.104	.08875	.498	.06905	15.880	.00000	1.718
770705 770707.5	.114	.06598	.495	.05908	15.889	.00486	1.726
770710 770712.5	.130	.06650	.486	.07187	15.898	.00588	1.806
770715 770717.5	.150	.07877	.470	.06931	15.907	.00563	1.922
770720 770722.5	.171	.06240	.455	.07084	15.916	.00588	2.002
770725 770727.5	.190	.09437	.441	.10051	15.926	.00716	1.974
770730 770732.5	.207	.07187	.431	.07826	15.936	.00563	1.880
770804 770806.5	.222	.07673	.417	.07928	15.945	.00000	1.818
770809 770811.5	.238	.06266	.397	.06777	15.955	.00512	1.834
770814 770816.5	.254	.08977	.374	.10384	15. <del>964</del>	.00691	1.960
770819 770821.5	.267	.09591	.351	.131 <i>7</i> 1	15.974	.00870	2.296
770824 770826.5	.272	.07800	.334	.08159	15.985	.00665	2.684
770829 770831.5	.275	.11151	.323	.12097	15.998	.00742	2.970
770903 770905.5	.274	.09437	.312	.10844	16.013	.00000	3.032
770908 770910.5	.271	.10921	.297	.11560	16.028	.00742	2.912
770913 770915.5	.268	.85396	.281	.38977	16.043	.03581	2.792
770918 770920.5	.267	.09693	.263	.21662	16.057	.00946	2.790
770923 770925.5 770928	.267 .264	.20588	.242 .222	.33632	16.071 16.085	.01586	2.864
770926 770930.5 771003	.254	.37340	.207		16.100	.01995	2.976
771003 771005.5 771008	.234	.09079 .07468	.195	.06419	16.115	.00000	3.082
771008 771010.5 771013	.240	.08823	.193	.07417	16.131	.00512	3.158
771013 771015.5 771018	.222	.08056	.164	.05933	16.147	.00514	3.222
771018 771020.5 771023	.219	.07954	.164	.06880	16.147	.00588	3.244
771023 771025.5	.219	.U/33 <del>4</del>	.141	.00000	10.104	.00300	3.224

					A1-UT1R	A1-UT1R	ΔLOD
Date	X ((()	x sigma (")	y (")	y sigma (")	(s)	sigma (s)	(ms)
YYMMDD	(")	<u> </u>				.00512	
771028	.215	.07417	.119	.07622	16.180		3.162
771030.5 771102	.207	.08031	.101	.09540	16.196	.00000	3.146
771104.5	.196	.08082	.088	.07417	16.211	.00588	
771107 771109.5	,170				17.007	.00767	3.180
771112	.178	.09974	.078	.07826	16.227	.00767	3.184
771114.5 771117	.154	.08491	.071	.05933	16.243	.00588	3.112
771119.5	.131	.07110	.063	.06496	16.259	.00614	
771122 771124.5					1/ 274	.00639	3.002
771127	.111	.07673	.053	.08056	16.274	.00039	2.888
771129.5 771202	.096	.06343	.041	.06522	16.288	.00000	2.900
771204.5	.081	.07647	.032	.05857	16.303	.00537	2.900
771207 771209.5	.001	.0/04/				00543	3.054
771212	.063	.06880	.023	.05780	16.318	,00563	3.318
<i>77</i> 1214.5 <i>77</i> 1217	.038	.07826	.009	.07622	16.334	.00563	3.498
771219.5	.004	.34450	009	.20844	16.352	.00000	3.470
771222 771224.5	.004				14 270	.00000	3.528
771227	027	.86215	023	.60026	16.370	.0000	3.396
771229.5 780101	053	.55473	024	.16036	16.387	.00000	3.148
780103.5	068	.23504	008	.17980	16.402	.01688	
780106 780108.5	000				16 417	.01049	2.900
780111 780112 5	074	.17059	.010	.11790	16.417	.01049	2.828
780113.5 780116	076	.12941	.024	.19386	16.431	.01330	2.870
780118.5	083	.12506	.034	.19565	16.445	.00844	
780121 780123.5	005				17.471	.00000	3.038
780126	097	.08159	.039	.09949	16.461	.0000	3.246
780128.5 780131	119	.15652	.040	.24143	16.477	.00000	3.426
780133.5 780205	152	.82916	.046	.63529	16.494	.00000	
780203 780207.5				00000	16.512	.00000	3.540
780210 780212.5	183	.00000	.059	.00000	16.512		3.566
780215	198	.50742	.078	.51969	16.529	.00000	3.506
780217.5 780220	195	.53223	.096	.24143	16.547	.04245	
<b>780222</b> .5				.48670	16.564	.09846	3.434
780225 780227.5	184	1.60690	.109	.40070			3.520
780302	185	.78184	.122	.32583	16.582	.00000	3.604
780304.5 780307	203	.63734	.138	.29284	16.600	.05038	
780309.5			.157	.21253	16.618	.02992	3.586
780312 780314.5	223	.63120	.137				3.470
780317	239	.55473	.178	.16164	16.635	.01662	3.340
780319.5 780322	241	.53223	.199	.17545	16.652	.01253	
780324.5		E10EE	217	.17417	16.668	.00000	3.294
780327 780329.5	236	.51355	.217				3.292
780401	225	.14118	.234	.08107	16.685	.00000	3.324
780403.5 780406	215	.09412	.249	.06343	16.701	.00767	
780408.5			2/7	.07008	16.718	.01074	3.356
780411 780413.5	208	.10921	.267				3.374
780416	204	.09923	.288	.05703	16.735	.01049	3.400
780418.5 780421	199	.10614	.311	.06471	16.752	.00972	
780423.5							3.396

Date	X	x sigma	y	y sigma	A1-UT1R	A1-UT1R	ΔLOD
YYMMDD	(")	(")	(")	(")	(s)	sigma (s)	(ms)
780426	192	.10051	.334	.07928	16.769	.00972	224
780428.5 780501	179	.12813	.352	.10256	16.786	.00000	3.364
780503.5 780506	166	.10077	.366	.06547	16.802	.00895	3.278
780508.5							3.176
780511 780513.5	153	.08747	.379	.05473	16.818	.00895	3.156
780516 780518.5	145	.09028	.392	.05473	16.834	.00895	
780521	137	.12251	.409	.07519	16.850	.00895	3.158
780523.5 780526	124	.10486	.430	.07366	16.865	.00921	3.094
780528.5	_						2.920
780531 780533.5	104	.16471	.451	.18824	16.880	.00000	2.694
780605 780607.5	084	.10716	.465	.11151	16.893	.00767	2.460
780610	071	.09079	.469	.07622	16.905	.00767	2.460
780612.5 780615	060	.09489	.470	.06471	16.917	.00793	2.260
780617.5 780620	045	.17954	.473	.11304	16.927	.00921	2.076
780622.5							1.918
780625 780627.5	029	.11253	.479	.10051	16.937	.00972	1.802
780630 780632.5	014	.33836	.484	.21049	16.946	.00000	
780705	.002	.10921	.489	.17621	16.955	.00767	1.810
780707.5 780710	.020	.16803	.494	.16522	16.964	.00895	1.908
780712.5							1.942
780715 780717.5	.037	.16138	.498	.14987	16.974	.00972	1.896
780720 780722.5	.055	.47033	.497	.21662	16.983	.00000	1.820
780725	.073	.19540	.490	.10614	16.993	.01049	
780727.5 780730	.087	.13683	.480	.15831	17.001	.00997	1.764
780732.5 780804	.098	.10332	.471	.13785	17.010	.00000	1.818
780806.5							1.982
780809 780811.5	.110	.10051	.464	.10614	17.020	.00537	2.220
780814 780816.5	.122	.10486	.458	.07826	17.031	.00614	
780819	.135	.08286	.450	.07008	17.044	.00614	2.418
780821.5 780824	.146	.07084	.441	.06675	17.056	.00588	2.534
780826.5 780829	.157	.12379	.431	.10358	17.069	.00665	2.564
780831.5							2.540
780903 780905.5	.167	.14706	.421	.18568	17.082	.00000	2.524
780908 780910.5	.177	.14859	.411	.16675	17.094	.00665	
780913	.189	.13095	.400	.13811	17.107	.00716	2.540
780915.5 780918	.198	.12302	.388	.09105	17.120	.00742	2.590
780920.5 780923	.205	.06854	.377		17.134		2.734
780925.5				.06292		.00742	2.940
780928 780930.5	.208	.08235	.365	.07136	17.148	.00793	3.110
781003	.212	.08133	.350	.07238	17.164	.00000	
781005.5 781008	.216	.06624	.332	.06215	17.180	.00614	3.166
781010.5 781013	.221	.06931	.315	.05831			3.126
781015.5					17.195	.00563	3.076
781018 781020.5	.224	.07673	.300	.06829	17.211	.00614	3.044
0.020.3							3. <del>044</del>

YYMMDD	(")	/ //\	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
		(")	(")	(")			(1115)
781023 781025.5	.224	.12890	.282	.19488	17.226	.00972	2.984
781028	.224	.11483	.262	.11662	17.241	.00895	2.988
781030.5 781102	.223	.11535	.242	.12737	17.256	.00000	3.016
781104.5 781107 781109.5	.223	.17315	.224	.14885	17.271	.01049	3.052
781112 781114.5	.218	.12379	.210	.09233	17.286	.00972	3.086
781117 781119.5	.208	.11176	.198	.09156	17.302	.00844	3.132
781122 781124.5	.196	.11151	.187	.13555	17.317	.01049	3.180
781127 781129.5	.183	.13887	.172	.13555	17.333	.01023	3.220
781202 781204.5	.173	.44348	.155	.24143	17.349	.00000	3.178
781207 781209.5	.167	.11202	.137	.09335	17.365	.01458 .01509	3.086
781212 781214.5	.164	.11662	.120	.11176	17.381 17.396	.01704	3.050
781217 781219.5	.159	.15550	.107	.15396	17.390	.01688	3.040
781222 781224.5	.149	.09233	.098 .094	.07954	17.426	.02813	3.024
781227 781229.5	.136	.51355 .07340	.089	.06215	17.441	.00000	3.030
790101 790103.5	.12 <b>4</b> .113	.08261	.080	.08977	17.457	.00563	3.082
790106 790108.5 790111	.103	.05089	.068	.05703	17.472	.00512	3.138
790113.5 790116	.093	.46419	.058	.76317	17.488	.04245	3.116
790118.5 790121	.077	.11100	.053	.17008	17.503	.01023	2.970
790123.5 790126	.059	.09437	.052	.07749	17.517	.00588	2.744
790128.5 790131	.040	.05524	.055	.04450	17.529	.00000	2.524 2.530
790133.5 790205	.023	.04066	.060	.03683	17.542	.00332	2.732
790207.5 790210	.008	.04834	.064	.04118	17.555	.00358	2.894
790212.5 790215	004	.05268	.064	.05550	17.570	.00512	2.966
790217.5 790220 790222.5	01 <b>7</b>	.13376	.065	.07187	17.585	.00409	3.056
790222.5 790225 790227.5	028	.05499	.069	.05550	17.600	.00435	3.158
790302 790304.5	039	.13299	.074	.11662	17.616	.00000	3.190
790307 790309.5	046	.06368	.077	.04629	17.632	.00588	3.162
790312 790314.5	052	.05908	.081	.05064	17.648	.00716	3.176
790317 790319.5	061	.10844	.086	.06266	17.663	.00716	3.220
790322 790324.5	073	.04987	.096	.03760	17.680	.00639	3.122
790327 790329.5	086	.05089	.108	.04987	17.695	.00665	2.936
790401 790403.5	096	.06880	.123	.08568	17.710	.00000	2.906
790406 790408.5	102	.05345	.135	.04322	17.724 17.740	.00537	3.066
790411 790413.5	106	.04808	.144	.04808	17.740 17.756	.00486	3.240
790416 790418.5	109	.04041	.155	.03683	17./30	<u>.00400</u>	3.242

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
790421	110	.03223	.169	.02813	17.772	.00460	
790423.5 790426	115	.04476	.188	.04859	17.787	.00512	3.042
790428.5 790501	145	.04706	.204	.06471	17.800	.00000	2.556
790503.5 790506	150	.07417	.216	.05013	17.814	.00435	2.712
790508.5 790511	152	.04322	.226	.03836	17.828	.00332	2.826
790513.5 790516	152	.03555	.235	.02890	17.843	.00332	2.950
790518.5 790521	152	.03376	.245	.03504	17.857	.00358	2.910
790523.5 790526	152	.04194	.256	.03836	17.871	.00358	2.672
790528.5 790531	149	.03402	.268	.03529	17.882	.00000	2.336
790533.5 790605	146	.07059	.280	.04425	17.893	.00332	2.136
790607.5 790610	143	.06112	.290	.03836	17.904	.00307	2.132
790612.5 790615	137	.04450	.301	.03632	17.915	.00307	2.206
790617.5 790620	130	.07800	.313	.03939	17.926	.00358	2.276
790622.5 790625	121	.03274	.323	.03632	17.937	.00332	2.286
790627.5 790630	112	.04757	.332	.05371	17.949	.00002	2.252
790632.5 790705	105	.05601	.343	.04245	17.960	.00435	2.224
790707.5 790710	103	.06598	.356	.05038	17.971	.00435	2.186
790710 790712.5 790715	096	.04527	.369	.03655			2.070
790717.5	087				17.981	.00384	1.894
790720 790722.5		.05627	.376	.07161	17.990	.00486	1.786
790725 790727.5	073	.05141	.380	.04041	17.999	.00435	1.814
790730 790732.5	058	.06138	.385	.03887	18.008	.00460	1.986
790804 790806.5	041	.06189	.392	.05396	18.018	.00000	2.152
790809 790811.5	021	.07238	.399	.06752	18.029	.00895	2.234
790814 790816.5	004	.06880	.404	.06061	18.040	.00460	2.234
790819 790821.5	.007	.09105	.409	.08517	18.052	.00537	2.182
790824 790826.5	.016	.04910	.415	.04629	18.062	.00409	2.078
790829 790831.5	.024	.23095	.419	.09489	18.073	.00000	2.038
790903 790905.5	.035	.29488	.422	.10102	18.083	.00000	2.104
790908 790910.5	.046	.06343	.423	.04552	18.094	.00563	2.256
790913 790915.5	.057	.04450	.422	.03223	18.105	.00460	
790918 790920.5	.069	.03146	.420	.02558	18.117	.00435	2.394
790920.5 790923 790925.5	.080	.05575	.415	.03248	18.129	.00384	2.464
790928	.090	.04348	.408	.02992	18.142	.00000	2.524
790930.5 791003	.098	.04706	.399	.02941	18.155	.00000	2.598
791005.5 791008	.102	.04220	.392	.02327	18.168	.00435	2.694
791010.5 791013	.105	.06880	.388	.02992	18.182	.00460	2.790
791015.5							2.848

Date	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
YYMMDD			.386	.01893	18.196	.00358	
791018 791020.5	.110	.02839				.00332	2.824
791023	.117	.02916	.381	.01662	18.210	.00332	2.692
791025.5 791028	.126	.03760	.372	.02378	18.224	.00358	2.528
791030.5		00146	.358	.02020	18.237	.00000	
791102 791104.5	.135	.03146	.556				2.454
791107.3	.142	.03529	.348	.02148	18.249	.00281	2.480
791109.5 791112	.144	.05882	.343	.03044	18.261	.00384	2.526
791114.5			.338	.02174	18.274	.00307	2.526
791117 791119.5	.142	.03734	.336				2.560
791122	.139	.03606	.331	.02174	18.287	.00332	2.578
791124.5 791127	.140	.02634	.319	.02404	18.300	.00281	0./10
791127 791129.5	.140		205	.02097	18.313	.00000	2.618
791202 791204 5	.143	.02558	.305	.02097			2.650
791204.5 791207	.145	.02506	.294	.01867	18.326	.00230	2.660
791209.5	.143	.02481	.287	.01816	18.339	.00256	
791212 791214.5	.143				10 252	.00281	2.624
791217	.140	.03504	.279	.02148	18.352	.00201	2.546
791219.5 791222	.138	.04425	.270	.01969	18.365	.00332	2.494
791224.5		04757	.260	.03887	18.378	.00358	
791227 791229.5	.140	.04757	.200			00000	2.526
800101	.147	.04501	.249	.02890	18.390	.00000	2.606
800103.5 800106	.145	.03683	.243	.02072	18.403	.00332	
800108.5			226	.01790	18.416	.00307	2.600
800111	.138	.02455	.236	.01790			2.620
800113.5 800116	.130	.02609	.228	.01586	18.429	.00332	2.700
800118.5 800121	.123	.02813	.220	.01739	18.443	.00332	
800121			24.4	01663	18.455	.00332	2.480
800126	.118	.03044	.214	.01662			2.364
800128.5 800131	.113	.02609	.206	.01432	18.467	.00000	2.116
800133.5	.104	.03044	.201	.01432	18.478	.00230	
800205 800207.5				01220	10.480	.00230	2.240
800210	.089	.02583	.195	.01330	18.489		2.240
800212.5 800215	.083	.02941	.188	.01407	18.500	.00230	2.660
800217.5 800220	.076	.02762	.188	.01355	18.513	.00256	
800220 800222.5				.01739	18.527	.00230	2.640
800225	.069	.02404	.183	.01/39			2.608
800227.5 800301	.069	.02813	.177	.01637	18.540	.00000	2.272
800303.5	.064	.02200	.178	.01432	18.551	.00205	
800306 800308.5					18.562	.00205	2.260
800311	.057	.02148	.179	.01228			2.420
800313.5 800316	.048	.01790	.179	.01279	18.574	.00205	2.600
800318.5	.035	.02174	.180	.01279	18.587	.00205	
800321 800323.5					18.601	.00230	2.660
800326	.030	.03069	.183	.01944	10.001		2.712
800328.5 800331	.020	.03555	.185	.01867	18.614	.00000	2.668
800333.5	013	നാവ	.188	.01790	18.628	.00230	
800405 800407.5	.012	.02200					2.740
800410	.003	.01918	.193	.01125	18.641	.00256	2.560
800412.5							

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
800415	009	.02430	.199	.01458	18.654	.00256	(12.7)
800417.5 800420	014	.02148	.204		18.667		2.580
800422.5				.01637	10.00/	.00230	2.640
800425 800427.5	029	.02506	.208	.02353	18.680	.00256	2.566
800430	033	.04041	.214	.02506	18.693	.00000	
800432.5 800505	035	.02609	.215	.02404	18.705	.00230	2.474
800507.5 800510	037	.02685	.222	.01509	18.718	.00256	2.620
800512.5							2.520
800515 800517.5	048	.03044	.230	.01969	18.731	.00281	2.320
800520 800522.5	041	.02532	.231	.01739	18.743	.00230	
800525	049	.03529	.239	.02046	18.754	.00256	2.320
800527.5 800530	047	.02737	.245	.01944	18.765	.00000	2.192
800532.5 800604	050	.01841	.249	.01483	18.775		1.908
800606.5						.00153	2.040
800609 800611.5	051	.02097	.255	.01560	18.785	.00179	2.040
800614 800616.5	050	.02404	.258	.02123	18.795	.00230	
800619	048	.01790	.263	.01688	18.805	.00179	1.960
800621.5 800624	040	.02404	.268	.02072	18.814	.00205	1.900
800626.5 800629	057	.04194	.281				1.622
800631.5				.03018	18.823	.00000	1.438
800704 800706.5	048	.02711	.287	.02251	18.830	.00256	1.740
800709 800711.5	047	.02123	.291	.01662	18.838	.00256	
800714	036	.02583	.293	.02072	18.847	.00281	1.620
800716.5 800719	034	.02558	.299	.01790	18.854	.00281	1.560
800721.5 800724	031	.02378	.304	.01867	18.862	.00256	1.640
800726.5							1.680
800729 800731.5	028	.03171	.311	.02327	18.871	.00281	1.656
800803 800805.5	030	.01841	.311	.01509	18.879	.00000	
800808	033	.01893	.315	.01432	18.887	.00128	1.584
800810.5 800813	028	.01483	.317	.01151	18.895	.00128	1.620
800815.5 800818	025	.01483	.319	.01279	18.904	.00128	1.680
800820.5							1.820
800823 800825.5	023	.01714	.324	.01458	18.913	.00128	1.900
800828 800830.5	022	.01893	.328	.01330	18.922	.00153	
800902	023	.02020	.329	.01381	18.932	.00000	2.012
800904.5 800907	023	.01893	.331	.01432	18.944	.00153	2.288
800909.5 800912	021	.01867	.334	.01202			2.280
800914.5					18.955	.00153	2.340
800917 800919.5	021	.01918	.338	.01355	18.967	.00153	2.300
800922 800924.5	023	.01918	.341	.01560	18.978	.00153	
800927	020	.01611	.345	.01381	18.990	.00128	2.420
800929.5 801002	015	.02404	.344	.01637	19.003	.00000	2.430
801004.5							2.450
801007 801009.5	013	.02072	.347	.01407	19.015	.00153	2.480

				, ciama	A1-UT1R	A1-UT1R	ΔLOD
Date	x (")	x sigma (")	y (")	y sigma (")	(s)	sigma (s)	(ms)
YYMMDD					19.027	.00153	
801012 801014.5	011	.01611	.352	.01304	19.027		2.620
801017	008	.01816	.357	.01534	19.040	.00153	2.580
801019.5 801022	004	.01637	.360	.01 <b>177</b>	19.053	.00153	
801024.5				01.400	19.067	.00179	2.700
8010 <b>27</b> 8010 <b>2</b> 9.5	001	.02123	.361	.01483	19.007		2.794
801101	.002	.01816	.363	.01330	19.081	.00000	2.846
801103.5 801106	.005	.01714	.364	.01100	19.095	.00128	
801108.5	010	.01944	.368	.01509	19.107	.00179	2.380
801111 801113.5	.010						2.380
801116	.019	.02302	.369	.01662	19.119	.00153	2.460
801118.5 801121	.027	.01867	.370	.01228	19.131	.00153	2.440
801123.5 801126	.034	.02148	.371	.01279	19.143	.00153	
801128.5					19.156	.00000	2.486
801201 801203.5	.038	.02916	.370	.01765	19.156		2.834
801206	.047	.02404	.371	.01637	19.170	.00179	2.420
801208.5 801211	.052	.02148	.372	.01355	19.182	.00179	
801213.5		.02353	.370	.01714	19.194	.001 <i>7</i> 9	2.380
801216 801218.5	.057	.02333					2.300
801221	.063	.02583	.367	.01816	19.205	.00205	2.400
801223.5 801226	.060	.05703	.368	.03453	19.217	.00256	2.436
801228.5 801231	.075	.02609	.356	.02072	19.229	.00000	
801233.5				00507	19.242	.00230	2.444
810105 810107.5	.081	.03529	.352	.02.506			2.300
810110	.085	.05166	.353	.04220	19.253	.00281	2.480
810112.5 810115	.083	.03453	.349	.02072	19.266	.00230	
810117.5		.05243	.344	.03862	19.278	.00307	2.560
810120 810122.5	.087						2.400
810125	.083	.03887	.340	.02302	19.290	.00205	2.230
810127.5 810130	.090	.03146	.333	.02097	19.302	,00000	1.970
810132.5 810204	.094	.03044	.329	.01637	19.311	.00205	
810206.5			.326	.03504	19.322	.00358	2.180
810209 810211.5	.100	.07136					2.200
810214	.097	.03478	.322	.02430	19.333	.00230	2.280
810216.5 810219	.094	.02609	.323	.02685	19.345	.00205	2.240
810221.5 810224	.092	.03504	.311	.01867	19.356	.00230	
810226.5				.01330	19.369	.00000	2.696
810301 810303.5	.089	.02020	.311				2.764
810306	.093	.01688	.308	.00997	19.383	.00179	3.020
810308.5 810311	.095	.01483	.305	.00946	19.398	.00179	2.880
810313.5	.096	.01688	.301	.00997	19.413	.00179	
810316 810318.5					19.426	.00179	2.660
810321 810323.5	.100	.01688	.296	.01202			2.520
810326	.105	.02097	.292	.01688	19.439	.00179	2.496
810328.5 810331	.110	.02941	.290	.01688	19.451	.00000	
810333.5		.02455	.283	.01662	19.462	.00205	2.264
810405 810407.5	.108	.02433	.203	.01002			2.600

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
							(1110)
810410 810412.5	.108	.01534	.279	.01177	19.475	.00179	2.820
810415	.104	.01611	.270	.01407	19.490	.00205	2 000
810417.5 810420	.103	.02148	.265	.01586	19.504	.00205	3.000
810422.5 810425	.099	.02404	.263	.01355	19.519	.00205	2.900
810427.5	-						2.390
810430 810432.5	.098	.02123	.263	.01407	19.531	.00000	2.270
810505	.102	.02506	.255	.01534	19.542	.00179	
810507.5 810510	.100	.02302	.253	.01330	19.554	.00179	2.420
810512.5							2.240
810515 810517.5	.101	.02378	.250	.01534	19.566	.00179	2.400
810520	.098	.02916	.247	.01458	19.578	.00179	
810522.5 810525	.103	.08286	.238	.04834	19.590	.00256	2.520
810527.5							2.354
810530 810532.5	.092	.04527	.243	.04476	19.602	.00000	2.346
810604	.092	.02046	.231	.01637	19.614	.00205	
810606.5 810609	.089	.02378	.229	.01304	19.624	.00230	2.140
810611.5	.082	.01918	.227	.01432	10.625	.00230	2.040
810614 810616.5	.062	.01910	.227	.01432	19.635	.00230	1.880
810619 810621.5	.081	.01739	.220	.01279	19.644	.00205	1.740
810624	.079	.02072	.217	.01279	19.653	.00230	1./40
810626.5 810629	.074	.01918	.212	.01432	19.660	.00000	1.440
810631.5							.960
810704 810706.5	.069	.02225	.208	.01560	19.665	.00153	1.300
810709	.068	.01662	.203	.01228	19.671	.00153	
810711.5 810714	.068	.01867	.196	.01228	19.677	.00153	1.140
810716.5 810719	.067	.01944	.191	.01330	19.683	.00153	1.160
810721.5	.007		.171	.01330	19.003	.00155	1.340
810 <b>72</b> 4 810 <b>72</b> 6.5	.061	.02174	.191	.01662	19.689	.00153	1.540
810729	.057	.01611	.188	.01279	19.697	.00153	
810731.5 810803	.044	.02762	.185	.02634	19.705	.00000	1.588
810805.5							1.652
810808 810810.5	.039	.02072	.185	.02097	19.713	.00153	1.720
810813	.028	.01969	.183	.01560	19.722	.00179	
810815.5 810818	.022	.01611	.183	.01304	19.729	.00153	1.500
810820.5 810823	.013	.01611	.182	01270	10 777		1.520
810825.5				.01279	19.737	.00153	1.520
810828 810830.5	.008	.01611	.182	.01355	19.745	.00179	1.502
810902	001	.02302	.188	.01125	19.752	.00000	1.502
810904.5 810907	009	.02251	.190	.01714	19.761	.00153	1.778
810909.5							1.680
810912 810914.5	017	.01714	.193	.01228	19. <b>769</b>	.00153	1.900
810917	026	.01381	.194	.01023	19.779	.00153	
810919.5 810922	033	.01509	.200	.01151	19.790	.00153	2.200
810924.5							2.320
810927 810929.5	044	.01355	.205	.01023	19.802	.00153	2.274
811002	057	.02200	.210	.01586	19.813	.00000	
811004.5							2.146

				w ciama	A1-UT1R	A1-UT1R	ΔLOD
Date	x (")	x sigma (")	y (")	y sigma (")	(s)	sigma (s)	(ms)
YYMMDD				.00997	19.824	.00128	
811007 811009.5	066	.01688	.214	.00997			2.220
811012	071	.01893	.220	.01228	19.835	.00153	2.400
811014.5 811017	074	.01739	.228	.01125	19.847	.00153	
811019.5			220	.00946	19.859	.00128	2.440
811022 811024.5	081	.01432	.238	,00940			2.460
811027	090	.03632	.248	.02148	19.871	.00230	2.406
811029.5 811101	093	.02404	.253	.01816	19.883	.00000	
811103.5	007	017700	.264	.01560	19.895	.00153	2.294
811106 811108.5	096	.01790	.204				2.220
811111	102	.01969	.268	.01125	19.906	.00179	2.340
811113.5 811116	105	.02481	.279	.01560	19.917	.00205	
811118.5	102	.02813	.287	.01355	19.928	.00205	2.180
811121 811123.5	102						2.200
811126	102	.04731	.297	.02276	19.939	.00281	2.114
811128.5 811201	102	.04373	.311	.01432	19.950	.00000	2.266
811203.5 811206	106	.03657	.318	.01560	19.961	.00230	2.200
811208.5					10.072	00081	2.300
811211 811213.5	107	.05064	.332	.02200	19.973	.00281	2.280
811216	101	.02685	.343	.01279	19.984	.00256	2.340
811218.5 811221	100	.02813	.353	.01279	19.996	.00256	
811223.5					20.007	.00281	2.120
811226 811228.5	094	.03146	.361	.01765	20.007		2.090
811231	089	.02046	.374	.01228	20.017	.00000	2.070
811233.5 820105	079	.01586	.383	.01100	20.027	.00128	
820107.5			201	.01100	20.038	.00153	2.140
820110 820112.5	066	.02276	.391	.01100	20.036		2.140
820115	055	.02839	.398	.01407	20.049	.00153	2.020
820117.5 820120	048	.05166	.403	.02378	20.059	.00332	
820122.5	028	.03887	.411	.01816	20.069	.00230	1.980
820125 820127.5	038	.03007	.411				1.914
820130 820133 5	034	.02941	.421	.01253	20.078	.00000	1.906
820132.5 820204	027	.01893	.426	.00972	20.088	.00153	
820206.5 820209	017	.02430	.431	.01458	20.098	.00179	2.080
820211.5	017					2000	2.120
820214 820216.5	.002	.03248	.429	.01739	20.109	.00205	2.320
820219	.009	.01893	.435	.01100	20.120	.00153	2.240
820221.5 820224	.021	.02404	.437	.01483	20.132	.00179	
820226.5						.00000	2.676
820301 820303.5	.038	.02506	.442	.01381	20.145	.0000	2.624
820306	.048	.01816	.442	.01074	20.158	.00153	2.360
820308.5 820311	.064	.02455	.439	.01202	20.170	.00179	
820313.5					20.181	.00179	2.320
820316 820318.5	.070	.02609	.438	.01432	20.101		2.320
820321	.089	.03350	.431	.01611	20.193	.00230	2.420
820323.5 820326	.097	.02430	.428	.02200	20.205	.00230	
820328.5				.01407	20.218	.00000	2.640
820331 820333.5	.112	.02378	.430	.0140/	20.210	.00000	2.680

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
820405	.125	.03913	.428	.01816	20.232	.00256	
820407.5 820410	.134	.02634	.420	.01586	20.245	.00205	2.700
820412.5 820415	.139	.01790	.415	.01074	20.259	.00153	2.700
820417.5							2.500
820420 820422.5	.150	.03146	.409	.03095	20.271	.00256	2.720
820425 820427.5	.162	.02276	.401	.02148	20.285	.00179	2.374
820430	.163	.03120	.384	.03146	20.297	.00000	
820432.5 820505	.178	.01151	.384	.01049	20.308	.00230	2.266
820507.5 820510	.182	.01867	.374	.01228	20.320	.00256	2.460
820512.5 820515	.190	.01202	.361	.00946	20.331	.00230	2.140
820517.5							2.100
820520 820522.5	.201	.01100	.348	.00921	20.342	.00230	2.180
820525 820527.5	.207	.01253	.337	.00921	20.353	.00230	1.980
820530 820532.5	.213	.06010	.324	.03453	20.362	.00000	1.960
820604	.216	.01586	.314	.01279	20.372	.00205	
820606.5 820609	.227	.01202	.298	.01407	20.383	.00205	2.120
820611.5 820614	.233	.01381	.283	.01407	20.392	.00205	1.940
820616.5 820619	.236	.01841	.266	.01509	20.402	.00205	1.880
820621.5							1.780
820624 820626.5	.237	.01228	.254	.00921	20.411	.00205	1.690
820629 820631.5	.233	.01483	.243	.01739	20.419	.00000	1.310
820704 820706.5	.231	.01458	.229	.01125	20.426	.00102	1.440
820709 820711.5	.227	.00972	.215	.00767	20.433	.00102	
820714	.227	.01023	.198	.00716	20.440	.00102	1.420
820716.5 820719	.219	.01509	.187	.01074	20.447	.00128	1.420
820721.5 820724	.213	.01611	.173	.01023	20.454	.00128	1.360
820726.5 820729	.206	.01304	.161	.00921	20.461	.00102	1.420
820731.5							1.336
820803 820805.5	.199	.01432	.149	.01125	20.468	.00000	1.144
820808 820810.5	.194	.01611	.138	.01125	20.473	.00102	1.360
820813 820815.5	.188	.01381	.125	.00972	20.480	.00102	1.640
820818	.174	.01586	.115	.00946	20.489	.00102	
820820.5 820823	.162	.02097	.105	.01151	20.497	.00128	1.760
820825.5 820828	.148	.01458	.097	.01074	20.507	.00128	1.920
820830.5 820902	.133	.01381	.089	.00946	20.518	.00000	2.168
820904.5 820907							2.232
820909.5	.119	.01534	.083	.00972	20.529	.00128	2.300
820912 820914.5	.100	.01202	.079	.00895	20.540	.00128	2.160
820917 820919.5	.088	.01330	.073	.01023	20.551	.00128	2.300
820922	.070	.01151	.068	.00870	20.563	.00128	
820924.5 820927	.049	.01330	.067	.00870	20.574	.00128	2.300
820929.5							2.326

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
	.034	.01023	.069	.00742	20.586	.00000	
821002 821004.5						.00102	2.434
821007 821009.5	.014	.01151	.069	.00742	20.598	.00102	2.280
821009.3 821012	002	.01304	.071	.00793	20.609	.00128	2.280
821014.5 821017	021	.01432	.076	.00742	20.621	.00128	
821019.5			000	00716	20.632	.00102	2.220
821022 821024.5	036	.01100	.078	.00716			2.200
821027	050	.01330	.082	.00716	20.643	.00128	2.196
821029.5 821101	068	.01228	.087	.00972	20.654	.00000	2.544
821103.5	078	.01355	.096	.00870	20.667	.00128	2.544
821106 821108.5					20.670	.00153	2.420
821111 821113.5	098	.01355	.104	.01304	20.679		2.520
821116	111	.01969	.118	.01125	20.691	.00179	2.520
821118.5 821121	125	.02865	.130	.01509	20.704	.00205	
821123.5	143	.02481	.141	.01304	20.716	.00205	2.440
821126 821128.5						.00000	2.446
821201 821203.5	147	.01739	.150	.01100	20.728		2.714
821206	163	.01688	.164	.01151	20.742	.00128	2.480
821208.5 821211	170	.01483	.182	.01074	20.754	.00128	
821213.5		01220	.203	.00793	20.767	.00128	2.500
821216 821218.5	182	.01228					2.540
821221	188	.01765	.224	.01253	20.779	.00153	2.500
821223.5 821226	193	.02634	.242	.01995	20.792	.00153	2.542
821228.5 821231	193	.01560	.253	.01074	20.805	.00000	
821233.5				.00691	20.817	.00102	2.558
830105 830107.5	197	.01023	.269				2.500
830110	202	.01304	.286	.00716	20.830	.00128	2.620
830112.5 830115	203	.01202	.302	.00895	20.843	.00102	2.900
830117.5 830120	201	.01228	.323	.01100	20.858	.00102	
830122.5				.00972	20.874	.00128	3.200
830125 830127.5	194	.01509	.340				2.836
830130	187	.01688	.356	.01355	20.888	.00000	2.904
830132.5 830204	184	.01151	.379	.00997	20.902	.00102	3.040
830206.5 830209	1 <i>7</i> 7	.01586	.394	.00997	20.917	.00128	
830211.5				.01483	20.932	.00128	2.920
830214 830216.5	173	.01330	.409				2.780
830219	168	.01125	.426	.01074	20.946	.00102	2.900
830221.5 830224	161	.01381	.444	.00946	20.961	.00128	3.054
830226.5 830301	153	.01637	.456	.00946	20.976	.00000	
830303.5					20.991	.00128	3.026
830306 830308.5	145	.01355	.470	.01049			2.820
830311	132	.01304	.488	.00921	21.005	.00128	2.940
830313.5 830316	121	.01151	.500	.00793	21.020	.00102	
830318.5	105	.01253	.513	.00895	21.034	.00102	2.940
830321 830323.5							2.920
830326 830328.5	084	.01279	.526	.01100	21.049	.00128	2.986
050320.3							

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
		, ,					(1113)
30331 30333.5	061	.01151	.533	.00818	21.064	.00000	2 224
30405	042	.01458	.543	.01330	21.081	.00102	3.334
330407.5	.012	.01100	.0.10	.01000	21.001	.00102	2.900
330410	020	.01100	.550	.00921	21.095	.00077	
330412.5	~~	00007	555	007700	21.100	000	2.760
330415 330417.5	.002	.00997	.555	.00793	21.109	.00077	2.800
830420	.021	.01534	.561	.00972	21.123	.00102	2.000
830422.5							2. <b>72</b> 0
830425	.040	.01534	.561	.00946	21.136	.00102	
830427.5 830430	.066	.01586	.547	.02813	21.149	.00000	2.586
330430 330432.5	.000	.01500	.347	.02613	21.149	.00000	2.194
330505	.082	.01100	.554	.01483	21.160	.00102	2.174
330507.5							2.320
330510	.100	.01151	.550	.01177	21.172	.00102	
330512.5 330515	.120	01202	EAE	01100	21 104	00100	2.460
330517.5	.120	.01202	.545	.01100	21.184	.00102	2.500
330520	.142	.011 <b>77</b>	.542	.01202	21.197	.00102	2.500
330522.5							2.280
330525	.164	.01253	.538	.01381	21.208	.00102	<u>.</u>
330527.5 330530	.183	በ15ፈብ	.514	01/22	21 221	00000	2.478
830532.5	.103	.01560	.514	.01432	21.221	.00000	2.382
830604	.196	.01279	.505	.01074	21.233	.00077	2.302
830606.5							2.100
830609	.210	.01355	.494	.01100	21.243	.00102	
330611.5 330614	.226	.01330	400	01100	21 254	00100	2.120
330614 330616.5	.226	.01550	.482	.01100	21.254	.00102	2.060
330619	.242	.01228	.468	.01202	21.264	.00077	2.000
330621.5							1.940
830624	.258	.01074	.455	.00972	21.274	.00077	
830626.5 830629	.267	.01611	431	01700	21 202	00000	1.706
830631.5	.207	.01011	.431	.01790	21.282	.00000	1.594
830704	.279	.02174	.411	.01355	21.290	.00102	1.574
330706.5						_	1.340
330709	.290	.05371	.393	.02123	21.297	.00153	
330711.5 330714	.299	.01100	.370	.01049	21.303	.00102	1.180
330714 330716.5	.233	.01100	.370	.01049	21.505	.00102	1.340
330719	.311	.01407	.351	.01125	21.309	.00102	1.540
330721.5							1.480
330724	.319	.01100	.333	.00997	21.317	.00102	
330726.5 330729	.326	.01023	.313	.00946	21 224	00100	1.480
330731.5	.320	.01023	.313	.00740	21.324	.00102	1.556
830803	.328	.01125	.293	.00997	21.332	.00000	1.550
830805.5							1.524
830808	.330	.01074	.272	.00895	21.340	.00077	
330810.5 330813	.330	.01151	.249	.00997	21.348	.00077	1.660
330815.5	.330	.01131	.247	.0077/	41.348	.000//	1.680
330818	.327	.00972	.230	.00972	21.356	.00077	1.000
330820.5							1.720
30823	.321	.01611	.206	.01458	21.365	.00102	
330825.5 330828	.316	.01534	.186	.01432	21.374	.00128	1.720
330830.5	.510	.01334	.100	.01432	21.3/4	.00128	1.694
330902	.304	.01151	.167	.01228	21.382	.00000	1.074
330904.5							1.606
30907	.294	.00767	.146	.00844	21.390	.00077	
30909.5	260	00001	130	00047	21 200	00100	1.740
330912 330914.5	.280	.00921	.128	.00946	21.399	.00102	1.800
330917	.268	.00716	.111	.00767	21.408	.00077	1.000
330919.5	. =		· •				1.780
330922	.253	.00716	.094	.00716	21.417	.00077	
30924.5							1.860

				v, ciama	A1-UT1R	A1-UT1R	ΔLOD
Date	x (")	x sigma (")	y (")	y sigma (")	(s)	sigma (s)	(ms)
YYMMDD				.00946	21.426	.00102	
830927 830929.5	.236	.00870	.077	.00946			2.270
831002	.217	.00997	.063	.01100	21.437	.00000	2.230
831004.5 831007	.202	.00639	.051	.00742	21.448	.00077	
831009.5				00743	21.459	.00102	2.180
831012	.183	.00691	.040	.00742	21.439		2.060
831014.5 831017	.164	.00742	.033	.00742	21.470	.00102	2.000
831019.5	.143	.00742	.026	.00742	21.480	.00102	
831022 831024.5						.00102	2.180
831027	.119	.00588	.018	.00614	21.490	.00102	2.484
831029.5 831101	.098	.00793	.016	.00691	21.503	.00000	2.796
831103.5	.075	.00972	.015	.00716	21.517	.00077	
831106 831108.5	.073					.00077	2.500
831111	.054	.00895	.014	.00665	21.529	.00077	2.380
831113.5 831116	.031	.00818	.016	.00767	21.541	.00077	2.340
831118.5	010	.00793	.021	.00665	21.553	.00077	2.340
831121 831123.5	.010	.00793				00077	2.260
831126	010	.00946	.026	.00921	21.564	.00077	2.162
831128.5 831201	031	.00767	.032	.00870	21.575	.00000	2.000
831203.5	054	000	.037	.00716	21.586	.00077	2.098
831206 831208.5	051	.00716	.037				1.980
831211	067	.00844	.044	.00742	21.596	.00077	1.980
831213.5 831216	082	.00895	.055	.00716	21.605	.00077	
831218.5		00005	.066	.00767	21.615	.00077	1.960
831221 831223.5	097	.00895	.000	.00707			1.960
831226	110	.00870	.078	.01279	21.625	.00102	1.994
831228.5 831231	122	.00563	.088	.00716	21.635	.00000	
831233.5		00588	.102	.00588	21.646	.00051	2.186
840105 840107.5	135	.00588	.102				1.860
840110	149	.00665	.117	.00537	21.655	.00077	1.600
840112.5 840115	160	.00563	.132	.00563	21.663	.00077	1 400
840117.5		.00588	.147	.00486	21.671	.00051	1.480
840120 840122.5	171						1.480
840125	184	.00563	.164	.00588	21.678	.00077	1.424
840127.5 840130	195	.00767	.179	.00742	21.685	.00000	1.356
840132.5	204	.00921	.193	.00844	21.692	.00077	
840204 840206.5	204				21 (00	.00077	1.520
840209	211	.00563	.212	.00537	21.699		1.620
840211.5 840214	219	.00665	.226	.00767	21.708	.00102	1.680
840216.5	224	.00588	.244	.00512	21.716	.00077	
840219 840221.5					01 777	00077	1.740
840224	230	.00793	.263	.00588	21.725	.00077	1.730
840226.5 840229	235	.00588	.282	.00588	21.733	.00000	1.650
840231.5	237	.00844	.303	.00639	21.742	.00077	
840305 840307.5							1.940
840310	238	.00639	.324	.00844	21.751	.00077	1.960
840312.5 840315	231	.00639	.345	.00742	21.761	.00077	2.040
840317.5		.00614	.366	.00614	21 <i>.7</i> 71	.00077	
840320 840322.5	224	.0014		.00011	======		2.060

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
340325	221	.00665	.386	.00588	21.782	.00077	(1113)
140327.5 140330	212	.00537	.404	.00614			2.054
340332.5		.00537	.404	.00614	21.792	.00000	1.866
340404 340406.5	201	.00665	.422	.00563	21.801	.00077	1.860
340409	188	.00563	.441	.00512	21.810	.00077	
840411.5 840414	174	.00460	.460	.00435	21.820	.00077	1.980
840416.5 840419	159	.00537	.475	.00563	21.831	.00077	2.040
840421.5							2.060
840424 840426.5	146	.00460	.491	.00460	21.841	.00077	1.982
840429 840431.5	130	.00537	.504	.00486	21.851	.00000	
340504	113	.00486	.518	.00435	21.861	.00051	1.958
340506.5 340509	092	.00512	.530	.00486	21.869	.00051	1.780
340511.5							1.680
840514 840516.5	076	.00512	.541	.00460	21.878	.00051	1.520
340519 340521.5	058	.00409	.547	.00358	21.885	.00051	
340524	038	.00435	.554	.00358	21.893	.00051	1.520
840526.5 840529	017	.00537	.558	.00435	21.901	.00000	1.488
840531.5 840603	.005	.00384	.561	.00358			1.492
840605.5					21.908	.00051	1.200
840608 840610.5	.027	.00537	.560	.00409	21.914	.00051	1.100
840613 840615.5	.048	.00460	.559	.00384	21.920	.00051	
840618	.069	.00435	.557	.00409	21.925	.00051	1.080
840620.5 840623	.088	.00588	.554	.00639	21.930	.00051	1.040
840625.5 840628							1.002
340630.5	.108	.00409	.548	.00384	21.935	.00000	.838
340703 340705.5	.131	.00537	.541	.00563	21.939	.00051	.580
340708	.152	.00486	.532	.00486	21.942	.00051	
340710.5 340713	.171	.00512	.521	.00409	21.945	.00051	.620
3 <b>407</b> 15.5 3 <b>407</b> 18	.191	.00563	.509	.00460	21.948	00051	.600
840720.5						.00051	. <i>7</i> 20
840723 840725.5	.211	.00512	.495	.00435	21.952	.00051	.860
340728 340730.5	.230	.00563	.482	.00537	21.956	.00051	
340802	.246	.00435	.468	.00384	21.961	.00000	.892
340804.5 340807	.262	.00460	.452	.00435	21.965	.00051	.768
340809.5 340812	.275						.960
340814.5		.00486	.434	.00409	21.969	.00051	1.200
340817 340819.5	.289	.00512	.417	.00435	21.975	.00051	1.340
340822	.298	.00435	.399	.00358	21.982	.00051	
340824.5 340827	.302	.00563	.380	.00409	21.988	.00051	1.200
340829.5 340901	.305	.00460	.360	.00435			1.398
340903.5					21.995	.00000	1.682
140906 140908.5	.309	.00460	.344	.00384	22.003	.00051	1.300
40911	.312	.00460	.323	.00384	22.010	.00051	
40913.5 40916	.314	.00537	.303	.00435	22.017	.00051	1.420
40918.5							1.560

Date	х	x sigma	у	y sigma	A1-UT1R	A1-UT1R	ΔLOD
YYMMDD	(")	(")	(")	(")	(s)	sigma (s)	(ms)
840921	.317	.00486	.285	.00358	22.025	.00051	1.480
840923.5 840926	.319	.00512	.266	.00409	22.032	.00051	1.568
840928.5 841001	.319	.00563	.247	.00460	22.040	.00000	1.712
341003.5 341006	.314	.00614	.228	.00460	22.049	.00051	1.760
841008.5 841011	.305	.00639	.209	.00435	22.057	.00051	1.740
841013.5 841016	.296	.00460	.190	.00409	22.066	.00051	1.640
841018.5 841021	.288	.00537	.175	.00460	22.074	.00051	1.840
841023.5 841026	.281	.00460	.160	.00435	22.083	.00051	1.840
841028.5 841031	.269	.00460	.143	.00384	22.093	.00000	1.660
841033.5 841105	.257	.00537	.129	.00512	22.101	.00051	1.680
841107.5 841110	.245	.00691	.114	.00512	22.109	.00051	1.500
841112.5 841115	.232	.00767	.101	.00512	22.117	.00051	1.620
841117.5 841120	.220	.00563	.091	.00512	22.125	.00051	1.740
841122.5 841125	.204	.00844	.080	.00767	22.134	.00077	1.692
841127.5 841130	.187	.00563	.069	.00486	22.142	.00000	1.848
841132.5 841205	.167	.00588	.056	.00486	22.151	.00051	1.620
841207.5 841210	.147	.00639	.046	.00588	22.160	.00051	1.420
841212.5 841215	.124	.00563	.039	.00537	22.167	.00051	1.320
841217.5 841220	.099	.00614	.032	.00537	22.173	.00051	1.300
841222.5 841225	.076	.01049	.027	.01100	22.180	.00128	1.786
841227.5 841230	.058	.01355	.024	.00870	22.189	.00000	1.754
841232.5 850104	.040	.00844	.023	.00818	22.197	.00128	1.680
850106.5 850109	.019	.00793	.025	.00614	22.206	.00128	1.640
850111.5 850114	0.000	.00072	.030	.00793	22.214	.00128	1.600
850116.5 850119	015	.00895	.035	.00639	22.222	.00102	1.500
850121.5 850124	032	.00716	.043	.00588	22.229	.00102	1.424
850126.5 850129	050	.01049	.049	.00870	22.237	.00000	1.316
850131.5 850203	063	.01074	.059	.00972	22.243	.00077	1.200
850205.5 850208	076	.01355	.067	.00870	22.249	.00102	1.280
850210.5 850213	088	.00793	.079	.00639	22.256	.00077	1.560
850215.5 850218	103	.00793	.090	.00793	22.263	.00102	1.660
850220.5 850223	121	.00844	.100	.00818	22.272	.00077	1.578
850225.5 850228	137	.01049	.113	.00895	22.280	.00000	1.582
850230.5 850305	150	.01509	.127	.00742	22.288	.00102	1.800
850307.5 850310	168	.01407	.141	.00870	22.296	.00102	2.040
850312.5 850315	178	.00844	.158	.00588	22.307	.00077	2.100
850317.5							

Date	X (")	x sigma (")	y (")	y sigma (")	A1-UT1R	A1-UT1R	ΔLOD
YYMMDD	(")	(")	(~)	(")	(s)	sigma (s)	(ms)
850320	186	.00793	.179	.00614	22.317	.00077	
850322.5 850325	191	.00946	.199	.00691	22.327	.00102	2.020
850327.5	171	.00740	.177	.00071	22.527	.00102	1.980
850330 850333 5	192	.00895	.217	.00691	22.337	.00102	1.004
850332.5 850404	196	.00742	.239	.00486	22.346	.00000	1.824
850406.5							1.876
850409 850411.5	194	.00716	.258	.00537	22.356	.00077	1 920
850411.5	191	.00665	.278	.00512	22.365	.00051	1.820
850416.5							2.000
850419 850421.5	188	.00691	.295	.00588	22.375	.00051	1.920
350424	186	.00639	.313	.00512	22.384	.00051	1.920
850426.5	100	20500	221	00500	00.000	000	1.800
850429 850431.5	188	.00588	.331	.00537	22.393	.00077	1.826
850504	182	.00691	.347	.00588	22.403	.00000	
850506.5 850500	174	.00665	.365	00513	22 412	00051	2.014
850509 850511.5	1/4	.00000	.363	.00512	22.413	.00051	1.660
350514	164	.00588	.383	.00460	22.421	.00051	
850516.5 850519	153	.00639	.398	.00486	22.429	.00051	1.540
850521.5	155	.00039	.570	.00400	22.427	.0001	1.440
850524	138	.00614	.411	.00486	22.436	.00051	
850526.5 850529	124	.00767	.425	.00639	22.443	.00077	1.360
350531.5							1.438
850603 850605.5	110	.00793	.436	.00870	22.450	.00000	1 5/0
850608	100	.00563	.447	.00512	22.458	.00077	1.562
850610.5	000	00510	400	00.400			1.280
350613 350615.5	090	.00512	.457	.00409	22.464	.00077	1.180
850618	078	.00563	.465	.00435	22.470	.00077	1.100
850620.5 850623	064	.00563	.472	.00435	22.475	.00077	1.080
850625.5	-,004	.00000	.4/2	.00433	22,475	.00077	1.120
350628	049	.00537	.478	.00435	22.481	.00077	
350630.5 350703	034	.00563	.483	.00588	22.485	.00000	.878
350705.5							.522
350708 350710.5	019	.00512	.486	.00486	22.488	.00051	500
350710.3 350713	0.000	.00060	.490	.00060	2.490	.00051	.500
350715.5	045						.600
850718 850720.5	.017	.00460	.492	.00409	22.493	.00051	.620
850723	.034	.00460	.495	.00460	22.497	.00051	
850725.5 850728	.049	.00486	.494	.00486	22 500	00051	.660
850730.5	,∪ <del>1</del> 7	. <del>UU100</del>	.474	.00400	22.500	.00051	.692
350802	.065	.00512	.494	.00435	22.503	.00000	
850804.5 850807	.081	.00588	.492	.00512	22.508	.00051	.908
850809.5						.00001	.620
350812	.099	.00486	.488	.00486	22.511	.00051	
350814.5 350817	.116	.00460	.484	.00486	22.514	.00051	.640
350819.5							.800
350822 350824.5	.132	.00409	.481	.00435	22.518	.00051	040
350824.5 350827	.146	.00460	.475	.00460	22.522	.00051	.840
350829.5							.976
350901 850002 5	.159	.00435	.465	.00512	22.527	.00000	1 224
350903.5 350906	.173	.00435	.456	.00460	22.533	.00051	1.224
50908.5							1.060
150911 150913.5	.185	.00409	.449	.00435	22.539	.00051	1 100
13.3							1.120

					A 1 I ITID	A1-UT1R	ΔLOD
Date	X	x sigma	<b>y</b>	y sigma	A1-UT1R	sigma (s)	(ms)
YYMMDD	(")	(")	(")	(")	(s)		(1115)
850916 850918.5	.195	.00435	.438	.00486	22.544	.00051	1.360
850921	.202	.00409	.426	.00435	22.551	.00051	1.420
850923.5 850926	.213	.00409	.417	.00460	22.558	.00051	1.534
850928.5 851001	.219	.00435	.403	.00486	22.566	.00000	1.806
851003.5 851006	.223	.00486	.388	.00486	22.575	.00051	1.700
851008.5 851011	.229	.00435	.372	.00512	22.583	.00051	1.800
851013.5 851016	.232	.00435	.358	.00486	22.592	.00051	1.820
851018.5 851021	.234	.00512	.343	.00512	22.601	.00051	1.900
851023.5 851026	.234	.00665	.325	.00614	22.611	.00077	1.898
851028.5 851031	.237	.00665	.318	.00588	22.620	.00000	1.962
851033.5 851105	.234	.00588	.301	.00486	22.630	.00051	1.640
851107.5 851110	.235	.00435	.289	.00460	22.638	.00051	1.680
851112.5 851115	.235	.00486	.275	.00486	22.647	.00077	1.720
851117.5 851120	.234	.00614	.260	.00486	22.655	.00077	1.760
851122.5 851125	.235	.00793	.250	.00691	22.664	.00077	1.726
851127.5 851130	.232	.00537	.240	.00818	22.673	.00000	1.954
851132.5 851205	.226	.00486	.228	.00486	22.683	.00077	1.660
851207.5 851210	.220	.00691	.217	.00665	22.691	.00077	1.580
851212.5 851215	.214	.00588	.205	.00563	22.699	.00077	1.440
851217.5 851220	.210	.00435	.195	.00409	22.706	.00077	1.420
851222.5 851225	.203	.00793	.181	.00895	22.713	.00102	1.222
851227.5 851230	.199	.00767	.176	.00870	22.719	.00000	1.198
851232.5 860104	.189	.00716	.164	.00614	22.725	.00077	1.200
860106.5 860109	.175	.00512	.155	.00409	22.731	.00077	1.320
860111.5 860114	.165	.00435	.144	.00512	22.738	.00077	1.460
860116.5 860119	.154	.00486	.136	.00460	22.745	.00077	1.460
860121.5 860124	.141	.00460	.131	.00409	22.752	.00077	1.556
860126.5 860129	.128	.00563	.125	.00486	22.760	.00000	1.824
860131.5 860203	.113	.00818	.122	.00588	22.769	.00077	1.600
860205.5 860208	.101	.00639	.119	.00537	22.777	.00051	1.540
860210.5 860213	.089	.00537	.115	.00537	22.785	.00051	1.500
860215.5 860218	.077	.00588	.113	.00614	22.792	.00077	1.320
860220.5 860223	.063	.00614	.114	.00639	22.799	.00077	1.490
860225.5 860228	.045	.00537	.114	.00537	22.807	.00000	1.370
860230.5 860305	.031	.00537	.114	.00486	22.813	.00051	1.400
860307.5 860310 860312.5	.016	.00742	.117	.00716	22.820	.00077	1.240

Date	X	x sigma	y	y sigma	A1-UT1R	A1-ÚT1R	ΔLOD
YMMDD	(")	(")	(")	(")	(s)	sigma (s)	(ms)
360315	.003	.00665	.119	.00742	22.827	.00077	
360317.5	000		,	007.47			1.060
860320 860322.5	008	.00588	.122	.00563	22.832	.00051	1 200
860322.5 860325	016	.00742	.130	.00512	22.838	.00051	1.200
860327.5		.507 46			22,030	1	1.436
860330	033	.00665	.133	.00895	22.845	.00000	
860332.5 860404	043	.00486	.140	.00486	22.853	.00077	1.584
860406.5	043	.00400	.140	.00400	22.833	.000//	1.580
860409	052	.00537	.149	.00435	22.861	.00077	1.500
860411.5 860414	058	00/01	1/1	00573	22.000	000	1.620
860414 860416.5	036	.00691	.161	.00563	22.869	.00077	1.680
860419	064	.00665	.173	.00614	22.877	.00077	1.000
860421.5							1.560
860424 860426 5	071	.00486	.182	.00435	22.885	.00077	
860426.5 860429	079	.01228	.188	.00716	22.893	.00000	1.620
860431.5		JILLU	.100	.00710	22.093		1.840
860504	080	.00895	.200	.00588	22.903	.00102	
860506.5 860509	084	.00793	210	00500	22.011	00100	1.700
860511.5	004	.00/93	.210	.00588	22.911	.00102	1.560
860514	087	.00639	.222	.00588	22.919	.00102	1.500
860516.5	600	000-0					1.200
860519 860521.5	089	.00818	.234	.00639	22.925	.00102	1 200
860524	093	.01151	.244	.00997	22.931	.00102	1.200
860526.5	.070			.00///	22.551	.00102	1.112
860529	094	.00946	.254	.00767	22.936	.00000	
860531.5 860603	095	.00844	.262	.00588	22.942	.00077	1.088
860605.5	073	.000**	.202	.00000	22.742	.000//	.760
860608	096	.00844	.275	.00588	22.946	.00077	.700
860610.5 860613	000	nno <del>m</del> e	204	00/00		00-05	.520
860613 860615.5	092	.00870	.284	.00639	22.948	.00102	.460
860618	082	.01023	.293	.00767	22.951	.00102	.400
860620.5	A=-	0.5.5					.840
860623 860625.5	076	.01560	.307	.01202	22.955	.00128	
860628	069	.01458	.316	.01100	22.959	.00000	.772
860630.5							.848
860703	065	.01177	.323	.00870	22.963	.00128	
860705.5 860708	057	.00997	.337	.00767	22.967	00120	.800
860710.5	037	.00777	.33/	.00/0/	22.70/	.00128	.660
860713	048	.00946	.347	.00691	22.970	.00128	1000
860715.5 860718	043	വനാരാ	252	one on	22.052	00100	.620
860720.5	043	.00793	.352	.00588	22.973	.00128	.540
860723	031	.01202	.360	.00818	22.976	.00153	.540
860725.5	020	01151	2/4	00005	00.070		.660
860728 860730.5	029	.01151	.364	.00895	22.979	.00153	540
860802	017	.00997	.369	.00793	22.982	.00000	.560
860804.5							.700
860807 860809.5	010	.00716	.374	.00665	22.986	.00077	<b>PRO</b> 0
360812	004	.00844	.379	.00793	22.989	.00077	.780
360814.5		.50011	.019	.507 75	44.707	.00077	.760
360817	.002	.01151	.385	.01228	22.993	.00102	
360819.5 360822	Δ11	01040	207	00077	22.007	00100	.600
360824.5	.011	.01049	.387	.00972	22.996	.00102	.740
360827	.019	.00742	.392	.00614	23.000	.00077	./40
860829.5	000	000	<u> </u>				. <b>714</b>
360901 340003 5	.028	.00844	.394	.00614	23.003	.00000	
860903.5 860906	.035	.00716	.397	.00665	23.007	.00077	.806
		.007 10	.571	·	٠٠.٠٠٠	.000//	

Deta		y sioma		y sigma	A1-UT1R	A1-UT1R	ΔLOD
Date YYMMDD	x (")	x sigma (")	y (")	y sigilia (")	(s)	sigma (s)	(ms)
860911	.043	.00665	.397	.00537	23.013	.00077	4 000
860913.5			.398	.00665	23.018	.00077	1.080
860916 860918.5	.048	.00895					1.300
860921	.057	.00793	.396	.00844	23.025	.00077	1.480
860923.5 860926	.061	.00691	.395	.00614	23.032	.00077	1.574
860928.5 861001	.067	.00691	.393	.00563	23.040	.00000	
861003.5	.072	.00614	.392	.00588	23.049	.00077	1.786
861006 861008.5				.00537	23.057	.00077	1.600
861011 861013.5	.079	.00614	.392				1.480
861016	.086	.00563	.389	.00460	23.064	.00051	1.560
861018.5 861021	.094	.00614	.389	.00563	23.072	.00077	1.700
861023.5 861026	.097	.00793	.389	.00614	23.081	.00077	
861028.5		00018	.385	.00537	23.089	.00000	1.622
861031 861033.5	.103	.00818			23.097	.00077	1.578
861105 861107.5	.111	.00614	.380	.00512			1.240
861110	.120	.00716	.376	.00691	23.103	.00077	1.420
861112.5 861115	.126	.00691	.371	.00742	23.110	.00077	1.380
861117.5 861120	.127	.00691	.364	.00537	23.117	.00077	
861122.5		.00691	.358	.00742	23.124	.00077	1.380
861125 861127.5	.128					.00000	1.356
861130 861132.5	.130	.00972	.353	.00895	23.130		1.324
861205	.138	.00614	.346	.00588	23.137	.00102	1.240
861207.5 861210	.144	.00563	.339	.00563	23.143	.00102	1.160
861212.5 861215	.146	.00742	.331	.00563	23.149	.00102	
861217.5 861220	.148	.00742	.324	.00716	23.155	.00102	1.160
861222.5			.323	.01177	23.162	.00102	1.340
861225 861227.5	.151	.00895				.00000	1.402
861230 861232.5	.151	.00588	.314	.00537	23.169		1.498
870104	.152	.00588	.308	.00537	23.176	.00077	1.280
870106.5 870109	.153	.00512	.303	.00435	23.183	.00051	1.180
8 <b>7</b> 0111.5 8 <b>7</b> 011 <b>4</b>	.146	.00563	.294	.00332	23.188	.00051	
870116.5 870119	.148	.00614	.287	.00460	23.194	.00051	1.140
870121.5				.00460	23.200	.00077	1.220
870124 870126.5	.147	.00946	.280				1.242
870129 870131.5	.143	.00409	.274	.00332	23.206	.00000	1.598
870203	.138	.00486	.270	.00358	23.214	.00051	1.400
870205.5 870208	.136	.00409	.264	.00384	23.221	.00051	1.520
870210.5 870213	.133	.00563	.259	.00332	23.229	.00051	
870215.5		.00358	.254	.00332	23.237	.00051	1.540
870218 870220.5	.132					.00051	1.640
870223 870225.5	.131	.00384	.251	.00358	23.245		1.948
870228	.126	.00870	.245	.00563	23.255	.00000	2.192
870230.5 870305	.125	.00818	.240	.00512	23.266	.00077	1.720
870307.5							1.720

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
70310	.119	.00537	.228	.00512	23.274	.00051	
70312.5 70315	.117	.00460	.223	.00409	23.283	.00051	1.680
370317.5 370320	.116	.00460	.222	.00384	23.291	.00051	1.680
870322.5 870325	.108	.00435	.214	.00460	23.300	.00051	1.820
870327.5 870330	.105	.00588	.217	.00460	23.309	.00000	1.714
870332.5 870404	.101	.00537	.212	.00409	23.316	.00051	1.566
870406.5 870409	.096	.00332	.211	.00332	23.325	.00051	1.700
870411.5 870414	.089	.00435	.208	.00384	23.333	.00051	1.580
870416.5 870419	.079	.00409	.203	.00512	23.341	.00051	1.620
870421.5 870424	.076	.00384	.202	.00460	23.348	.00051	1.500
870426.5 870429	.073	.00460	.204	.00460	23.356	.00000	1.564
870431.5 870504	.065	.00384	.202	.00332	23.364	.00051	1.576
870506.5 870509	.061	.00332					1.360
8 <b>7</b> 0511.5			.199	.00332	23.371	.00051	1.340
870514 870516.5	.054	.00435	.199	.00384	23.378	.00051	1.280
870519 870521.5	.046	.00435	.196	.00409	23.384	.00051	1.340
870524 870526.5	.039	.00563	.196	.00537	23.391	.00051	1.430
870529 870531.5	.037	.00716	.200	.00563	23.398	.00000	1.470
870603 870605.5	.032	.00435	.197	.00486	23.405	.00077	.940
870608 870610.5	.031	.00409	.199	.00409	23.410	.00077	1.120
870613 870615.5	.025	.00358	.199	.00358	23.416	.00077	1.000
870618 870620.5	.018	.00435	.200	.00332	23.421	.00077	.960
870623 870625.5	.012	.00435	.201	.00435	23.425	.00077	
870628 870630.5	.006	.00409	.205	.00409	23.430	.00000	.842
870703 870703 870705.5	0.000	.00060	.207	.00058	3.434	.00051	.898
870708	003	.00409	.210	.00332	23.437	.00051	.660
870710.5 870713	012	.00384	.212	.00384	23.440	.00051	.560
870715.5 870718	017	.00435	.216	.00358	23.443	.00051	.540
870720.5 870723	018	.00358	.220	.00307	23.446	.00051	.540
870725.5 870728	018	.00332	.225	.00358	23.448	.00051	.440
8 <b>7</b> 0730.5 8 <b>7</b> 080 <b>2</b>	021	.00384	.228	.00384	23.450	.00000	.486
870804.5 870807	025	.00332	.233	.00332	23.454	.00026	.814
870809.5 870812	026	.00358	.237	.00332	23.457	.00020	.580
370812 370814.5 370817	028	.00384	.242	.00358			.700
870819.5					23.461	.00051	.880
370822 370824.5	029	.00435	.248	.00332	23.465	.00051	1.100
370827 370829.5	029	.00486	.257	.00409	23.471	.00051	1.098
870901 870903.5	033	.00435	.260	.00460	23.476	.00000	1.122

Date	X (")	x sigma	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
YYMMDD	(")					.00051	
870906	035	.00512	.265	.00409	23.482	.00051	1.200
870908.5 870911	034	.00384	.268	.00281	23.488	.00051	1 220
870913.5		.00384	.274	.00332	23.494	.00051	1.220
870916 870918.5	037	.00304					1.260
870921	040	.00384	.279	.00358	23.500	.00077	1.580
870923.5 870926	042	.00486	.287	.00409	23.508	.00077	1.500
870928.5		00004	.294	.00358	23.516	.00000	1.502
871001 871003.5	047	.00384	.474				1.678
871006	050	.00409	.301	.00358	23.524	.00051	1.700
871008.5 871011	051	.00384	.307	.00332	23.532	.00051	1 500
871013.5		00405	.313	.00358	23.540	.00051	1.580
871016 871018.5	054	.00435	.313	.00530			1.540
871021	055	.00435	.319	.00332	23.548	.00051	1.620
871023.5 871026	051	.00588	.324	.00512	23.556	.00051	
871028.5			.330	.00486	23.564	.00000	1.638
871031 871033.5	057	.00486	.330	.00400			1.902
871105	055	.00435	.338	.00332	23.574	.00051	1.660
871107.5 871110	051	.00512	.343	.00384	23.582	.00051	
871112.5				00050	23.591	.00051	1.780
871115 871117.5	049	.00460	.355	.00358	23.391		1.640
871120	046	.00512	.362	.00332	23.599	.00051	1.620
871122.5 871125	047	.00537	.370	.00435	23.607	.00051	
871123 871127.5			OFF	00500	23.616	.00000	1.676
871130 871132.5	054	.00844	.375	.00588	23.010		2.004
871205	051	.00614	.381	.00486	23.626	.00051	1.560
871207.5 871210	046	.00435	.388	.00358	23.633	.00051	
871212.5			207	00400	23.641	.00051	1.420
871215 871217.5	040	.00512	.396	.00409	25.041		1.480
871220	036	.00512	.401	.00460	23.648	.00051	1.600
871222.5 871225	029	.00537	.406	.00563	23.656	.00077	
871227.5				005(2	23.664	.00000	1.666
871230 871232.5	018	.00767	.411	.00563	23.004		1.614
880104	010	.00614	.415	.00512	23.672	.00077	1.560
880106.5 880109	001	.00435	.420	.00358	23.680	.00077	
880111.5			422	.00307	23.688	.00077	1.520
880114 880116.5	.005	.00384	.422				1.520
880119	.009	.00716	.424	.00512	23.695	.00077	1.160
880121.5 880124	.019	.00742	.427	.00614	23.701	.00077	
880126.5			.428	.00460	23.707	.00000	1.130
880129 880131.5	.032	.00716					1.510
880203	.045	.00460	.429	.00384	23.714	.00051	1.520
880205.5 880208	.057	.00435	.432	.00384	23.722	.00051	
880210.5		.00409	.433	.00332	23.731	.00051	1.780
880213 880215.5	.060						1.800
880218	.065	.00384	.430	.00332	23.740	.00051	1.960
880220.5 880223	.074	.00486	.431	.00486	23.750	.00051	
880225.5		ME00	.427	.00639	23.761	.00051	2.280
880228 880230.5	.076	.00588	.427	.0003	25.701		2.000
000200.0							

Date	x	x sigma	y	y sigma	A1-UT1R	A1-UT1R	ΔLOD
YMMDD	(")	(")	(")	(")	(s)	sigma (s)	(ms)
80304	.087	.00512	.433	.00460	23.771	.00051	
380306.5							2.060
380309 380311.5	.097	.00537	.430	.00409	23.781	.00051	1.640
880314	.114	.00870	.427	.00537	23.790	.00051	1.040
880316.5							1.360
880319	.122	.00537	.425	.00332	23.796	.00051	1.540
880321.5 880324	.130	.00512	.415	.00358	23.804	.00051	1.540
880326.5				.50000			1.760
880329	.137	.00614	.410	.00358	23.813	.00000	1 004
880331.5 880403	.139	.00742	.401	.00639	23.822	.00000	1.884
880405.5	.137	.007-12	.101	.0000	20.022	.00000	1.916
880408	.140	.00537	.395	.00358	23.832	.00051	
880410.5	.146	.00435	.389	.00384	23.842	.00051	2.000
880413 880415.5	.140	CCAUU.	.507	.00004	∠2.04∠	icuu.	1.980
880418	.154	.00588	.377	.00435	23.852	.00077	
880420.5	1/1	00470	077	00400	22.040	00051	1.660
880423 880425.5	.161	.00460	.376	.00409	23.860	.00051	1.560
880428	.168	.00588	.368	.00691	23.868	.00077	1.000
880430.5	4 55	0040-		0000	** ***	00000	1.632
880503 880505.5	.177	.00691	.359	.00793	23.876	.00000	1.508
880508	.176	.00537	.353	.00512	23.884	.00051	1.300
880510.5							1.580
880513	.181	.00563	.344	.00486	23.892	.00051	1 400
880515.5 880518	.183	.00409	.337	.00435	23.900	.00051	1.680
880520.5							1.380
880523	.183	.00435	.328	.00409	23.907	.00051	
880525.5 880528	.181	.00435	.318	.00358	23.914	.00051	1.400
880530.5	.101	·······································	.010		T	.50001	1.312
880602	.174	.00486	.308	.00537	23.920	.00000	
880604.5 880607	.171	.00512	.300	.00460	23.926	.00077	1.208
880609.5	.171	.00312	.500	.00400	20.920	.000//	1.040
880612	.172	.00384	.289	.00358	23.932	.00077	
880614.5 880617	.172	.00460	.281	.00460	23.936	.00077	.920
880619.5	.172	JUNEOU	.201	.UUHOU	23.730	.000//	.660
880622	.172	.00409	.270	.00332	23.940	.00077	
880624.5	176	.00460	250	00460	22 042	000	.520
880627 880629.5	.176	.UU46U	.259	.00460	23.942	.00077	.394
880702	.177	.00486	.251	.00384	23.944	.00000	
880704.5	100	00435	340	00050	22.044	00054	.426
880707 880709.5	.175	.00435	.240	.00358	23.946	.00051	.380
880712	.173	.00409	.230	.00384	23.948	.00051	.500
880714.5		004/0	202	00100	22.25-	00055	.500
880717 880719.5	.171	.00460	.222	.00409	23.951	.00051	.540
880722	.168	.00358	.211	.00332	23.953	.00051	.540
880724.5							.620
880727 880720 5	.161	.00332	.201	.00332	23.956	.00051	.576
880729.5 880801	.155	.00358	.192	.00358	23.959	.00000	.376
880803.5							.784
880806	.148	.00358	.182	.00409	23.963	.00051	F40
880808.5 880811	.141	.00358	.173	.00358	23.966	.00051	.540
880813.5	.141	.cc.so	.173	.www	£J.700	.co.	.580
880816	.134	.00358	.166	.00358	23.969	.00051	
880818.5	***	00050	•/•	00400	22.072	00054	.660
880821 880823.5	.124	.00358	.161	.00409	23.972	.00051	.580
880826	.112	.00384	.152	.00435	23.975	.00051	.000
880828.5						<del></del>	. <b>75</b> 0

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
			.149	.00639	23.979	.00000	
880831 880833.5	.102	.00537	.149	.00039			.890
880905	.090	.00409	.144	.00460	23.983	.00077	.760
880907.5 880910	.079	.00307	.139	.00332	23.987	.00077	
880912.5			-05	00050	23.991	.00077	.800
880915 880917.5	.069	.00384	.135	.00358	23.991	.00077	1.020
880920	.054	.00563	.131	.00639	23.996	.00077	1.140
880922.5 880925	.036	.00665	.127	.00793	24.002	.00102	1.140
880927.5					24.000	00000	1.190
880930	.023	.00537	.133	.00793	24.008	.00000	1.330
880932.5 881005	.003	.00332	.131	.00332	24.014	.00077	1 400
881007.5	000	.00307	.133	.00332	24.022	.00077	1.480
881010 881012.5	009	.00307	.133				1.580
881015	028	.00435	.135	.00332	24.030	.00077	1.420
881017.5 881020	044	.00537	.134	.00384	24.037	.00077	
881022.5		20/20	120	.00460	24.044	.00077	1.480
881025 881027.5	058	.00639	.139	.00400	24.044		1.560
881030	082	.00895	.146	.00767	24.052	.00077	1.736
881032.5 881104	082	.00435	.163	.00435	24.061	.00000	
881106.5				00001	04.071	.00051	2.024
881109	100	.00384	.171	.00281	24.071	.00051	1.660
881111.5 881114	111	.00384	.180	.00460	24.079	.00077	1.640
881116.5	119	.00358	.192	.00409	24.087	.00077	1.040
881119 881121.5	119	.00030				000000	1.720
881124	131	.00460	.203	.00588	24.096	.00077	1.720
881126.5 881129	137	.00818	.214	.00870	24.104	.00077	
881131.5	1.47	.00691	.237	.00409	24.113	.00000	1.680
881204 881206.5	147	,00691	.231				1.720
881209	151	.00384	.250	.00332	24.122	.00051	1.340
881211.5 881214	156	.00409	.263	.00332	24.128	.00051	
881216.5	150	00400	.278	.00563	24.134	.00077	1.160
881219 881221.5	159	.00409	.270	.00505			1.160
881224	161	.01100	.297	.01049	24.140	.00102	.960
881226.5 881229	157	.00742	.309	.01560	24.145	.00153	
881231.5		00/20	.322	.01202	24.152	.00000	1.388
890103 890105.5	154	.00639	.32.2	.01202			1.292
890108	145	.00512	.332	.00563	24.158	.00128	1.100
890110.5 890113	141	.00307	.346	.00332	24.163	.00128	
890115.5					24.170	.00128	1.220
890118 890120.5	136	.00281	.358	.00281	<b>24.17</b> 0		1.220
890123	130	.00409	.368	.00332	24.176	.00128	1.380
890125.5 890128	123	.00358	.381	.00358	24.183	.00128	
890130.5							1.454
890202 890204 5	120	.00332	.387	.00332	24.190	.00000	1.646
890204.5 890207	109	.00307	.404	.00435	24.198	.00051	1 440
890209.5	000	.00332	.412	.00307	24.205	.00051	1.460
890212 890214.5	099						1.360
890217	085	.00435	.424	.00512	24.212	.00051	1.240
890219.5 890222	076	.00563	.434	.00588	24.218	.00051	
890224.5	*** =						1.440

Date YYMMDD	x (")	x sigma (")	y (")	y sigma (")	A1-UT1R (s)	A1-UT1R sigma (s)	ΔLOD (ms)
390227	057	.00614	.449	.00537	24.226	.00051	·
390229.5 390304	046	.00537	.452	.00537	24.234	.00000	1.624
190306.5 190309	036	.00460	.461	.00384	24.242	.00051	1.696
90311.5							1.860
390314 390316.5	022	.00358	.465	.00307	24.251	.00051	1.600
390319 390321.5	007	.00486	.472	.00384	24.260	.00051	1.640
390324 390326.5	.008	.00460	.478	.00384	24.268	.00051	1.740
390329	.025	.00435	.480	.00435	24.276	.00051	1.360
390331.5 390403	.038	.00716	.477	.00460	24.283	.00000	
390405.5 390408	.057	.00384	.479	.00332	24.290	.00051	1.400
390410.5 390413	.070	.00384	.481	.00281	24.297	.00051	1.440
390415.5	.085	.00460	.481	.00332	24.305	.00051	1.560
390418 390420.5							1.900
390423 390425.5	.101	.00588	.482	.00358	24.315	.00051	2.020
890428 890430.5	.108	.00588	.483	.00409	24.325	.00051	2.020
890503 890505.5	.110	.00716	.473	.00409	24.335	.00000	1.840
890508	.127	.00460	.471	.00460	24.344	.00051	
890510.5 890513	.145	.00614	.467	.00614	24.352	.00051	1.580
890515.5 890518	.158	.00384	.457	.00409	24.360	.00051	1.640
890520.5 890523	.173	.00486	.451	.00384	24.369	.00051	1.700
890525.5			.442	.00435	24.377	.00051	1.640
890528 890530.5	.179	.00486					1.624
890602 890604.5	.195	.011 <b>7</b> 7	.437	.01049	24.385	.00000	1.636
890607 890609.5	.198	.00614	.420	.00460	24.393	.00102	1.180
890612 890614.5	.205	.00563	.414	.00435	24.399	.00102	1.240
890617	.218	.00588	.405	.00435	24.405	.00102	
890619.5 890622	.227	.00537	.396	.00384	24.411	.00102	1.120
890624.5 890627	.238	.00639	.381	.00742	24.415	.00102	.900
890629.5 890702	.239	.01355	.358	.01202	24.419	.00000	.768
890704.5							.952
890707 890709.5	.254	.01202	.347	.00665	24.424	.00179	.760
890712 890714.5	.256	.00486	.334	.00384	24.428	.00179	1.020
890717 890719.5	.264	.00409	.322	.00384	24.433	.001 <b>7</b> 9	1.060
890722	.267	.00537	.309	.00460	24.438	.00179	
890724.5 890727	.269	.00639	.292	.00537	24.444	.00179	1.100
890729.5 890801	.272	.01049	.285	.01049	24.448	.00256	.820
890803.5 890806	.267	.01074	.254	.00614	24.453	.00000	1.070
890808.5							1.010
890811 890813.5	.266	.00614	.244	.00460	24.458	.00077	1.080
890816 890818.5	.266	.00588	.230	.00358	24.464	.00077	1.200
890821	.262	.00614	.218	.00588	24.470	.00077	
890823.5							1.140

		v oioma	77	y sigma	A1-UT1R	A1-UT1R	ΔLOD
Date YYMMDD	x (")	x sigma (")	y (")	y 31g11tt (")	(s)	sigma (s)	(ms)
890826	.260	.00997	.205	.00818	24.475	.00102	
890828.5				.00921	24.480	.00128	1.020
890831 890833.5	.248	.01177	.192				1.340
890905	.245	.00870	.166	.00537	24.487	.00000	1.280
890907.5 890910	.232	.00742	.154	.00435	24.493	.00077	
890912.5		.00742	.142	.00486	24.499	.00077	1.160
890915 890917.5	.217					.00077	1.340
890920 890922.5	.208	.00512	.131	.00486	24.506		1.360
890925	.193	.00665	.121	.00486	24.513	.00077	1.540
890927.5 890930	.174	.00972	.112	.00486	24.521	.00102	
890932.5		.00895	.098	.00486	24.529	.00000	1.718
891005 891007.5	.167	.00693				.00051	1.802
891010	.145	.00870	.092	.00512	24.538		1.800
891012.5 891015	.120	.00742	.089	.00512	24.547	.00051	1.960
891017.5 891020	.102	.00460	.082	.00435	24.557	.00051	_
891022.5			.079	.00358	24.568	.00051	2.180
891025 891027.5	.084	.00486					2.100
891030	.066	.00639	.079	.00435	24.578	.00051	2.066
891032.5 891104	.050	.00691	.073	.00614	24.589	.00000	2.114
891106.5 891109	.029	.00460	.074	.00307	24.599	.00051	
891111.5				.00332	24.609	.00051	2.000
891114 891116.5	.008	.00358	.076				2.140
891119	007	.00332	.080	.00332	24.620	.00051	2.140
891121.5 891124	022	.00358	.087	.00332	24.631	.00051	2.400
891126.5	043	.00358	.096	.00307	24.643	.00051	
891129 891131.5					24.654	.00000	2.274
891204 891206.5	061	.00409	.096	.00358	24.034		2.086
891209	071	.00435	.108	.00384	24.664	.00051	1.820
891211.5 891214	084	.00409	.119	.00307	24.674	.00051	1.780
891216.5	095	.00358	.132	.00307	24.682	.00051	
891219 891221.5				.00486	24.691	.00051	1.800
891224 891226.5	103	.00716	.142	.00400			1.860
891229	121	.00972	.149	.00691	24.701	.00077	1.862
891231.5 900103	122	.01944	.175	.01534	24.710	.00000	1.858
900105.5 900108	135	.00537	.186	.00537	24.719	.00128	
900110.5				.00537	24.727	.00128	1.580
900113 900115.5	148	.00563	.199				1.580
900118	155	.00460	.212	.00691	24.735	.00128	1.680
900120.5 900123	169	.00614	.227	.00665	24.743	.00128	1.880
900125.5 900128	182	.00844	.241	.00844	24.753	.00128	
900130.5			.267	.00742	24.763	.00000	2.110
900202 900204.5	185	.00716					2.270
900207	195	.00409	.279	.00435	24.775	.00051	2.460
900209.5 900212	197	.00409	.300	.00384	24.787	.00051	2.460
900214.5 900217	193	.00358	.318	.00384	24.799	.00051	
900217	173	.50000					2.320

Date	x	x sigma	у	y sigma	A1-UT1R	A1-UT1R	ΔLOD
YYMMDD	(")	(")	(")	(")	(s)	sigma (s)	(ms)
900222	195	.00307	.336	.00307	24.811	.00051	
900224.5			1000		21.011	.00031	2.060
900227	187	.00384	.355	.00384	24.821	.00051	2.000
900229.5							2.020
900304	186	.00460	.371	.00588	24.831	.00000	2.020
900306.5							2.100
900309	183	.00358	.391	.00358	24.842	.00051	
900311.5							2.240
900314	178	.00307	.410	.00307	24.853	.00051	
900316.5							2.300
900319	175	.00256	.425	.00307	24.865	.00051	
900321.5							2.540
900324	164	.00358	.442	.00358	24.877	.00051	
900326.5						-	2.540
900329	155	.00767	.459	.00435	24.890	.00051	
900331.5							2.398
900403	141	.00460	. <b>47</b> 5	.00486	24.902	.00000	
900405.5							2.282
900408	130	.00818	.491	.00716	24.913	.00051	
900410.5							2.340
900413	111	.01151	.508	.01125	24.925	.00077	
900415.5							2.220
900418	097	.00946	.518	.00639	24.936	.00077	
900420.5					• •		2.280
900423	088	.01637	.525	.01049	24.948	.00102	00
900425.5							2.120
900428	078	.00972	.537	.00818	24.958	.00077	0
900430.5							1.906
900503	064	.00307	.550	.00384	24.968	.00000	
900505.5							1.734
900508	044	.00307	.555	.00358	24.976	.00026	
900510.5							1.820
900513	020	.00460	.565	.00486	24.986	.00051	
900515.5							1.980
900518	001	.00409	.568	.00409	24.995	.00051	
900520.5						·	2.040
900523	.018	.00435	.570	.00409	25.006	.00051	
900525.5							1.940
900528	.037	.00409	.572	.00614	25.015	.00051	
900530.5							1.814
900602	.057	.00588	.575	.00921	25.024	.00000	
900604.5							1.706
900607	.075	.00435	.574	.00460	25.033	.00077	
900609.5							1.680
900612	.098	.00691	.568	.00639	25.041	.00077	
900614.5							1.640
900617	.114	.00512	.563	.00512	25.049	.00077	
900619.5							1.560
900622	.133	.00460	.558	.00537	25.057	.00077	
900624.5							1.440
900627	.155	.00055	.002	.00506	.767	.00000	
900629.5							

## LAGEOS Geodetic Analysis - SL7.1

Appendix 5

Quarterly Station Coordinates

									C . 1 . 1 . C	. 1 D	• ••	
Stati	on	ī	atit	udo	1.	ongit	ndo	Height	Scaled S Lat.	tna. Dev Lon.	viations Ht.	
Name	Num			(")		(')	(")	(m)	(")	(")	(m)	
		` '	<u> </u>						` '	· · · · · ·	\	
April -	Iune	78	R	MS.374+0	0	637	8137.00	298.257				
GORF70	7063	39	1	13.3754230	283	10	19.9493290	19.0982000	0.0000	0.0000	.0741	
BERM70	7067	32	21	13.7601000	295	20	38.0212710	-22.7736000	.3257	.4484	7.7205	
GOLD70	7085	35	25	28.0268010	243	6	49.1247780	965.2321000	.2294	.1499	1.2732	
HAYS70 AREQ79	7091 7907	-16	37 27	21.7020270 56.6640620	288 288	30 30	44.4908810 24.7517330	91.6469000	.0041	.0063	.1201	
MOUN79	7921	31	41	3.2305150	249	<i>5</i> 0	18.9822860	2492.0584000 2352.5488000	.0030 .0036	0.0000 .0039	.0524 .0606	
ORRO79	7943	-35	37	29.7571420	148	57	17.2776140	949.0492000	.0069	.0051	.0759	
July - S				RMS.29	99+0	00	6378137	.00 298.257	•			
OTAY70	7062	32	36	2.6672790	243	9	32.9237730	988.4148000	.0025	.0022	.0519	
GORF70 BERM70	7063 7067	39 32	1 21	13.3753980 13.7760250	283 295	10 20	19.9491400	19.0927000	0.0000	0.0000	.0643	
GRAN70	7068	21	27	37.7965910	288	52	38.0782730 5.1647030	-23.1123000 -18.6289000	.0024 .0050	.0028 .0070	.0666 .1070	
WETT78	7834	49	8	41.7609350	12	52	41.1294170	661.1274000	.0044	.0061	.0792	
AREQ79	7907	-16	27	56.6840430	288	30	24.7516750	2492.2194000	.0020	0.0000	.0353	
MOUN79	7921	31	41	3.2351180	249	7	18.9841540	2352.7991000	.0030	.0031	.0611	
NATA79 ORRO79	7929 7943	-5 -35	55 37	40.1217100 29.7814900	324 148	50 57	7.3823630 17.2908480	39.5956000 948.7678000	.0036 .0064	.0027 .0043	.0544 .0774	
Onnor	7743	-55	37	27.7014700	140	3,	17.2700100	240.7070000	.0004	.0043	.0774	
Octobe	r - Dec	cem	ber'	78 RMS	5.39 <i>6</i>	5+00	63781	37.00 <b>29</b> 8.2	57			
OTAY70	7062	32	36	2.6917070	243	9	32.9585220	988.4432000	.0169	.0219	.0904	
GORF70	7063	39	1	13.3754450	283	10	19.9489560	19.8241000	.0001	0.0000	.7007	
WETT78	7834	49	8	41.7276800	12	52	41.1255280	661.0660000	.0244	.0161	.1321	
AREQ79 MOUN79	7907 7921	-16 31	27 41	56.6949790	288	30 7	24.7516220	2492.2470000	.0082	0.0000	.0400	
NATA79	7929	-5	55	3.2428730 40.1581940	249 324	50	19.0134490 7.3753480	2352.6948000 39.6561000	.01 <b>44</b> .01 <b>7</b> 5	.0190 .0065	.0983 .0595	
ORRO79	7943	-35	37	29.7434140	148	57	17.3103410	948.9819000	.0173	.0190	.0560	
January	y - Ma	rch	79	RMS.20	1+0	0	6378137.	00 298.257				
QUIN70	7051	39	58	24.5766870	239	3	37.7013770	1059.8905000	.0027	.0109	.0998	
OTAY70	7062	32	36	2.6698620	243	9	32.9258680	988.4840000	.0022	.0021	.0413	
GORF70 PATR70	7063 7069	39 28	1 13	13.3757020 40.6312180	283 279	10 23	19.9487890	19.0928000	0.0000	0.0000	.0471	
BEAR70	7082	41	56	.9053530	248	34	39.5423280 45.6647520	-23.3885000 1962.7708000	.0101 .0051	.0240 .0091	.15 <b>43</b> .1128	
GORF71	7101	39	1	16.2044620	283	10	42.9998270	8.7036000	.0022	.0024	.0553	
GORF71	7102	39	1	14.3920730	283	10	18.9472330	17.7902000	.0017	.0020	.0513	
GORF71 GORF71	7103	39	1	14.6159720	283	10	18.9427170	17.9188000	.0023	.0030	.0576	
WETT78	7104 7834	39 49	1 8	17.1332220 41.7684780	283 12	10 52	36.8791490 41.1344820	11.6082000 661.3 <b>79</b> 6000	.0386 .0059	.1587 .0187	2.5067 .1017	
AREQ79	7907	-16	27	56.6809290	288	30	24.7515660	2492.3213000	.0020	0.0000	.0306	
MOUN79	7921	31	41	3.2386850	249	7	18.9841930	2352.8391000	.0026	.0023	.0494	
NATA79 ORRO79	7929 7943	-5 25	55	40.1293690	324	50	7.3800540	39.5647000	.0038	.0035	.0515	
ORRO/9	7943	-35	37	29.7717570	148	57	17.2841050	948.9454000	.0034	.0023	.0371	
April -	June 7	79	ΒV	/IS.198+00	) 4	4 <b>3</b> 79	3137.00	298.257				
OUIN70	7051	39	58	24.5783070	239	3	37.7019600	1060.0334000	0017	0000	047	
OTAY70	7062	32	36	2.6656300	243	9	32.9338430	988.7272000	.0017 .0014	.0023 .0015	.0472 .0344	
GORF70	7063	39	1	13.3756430	283	10	19.9485960	19.1878000	0.0000	0.0000	.0359	
PATR70	7069	28	13	40.6689980	279	23	39.4648350	-23.9476000	.0051	.0076	.0617	
BEAR70 GORF71	7082 7102	41 39	56 1	.9115390 14.3961160	248 283	34 10	45.6777520	1962.5837000	.0015	.0022	.0425	
GORF71	7102	39	1	14.6204650	283	10	18.9417010 18.9461610	17.7596000 17.8773000	.0051 .0019	.0068 .0023	.1216 .0469	
GORF71	7104	39	i	17.1008020	283	10	36.9951320	10.0145000	.0014	.0023	.0409	
LURE72	7210	20	42	25.9563620	203	44	38.7377930	3068.3830000	.0024	.0032	.1968	
KOOT78	7833	52	10	42.2319180	5	48	35.2723690	93.2646000	.0102	.0169	.1627	
WETT78 AREQ79	7834 7907	49 -16	8 27	41.7628000	12	52 30	41.1218100 24.7515070	661.3984000	.0031	.0034	.0516	
MOUN79	7907 7921	31	41	56.6793410 3.2288970	288 249	30 7	18.9840040	2492.2926000 2352.9692000	.0013 .0023	0.0000 .0018	.0246 .0426	
NATA79	7929	-5	55	40.1098180	324	50	7.3576410	39.8313000	.0023	.0035	.0535	
ORRO79	7943	-35	37	29.7636500	148	57	17.2856990	949.0488000	.0031	.0021	.0350	

									caled St	nd. Devi	ations
					_		•			Lon.	Ht.
Statio	on	La	titu	de		gitu		Height			
Name	Num.	(°) (	(′)	(")	(°) (	<u>')</u>	(")	(m)	(")	(")	(m)
1 (411.10		,			· · · · · · · · · · · · · · · · · · ·						
			70	DMC 15	0.00	4	6378137.00	298.257			
July - S		ber 7	/9	RMS.15		_		19.2931000	0.0000	0.0000	.0284
GORF70	7063	39	_	13.3756700			19.9484190 39.4589010	-23.5777000	.0006	.0083	.0328
PATR70	7069	28 41	13 56	40.6764040 .9058890			45.6838360	1962.4753000	.0017	.0027	.0333
BEAR70 MCDO70	7082 7086	30	40	37.3513690		59	2.6978250	1961.5488000	.0282	.0563	.1021
HAYS70	7091	42	37	21.6942310		30	44.5010830	92.0730000	.0013	.0018	.0360 .0652
AMER70	7096	-14	20	7.5093020			30.4922100	49.1495000	.0032 .0013	.0044 .0014	.0270
OWEN71	7114	37	13	57.2214800			22.3580470	1178.1455000 93.1280000	.0013	.0175	.1782
KOOT78	7833	52	10	42.2346960	5 12		35.2897610 41.1635400	660.9303000	.0062	.0153	.1151
WETT78	7834 7835	49 43	8 45	41.7776130 16.8744910	6		16.0146750	1322.5151000	.0171	.0233	.4680
GRAS78	7835 7907	-16	27	56.6835910	288		24.7514550	2492.3154000	.0013	0.0000	.0250
AREQ79 NATA79	7929	-10 -5	55	40.1067830	324	50	7.3803510	39.6377000	.0075	.0047	.0935
ORRO79	7943	-35	37	29.7654340	148	57	17.2842160	949.0874000	.0028	.0015	.0359
Cititori											
	_		,	70 D16	C 107	. ^^	637813	37.00 298.3	257		
Octobe				-	S.137				0.0000	0.0000	.0121
GORF70	7063	39	1	13.3755960	283	10	19.9482380	19,3033000 -24,1048000	.0061	.0125	.1789
PATR70	7069	28	13	40.6792000	279 255	23 59	39.4782960 2.6257510	1961.4405000	.0005	.0006	.0107
MCDO70	7086	30 -29	40 2	37.3177620 47.4223580	255 115	20	48.2563040	241.3229000	.0015	.0010	.0169
YARA70 HAYS70	7090 7091	-29 42	37	21.7023530	288	30	44.4970160	92.0016000	.0004	.0006	.0126
AMER70	7096	-14	20	7.5200280	189	16	30.5035860	49.1775000	.0012	.0010	.0143
GORF71	7102	39	1	14.3858230	283	10	18.9498540	17.8094000	.0006	.0008	.0213
OWEN71	7114	37	13	57.2251390	241	42	22.3568110	1178.0655000	.0006	.0006 .0006	.0112 .0113
GOLD71	7115	35	14	53.9136970	243	12	29.0912840	1038.6805000	.0006 .0073	.0125	.1355
KOOT78	7833	52	10	42.2339140	5	48	35.2689950	93.2487000 1322.9725000	.0126	.0225	.3196
GRAS78	7835	43	45	16.8598400	6 288	55 30	16.0343990 24.7513970	2492.3335000	.0007	0.0000	.0124
AREQ79	7907	-16 -5	27 55	56.6793410 40.1260580	324	50	7.3697900	40.0242000	.0039	.0026	.0547
NATA79	7929 7943	-35	37	29.7614600	148	57	17.2893160	948.9758000	.0014	.0013	.0222
ORRO79	7,743	-55	0,	27.7011000							
		_		D1 40 4	00 00		/07010T	00 298.257	7		
Januar	ry - Ma	irch	80	RMS.1		_	6378137.0	•		0.0000	.0098
GORF70	7063		1	13.3756050	283	10	19.9480530	19.2617000 -23.6336000	0.0000	.0044	.0267
PATR70	7069		13	40.6745660	279	23	39.4599740	1961.4602000	.0005	.0005	.0068
MCDO70	7086		40	37.3163980	255 115	59 20	2.6281550 48.2542730	241.3522000	.0008	.0005	.0065
YARA70	7090	-29 42	2 37	47.4240070 21.6982200	288	30	44,4957870	91.9789000	.0005	.0007	.0080
HAYS70 KWAJ70	7091 7092		23	37.6891420	167	28	32.6416210	33.0453000	.0013	.0011	.0221
AMER70	7096		20	7.5127070		16	30.5097050	49.0880000	.0010	.0008	.0096
GORF71	7102		1	14.3956480		10	18.9485100	17.9648000	.0005	.0007	.011 <b>7</b> .00 <b>7</b> 6
OWEN71	7114		13	57.2237370		42	22.3580480	1178.0597000 1038.6001000	.0007 .0006	.0005 .0005	.0074
GOLD71	7115		14	53.9128220		12 48	29.0916680 35.2862380	93.3242000	.0260	.0604	.3791
KOOT78	7833			42.2215930 41.7668780		52	41.1290450	660.9669000	.0013	.0017	.0164
WETT78 AREQ79	7834 7907			56.6828770		30	24.7513450	2492.3151000	.0007	0.0000	.0117
NATA79	7929			40.1219990		50	7.3912870	39.7872000	.0034		.0346
ORRO79	7943			29.7639900		57	17.2806910	949.0370000	.0009	.0007	.0089
,	т	00	יח	MS.158+	20	627	8137.00	298.257			
•	- June						19.9478780	19.2549000	0.0000	0.0000	.0198
GORF70	7063					10 23	19.9478780 39.4280710	-23.6794000	.0022		.1271
PATR70	7069					23 59	2.6282480	1961.3492000	.0011		.0166
MCDO70						20	48.2603810	241.3457000	.0015	.0009	.0102
YARA70 HAYS70						30	44.5021200	92.0621000	.0015		.0368
KWA]70							32.6334160	32.9667000	.0019		.0233
AMER70		6 -14	20	7.518652	0 189		30.5086840	48.9788000	.0016		.0141 .0199
GORF71	710	2 39	1	14.394384			18.9461870	18.0631000	.0010		.0199
OWEN7								1178.0815000 1038.5865000			.0203
GOLD71	711								.0258		1.4876
											.0084
								39.6853000		.0024	.0297
								949.0520000		.0011	.0114
OKKO/5	, ,,,,,		,	57266							
KOOT78 AREQ79 NATA79 ORRO79	783 790 792	3 52 17 -16 19 -5	5 27 5 55	7 56.682409 5 40.122885	0 288 0 324	30 50	24.7512840 7.3603250		.0008 .0021	0.0000 0.0024	.00 .02

								•	Scaled S	tnd. Dev	viations	
Stati	ion	L	atiti	ude	Lo	ngit	tude	Height	Lat.	Lon.	Ht.	
Name	Num.	(°)	(')	(")			(")	(m)	(")	(")	(m)	
								•				
		,	00	D) (C 10	30.0	^	<b>4050105</b>	00 000 055				
July - S			80	RMS.13			6378137					
GORF70	7063	39	1	13.3756880	283	10	19.9476950	19.2039000	0.0000	0.0000	.0136	
PATR70	7069	28	13	40.6661810	279	23	39.4093900	-23.1883000	.0030	.0257	.1715	
MCDO70	7086 7090	30 -29	40	37.3166390	255	59	2.6290680	1961.5875000	.0010	.0014	.0245	
YARA70 HAYS70	7090	-29 42	2 37	47.4251120 21.7010220	115 288	20 30	48.2581720 44.4933900	241.3270000 91.9149000	.0010 .0006	.0008 .0009	.0068 .0116	
KWAJ70	7092	9	23	37.6814680	167	28	32.6293410	32.9305000	.0008	.0010	.0116	
AMER70	7096	-14	20	7.5163650	189	16	30.5125770	48.9754000	.0008	.0011	.0133	
GORF71	7102	39	1	14.3938880	283	10	18.9440090	17.8429000	.0011	.0013	.0218	
OWEN71	7114	37	13	57.2215 <b>72</b> 0	241	42	22.3552420	1178.0495000	.0007	.0013	.0157	
GOLD71	7115	35	14	53.9095860	243	12	29.0939270	1038.6294000	.0007	.0011	.0123	
LURE71	7120	20	42	27.3928830	203	44	38.2449540	3067.7111000	0.0000	.0010	.0095	
KIRK78	7805	60	13	2.2552450	24	23	40.4266700	77.7391000	.0523	.1431	.9608	
KOOT78	7833	52	10	42.2308070	5	48	35.2851020	93.5456000	.0128	.0287	.3521	
GRAS78	7835 7899	43 39	45	16.8650150	6	55	16.0232050	1322.8989000	.0154	.0248	.2288	
GORF78 AREQ79	7899 7907	-16	1 27	15.3534550 56.6816350	283 288	10 30	48.1391280 24.7523430	10.0373000 2492.2452000	.0008 .0006	.0011 .0010	.01 <b>7</b> 9 .0070	
NATA79	7929	-16 -5	55	40.1211520	324	50 50	7.3667270	39.7526000	.0015	.0010	.0070	
ORRO79	7943	-35	37	29.7651100	148	57	17.2844010	949.0135000	.0013	.0021	.0086	
Omico	7710	00	٠,	25.7 001100	110		17.2011010	717.0155666	.0007	.0007	.0000	
Octobe	er - Dec	cem	ber	80  RM	S.12!	5+0	0 <b>6378</b> :	137.00 298.2	257			
GORF70	7063	39	1	13.3757450	283	10	19.9475160	19.2079000	0.0000	0.0000	.0137	
YARA70	7090	-29	2	47.4224310	115	20	48.2593630	241.3201000	.0008	.0009	.0060	
HAYS70	7091	42	37	21.7002300	288	30	44.4918200	91.9777000	.0006	.0010	.0094	
KWAJ70	7092	9	23	37.6778890	167	28	32.6366580	32.8915000	.0010	.0014	.0162	
AMER70	7096	-14	20	7.5170240	189	16	30.5060500	49.0363000	.0008	.0012	.0150	
GORF71	7102	39	1	14.3928220	283	10	18.9456060	17.9827000	.0009	.0012	.0185	
OWEN71	7114	37	13	57.2219350	241	42	22.3568210	1178.0200000	.0005	.0010	.0093	
GOLD71 LURE71	7115 7120	35 20	14 42	53.9098940 27.3926000	243 203	12 44	29.0913800 38.2480650	1038.5704000 3067.7572000	.0006 0.0000	.0010	.0092	
KIRK78	7805	60	13	2.2809730	24	23	40.3799320	79.1077000	.0109	.0011 .0195	.0105 .1365	
KOOT78	7833	52	10	42.2143130	5	48	35.3352060	93.5391000	.0191	.0363	.2058	
WETT78	7834	49	8	41.7949040	12	52	41.1286990	660.6728000	.1111	.0609	2.4432	
GRAS78	7835	43	45	16.8746250	6	55	16.0232030	1322.7246000	.0055	.0085	.0926	
JPL 78	7896	34	12	19.9865670	241	49	39.8440400	441.6382000	.0005	.0010	.0103	
GORF78	7899	39	1	15.3571850	283	10	48.1421610	9.8922000	.0017	.0016	.0441	
AREQ79	7907	-16	27	56.6812320	288	30	24.7537180	2492.2912000	.0007	.0011	.0086	
NATA79	7929	-5 25	55	40.1171480	324	50	7.3716610	39.6695000	.0012	.0013	.0193	
ORRO79	7943	-35	37	29.7646020	148	57	17.2819960	949.0739000	.0006	.0009	.0078	
Januar	v - Ma	rch	81	RMS.13	0+0	)	6378137.	00 298.257				
QUIN70	7051	39	58	24.5820290	239	3	37.6929870	1060.0080000	.0006	.0009	.0122	
GORF70	7063	39	1	13.3757220	283	10	19.9473430	19.1953000	0.0000	0.0000	.0104	
YARA70	7090	-29	2	47.4230230	115	20	48.2586400	241.3374000	.0008	.0007	.0072	
GORF71	7102	39	1	14.3972400	283	10	18.9366710	17.9287000	.0014	.0022	.0307	
GORF71	7105	39	1	14.1754970	283	10	20.3132710	19.0845000	.0005	.0008	.0128	
PLAT71	7112	40	10	58.0097190	255	16	26.4861890	1501.6626000	.0013	.0018	.0343	
OWEN71	7114	37	13	57.2184880	241	42	22.3552950	1177.9476000	.0018	.0025	.0616	
GOLD71	7115	35	14	53.9095950	243	12	29.0918850	1038.6142000	.0005	.0008	.0110	
LURE71	7120 7805	20	42	27.3934870	203	44	38.2476610	3067.7538000	0.0000	.0008	.0087	
KIRK78 WETT78	7805 7834	60 49	13 8	2.3165850 41.7637190	24 12	23 52	40.3379730 41.1229850	74.5956000 661.0547000	.0211 .0020	.0239 .0029	.2385	
AUST78	7890	30	18	55.7909130	262	8	4.0203160	257.3139000	.0020	.0029	.0320 .0710	
AREQ79	7907	-16	27	56.6815750	288	30	24.7514310	2492.3439000	.0033	.0038	.0214	
NATA79	7929	-5	55	40.1221480	324	50	7.3717860	39.7370000	.0014	.0014	.0283	
ORRO79	7943	-35	37	29.7629500	148	57	17.2797610	948.9755000	.0008	.0009	.0165	

									Scaled St	nd. Dev	iations	
C+ 4:		τ.		do	Lot	ngitu	ıdo	Height	Lat.	Lon.	Ht.	
Stati			titu		(°)			(m)	(")	(")	(m)	
Name	Num.	(°)	(*)	(")	(3)	<u> </u>	()	(1117)	( )			
April -	Tuna 8	1	RM	[S.126+00	6	378	137.00	298.257				
	7051	39	58	24.5790760	239	3	37.6964510	1059.9053000	.0008	.0016	.0090	
QUIN70 GORF70	7063	39	1	13.3757360	283	10	19.9471620	19.1671000	0.0000	0.0000	.0291	
BEAR70	7082	41	56	.9021160	248	34	45.6792710	1963.0171000	.0011	.0017	.0135	
YARA70	7090	-29	2	47.4202860	115	20	48.2594240	241.3877000	.0014	.0018	.0067 9.0792	
GORF71	7102	39	1	14.0278790	283	10	18.6086360	25.7847000	.4182	.3830 .0017	.0123	
PLAT71	7112	40	10	58.0108550	255	16	26.4848050	1501.6465000	.0011 .0010	.0017	.0147	
GOLD71	7115	35	14	53.9092580	243	12	29.0969140	1038.5335000 3067.7694000	0.0000	.0017	.0081	
LURE71	7120	20	42	27.3938060	203	44 23	38.2484100 40.3452120	74,7935000	.0119	.0122	.1362	
KIRK78	7805	60	13	2.2295400 41.7709720	24 12	52	41.1274880	661.1124000	.0013	.0033	.0178	
WE1178	7834 7801	49 35	8 12	52.3431920	248	21	55.7646270	2144.3319000	.0012	.0019	.0225	
FLAG78	7891 7892	30 40	19	36.6527250	250	25	45.0259120	1590.3606000	.0011	.0017	.0146	
VERN78 AREQ79	7907	-16	27	56.6822150	288	30	24.7503420	2492.3251000	.0013	.0019	.0089	
NATA79	7929	-5	55	40.1270740	324	50	7.3653700	39.6969000	.0016	.0021	.0172	
ORRO79	7943	-35	37	29.7564320	148	57	17.2875730	949.0420000	.0013	.0021	.0146	
			04	D) 4C 10	· Λ	^	6378137	.00 298.257	7			
July - S	Septem	ber	81	RMS.12				•		.0008	.0136	
GORF70	7063	39	1	13.3752320	283	10	19.9466320	19.2364000	,0006 8000.	.0006	.0070	
YARA70	7090	-29	2	47.4212210	115	20	48.2595850	241.3977000 18.1584000	.0009	.0014	.0198	
GORF71	7102	39	1	14.3885090	283 283	10 10	18.9408450 20.3097770	19.1885000	0.0000	0.0000	.0111	
GORF71	7105	3 <del>9</del>	1 53	14.1757730 30.2528800	243	34	38.4059440	1838.9250000	.0005	.0008	.0115	
MOUN71	7110 7112	32 40	10	58.0120240	255	16	26.4820920	1501.5778000	.0005	.0008	.0114	
PLAT71 OWEN71	7114	37	13	57.2209980	241	42	22.3565510	1178.0679000	.0006	.0009	.0155	
LURE71	7120	20	42	27.3935100	203	44	38.2452640	3067.8193000	0.0000	.0007	.0077	
LURE72	7210	20	42	25.9699250	203	44	38.7466730	3067.5164000	.0013	.0012	.0237 .2984	
KIRK78	7805	60	13	2.2825590	24	23	40.4895380	75.2702000	.0168	.0404 .0028	.0323	
WETT78	7834	49	8	41.7708280	12	52	41.1242340	661.0912000 2144.3305000	.0023	.0020	.0153	
FLAG78	7891	35	12	52.3440780	248	21 30	55.7590000 24.7498640	2492.3033000	.0005	.0008	.0069	
AREQ79	7907	-16	27 55	56.6799600 40.1198250	288 324	50 50	7.3666380		.0008	.0009	.0091	
NATA79	7929 7943	-5 -35	37	29.7630420	148	57	17.2862080	949.0432000	.0006	.0008	.0104	
ORRO79	7.743	-33	37	27.7000120	1 10		<b>20</b> 1 <b>2</b> 2 2 2 2 2 2					
Octob	er - De	cem	ber	81 RM	S.913	<b>3-</b> 01	l 63781	137.00 <b>29</b> 8.	257			
OTAY70	7062	32	36	2.6683180	243	9	32.9250640		.0005	.0007	.0089	
YARA70	7090	-29	2	47.4213830	115	20	48.2601350	241.3666000	.0007	.0007	.0047	
GORF71	7102	39	1	14.3920720	283	10	18.9472830		.0005	.0008	.0105	
GORF71	7105	39	1	14.1757390	283	10	20.3095990		0.0000	0.0000	.01 <b>22</b> .0105	
QUIN71	7109	39	58	30.0121850	239	3	19.0931910		,0006 ,0004	.0009	.0068	
MOUN71		32	53	30.2536940	243	34	38.4055880 26.4824000		.0004	.0007	.0081	
PLAT71	7112	40	10	58.0119530	255 203	16 44	38.2455520		.0004	.0007	.0058	
LURE71	7120 7210		42 42	27.3965040 25.9757710	203	44	38.7481490		0.0000		.0067	
LURE72 KIRK78	7210 7805		13	2.2903800	24	23	40.4445790		.0134	.0297	.2033	
GRAS78	7835		45	16.8721540	6	55	16.0126300	1323.1051000	.0226		.3159	
AREQ79	7907			56.6812820	288	30	24.7482290	2492.3166000	.0006		.0080	
MOUN79			41	3.2098900		7	18.9024500		.1201		4.3699	
NATA79	7929	-5	55		324		8.4082450	28.8656000	.1820		3.5606 .0138	
ORRO79	7943	-35	37	29.7585810	148	57	17.2827400	949.0447000	.0008	.0010	.0130	

									Scaled S	tnd. Dev	viations	
Statio	n	L	atiti	ude	Lo	ngit	ude	Height	Lat.	Lon.	Ht.	
Name	Num.	(°)	(')	(")	(°)	( <u>'</u> )	(")	(m)	(")	(")	(m)	
Ianuaru	Mai	rch	၉၁	M S.123	יייי	_	279127 00	209 257				
January							378137.00	298.257				
OTAY70 YARA70	7062 7090	32 -29	36	2.6670560	243	9	32.9136040	988.5771000	.0028	.0086	.1439	
GORF71	7102	39	2 1	47.4196920 14.3914180	115 283	20 10	48.2598480 18.9422360	241.3784000 17.9885000	.0010 .0009	.0006 .0011	.0068 .01 <i>77</i>	
GORF71	7105	39	1	14.1757660	283	10	20.3094280	19.1772000	0.0000	0.0000	.0177	
QUIN71	7109	39	58	30.0128040	239	3	19.0862730	1106.2504000	.0013	.0018	.0220	
MOUN71	7110	32	53	30.2524860	243	34	38.4025100	1838.9459000	.0008	.0010	.0151	
PLAT71	7112	40	10	58.0121250	255	16	26.4810360	1501.5824000	.0006	.0010	.0150	
LURE71	7120	20	42	27.3981190	203	44	38.2459480	3067.8437000	.0010	.0011	.01 <b>7</b> 3	
LURE72	7210	20	42	25.9758160	203	44	38.7442730	3067.5228000	0.0000	.0009	.0117	
KIRK78	7805	60	13	2.2964250	24	23	40.3281900	<i>77.</i> 2882000	.0224	.0522	.4934	
WETT78	7834	49	8	41.7634390	12	52	41.1407590	660.9418000	.0043	.0056	.0496	
MOUN78	7888	31	41	6.3740810	249	7	18.6256820	2331.3272000	.0007	.0009	.0154	
AREQ79	7907	-16	27	56.6832410	288	30	24.7507640	2492.2957000	.0008	.0012	.0142	
MOUN79	7921	31	41	3.2360100	249	7	18.9805770	2353.0999000	.0009	.0011	.0208	
ORRO79	7943	-35	37	29.7646970	148	57	17.2820800	949.0114000	.0010	.0010	.0169	
Ameril T		2	M	C 025 01	62	701	27.00 20	0.057				
April - J				S.835-01				3.257				
YARA70	7090	-29	2	47.4176340	115	20	48.2588500	241.3738000	.0009	.0006	.0118	
GORF71	7101	39	1	16.2029870	283	10	43.0092800	8.5404000	.0264	.0437	.2393	
GORF71	7102	39	1	14.3915570	283	10	18.9445750	17.9988000	.0005	.0006	.0134	
GORF71	7105	39	1	14.1757950	283	10	20.3092430	19.1779000	0.0000	0.0000	.0111	
QUIN71	7109	39 32	58 53	30.0127900	239	3	19.0905660	1106.2624000	.0004	.0006	.0109	
MOUN71 PLAT71	7110 7112	32 40	10	30.2557490	243 255	34	38.4002830	1838.9987000	.0004	.0007	.0112	
LURE72	7210	20	42	58.0120120 25.9760910	203	16 44	26.4814980 38.7451610	1501.6498000	.0004	.0006	.0111	
KOOT78	7833	52	10	42.2324500	5	48	35.2823960	3067.5092000 93.4591000	0.0000 .0059	.0007 .0115	.0084 .1068	
WETT78	7834	49	8	41.7654370	12	52	41.1275490	661.1224000	.0033	.0010	.0169	
GRAS78	7835	43	45	16.8691020	6	55	16.0217030	1323.1229000	.0012	.0092	.0972	
SIMO78	7838	33	34	39.7058700	135	56	13.3353800	99.4217000	.0013	.0013	.0144	
MOUN78	7888	31	41	6.3770380	249	7	18.6281720	2331.3667000	.0008	.0009	.0204	
VERN78	7892	40	19	36.6534930	250	25	45.0217210	1590.2615000	.0007	.0010	.0187	
AREQ79	7907	-16	27	56.6839920	288	30	24.7467960	2492.3222000	.0004	.0008	.0089	
July - Se	ptem		82	M S.797	7-01	6	378137.00	298.257				
YARA70	7090	-29	2	47.4171030	115	20	48.2598170	241.3804000	.0006	.0004	.0074	
GORF71	7102	39	1	14.3897820	283	10	18.9519150	17.8660000	.0023	.0021	.0778	
GORF71	7103	39	1	14.6177450	283	10	18.9461440	17.9296000	.0007	.0012	.0162	
GORF71	7105	39	1	14.1758020	283	10	20.3090560	19.2197000	0.0000	0.0000	.0074	
QUIN71	7109	39	58	30.0126920	239	3	19.0883740	1106.3875000	.0003	.0005	.0072	
MOUN71	7110	32	53	30.2572110	243	34	38.4015740	1839.0264000	.0003	.0005	.0080	
PLAT71 LURE72	7112	40 20	10	58.0143400	255	16	26.4768320	1501.6668000	.0003	.0005	.0089	
KIRK78	7210 7805	20 60	42 13	25.9763480 2.3306600	203	44 23	38.7428100	3067.5823000	0.0000	.0005	.0063	
KOOT78	7833	52	10	42.2424020	<b>24</b> 5	48	40.3863040	78.2979000 93.3447000	.0056	.0109	.0701	
WETT78	7834	49	8	41.7666270	12	52	35.2827090 41.1261620	661.1568000	.0115 .0008	.0204 .0007	.1362	
GRAS78	7835	43	45	16.8816470	6	55	16.0168860	1323.4308000	.0027	.0007	.0088 .0608	
SIMO78	7838	33	34	39.7144270	135	56	13.3704280	99.7821000	.0027	.0044	.2311	
MCDO78	7885	30	40	37.3180790	255	59	2.6215600	1961.3972000	.0004	.0005	.0103	
VERN78	7892	40	19	36.6570570	250	25	45.0212660	1590.2803000	.0005	.0007	.0138	
AREQ79	7907	-16	27	56.6806310	288	30	24.7484530	2492.3501000	.0003	.0006	.0058	

									Scaled St	nd. Dev		
Station	n	I.a	ıtitu	de	Lo	ngiti	ude	Height	Lat.	Lon.	Ht.	
	Num.				(°)		(")	(m)	(")	(")	(m)	
Ivalile	14uii.	· /	· /	( )		`						
October	- Dec	emb	er 8	82 MS.	690-	01	6378137					
MCDO70	7086	30	40	37.3186920	255	59	2.6275920	1961.5450000	.0003	.0005	.0084	
YARA70		-29	2	47.4185750	115	20	48.2620640	241.3982000	.0005	.0004 .0010	.0060 .0242	
GORF71	7102	39	1	14.3895110	283	10	18.9436210	17.9902000 17.9421000	.0008 .0003	.0010	.0071	
GORF71	7103	39	1	14.6199340	283 283	10 10	18.9478750 20.3088690	19.1965000	0.0000	0.0000	.0062	
GORF71	7105	39	1 58	14.1758440 30.0131370	239	3	19.0895800	1106.3570000	.0003	.0004	.0060	
QUIN71 MOUN71	7109 7110	39 32	53	30.2558820	243	34	38.4015920	1839.0323000	.0002	.0004	.0047	
PLAT71	7112	40	10	58.0135470	255	16	26.4819310	1501.5492000	.0002	.0003	.0058	
OWEN71	7114	37	13	57.2236950	241	42	22.3555690	1177.9757000	.0003	.0005	.0091	
LURE72	7210	20	42	25.9762840	203	44	38.7408480	3067.5320000	0.0000	.0005	.0049	
KIRK78	7805	60	13	2.3299500	24	23	40.3388940	78.5693000	.0053	.0094	.0821	
KOO178	7833	52	10	42.2317780	5	48	35.2819070	93.4587000	.0047	.0080 .0008	.0826 .0084	
WETT78	7834	49	8	41.7679670	12	52	41.1294340	661.2040000	.0007	.0008	.0136	
SIMO78	7838	33	34	39.7029310	135	56	13.3306750	99.4950000 1961.3496000	.0007 .0020	.0030	.0619	
MCDO78	7885	30	40	37.3139940	255 288	59 30	2.6207000 24.7504920	2492.3142000	.0020	.0005	.0058	
AREQ79	7907	-16	27	56.6775870	200	30	24./304920	2492.5142000	.0000	.0000		
								***				
January	- Mai	rch 8	83	M S.931	-01	6	378137.00	298.257				
EAST70	7061	-27	8	52.1462150	250	36	59.1450990	115.8103000	.0121	.0207	.4257	
MCDO70	7086	30	40	37.3182160	255	59	2.6269010	1961.4638000	.0005	.0010	.0143	
YARA70	7090	-29	2	47.4159670	115	20	48.2623630	241.3872000	.0010	.0008 0.0000	.0115 .0168	
GORF71	7105	39	1	14.1758730	283	10	20.3086980	19.2188000 1106.3292000	0.0000	.0009	.0129	
QUIN71	7109	39	58	30.0134240	239	3	19.0911170	1838.9589000	.0004	.0008	.0109	
MOUN71	7110	32	53 10	30.2575780 58.0156360	243 255	34 16	38.4006480 26.4837330	1501.6519000	.0004	.0009	.0136	
PLAT71	7112 7114	40 37	13	57.2218350	241	42	22.3554960	1177.9515000	.0005	.0009	.0154	
OWEN71 LURE72	7210	20	42	25.9764630	203	44	38.7410920	3067.5054000	0.0000	.0008	.0080	
KIRK78	7805	60	13	2.2993210	24	23	40.3493420	78.8335000	.0105	.0176	.1487	
KOOT78	7833	52	10	42.2359400	5	48	35.2775530	93.6009000	.0053	.0082	.0902	
WETT78	7834	49	8	41.7720330	12	52	41.1332390	661.1460000	.0013	.0018	.0189	
SIMO78	7838	33	34	39.6996000	135	56	13.3327740	99.4509000	.0009	.0012 .0069	.0136 .1863	
VAND78	7887	34	33	58.4099040	239	29	58.1026270	601.3928000	.0068 .0029	.0069	.0651	
YUMA78	7894	32	56	20.9387400	245	47 30	48.7397950 24.7497010	241.6877000 2492.3005000	.0006	.0009	.0094	
AREQ79	7907	-16	27	56.6780130	288	30	24.7497010	2492.5005000	.0000	.0007	.007.	
April - ]	June 8	33	M	S.900-01	63	781		98.257				
EAST70	7061	-27	8	52.1417770	250	36	59.1447620	115.9666000	.0023	.0029	.0552	
MCDO70	7086	30	40	37.3115710	255	59	2.6229180	1961.2946000	.0005	.0007	.0113	
YARA70	7090	-29	2	47.4155030	115	20	48.2665690	241.3349000	.0008	.0007 .0006	.0109 .0095	
GORF71	7102	39	1	14.3910800	283	10	18.9460040	18.0442000 19.1649000	.0004		.0095	
GORF71	7105	39	1	14.1759030	283 239	10 3	20.3085300 19.0891190	1106.2977000	.0004	.0006	.0094	
QUIN71	7109 7110	39 32	58 53	30.0138060 30.2554590	243	34	38.3984240	1838.9916000	.0003	.0005	.0087	
MOUN71 PLAT71	7110 7112	32 40	10	58.0133060	255	16	26.4798300	1501.5551000	.0006	.0009	.0161	
MAZA71	7122	23	20	34.2619280	253	32	27.3006120	30.8614000	.0004	.0007	.0094	
LURE72	7210	20	42	25.9767180	203	44	38.7398910	3067.4888000	0.0000		.0062	
KIRK78	7805	60	13	2.2218720		23	40.2820650	78.5045000	.0650		.2812	
KOOT78	7833	52	10	42.2233470	5		35.2883520	93.3208000	.0118	.0207	.2018 .0207	
WETT78	7834	49	8	41.7707920	12		41.1193490	661.0951000	.0014 .0022	.0019 .0020	.0207	
SIMO78	7838	33	34	39.7100620	135			99.4500000 75.4124000	.0022	.0020	.0158	
ROYA78	7840	50	52 56	2.5599490 20.9388040	0 245			241.7964000	.0005		.0100	
YUMA78	7894 7907	-16		56.6798610	243 288			2492.2960000	.0003		.0052	
AREQ79	/ 70/	-10	4.1	30.07 70010	200	50	22 172010					

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		_		_	_					tnd. Dev		
Stati			atiti	ude	Lo	ongit		Height	Lat.	Lon.	Ht.	
Name	Num.	(°)	(')	(")	(°)	(')	(")	(m)	(")	(")	(m)	
			~~			_	050405.00	200 255				
July - S	eptem	ber	83	M S.556	5-01	6	378137.00	298.257				
POTS11	1181	52	22	48.9393440	13	3	54.9972290	147.8504000	.0157	.0439	.3372	
OTAY70	7062	32	36	2.6702570	243	9	32.9203440	988.4268000	.0005	.0009	.0115	
MCDO70	7086	30	40	37.31 <b>7</b> 5910	255	59	2.6255830	1961.4502000	.0004	.0008	.0093	
GORF71	7105	39	1	14.1759240	283	10	20.3083400	19.1157000	0.0000	0.0000	.0066	
QUIN71	7109	39	58	30.0125900	239	3	19.0873190	1106.3733000	.0002	.0005	.0036	
MOUN71	7110	32	53	30.2570570	243	34	38.4027730	1839.1544000	.0008	.0011	.0287	
PLAT71	7112	40	10	58.0132310	255	16	26.4837810	1501.3575000	.0005	.0011	.0156	
HUAH71	7121	-16	44	.6694900	208	57	31.9268730	43.5892000	.0003	.0005	.0053	
MAZA71	7122	23	20	34.2601420	253	32	27.2987140	30.9299000	.0003	.0006	.0066	
LURE72	7210	20	42	25.9770060	203	44	38.7397690	3067.5062000	0.0000	.0005	.0037	
MOUN72	7220	32	53	30.2371150	243	34	37.7881450	1838.8185000	.0003	.0005	.0055	
KOOT78	7833	52	10	42.2321670	5	48	35.2864690	93.4462000	.0133	.0465	.3948	
WETT78	7834	49	8	41.7651020	12	52	41.1299510	661.1000000	.0010	.0015	.0162	
SIMO78	7838	33	34	39.7004520	135	56	13.3295900	99.3271000	.0006	.0008	.0105	
GRAZ78	7839	47	4 58	1.6742550	15	29 3	36.0729770	539.4125000	.0007	.0010	.0122	
QUIN78 YUMA78	7886 7894	39 32	56	30.0298330 20.9363350	239 245	47	18.7620080 48.7434160	1109.6232000 241.8301000	.0004 .0013	.0007 .0016	.0093 .0345	
	7907	-16	27	56.6797230	288	30	24.7467490	2492.2866000	.0013	.0005	.0020	
AREQ79 MATE79	7939	40	38	55.7807620	16	42	16.8471180	535.8907000	.0005	.0003	.0020	
IVIA I E/ 9	7939	40	30	33.7607620	10	42	10.0471100	333.0907000	.0005	.0006	.00/3	
Octobe	Do	1	h	83 M S	661	Λ1	6378137	.00 298.25	.7			
POTS11	1181	52	22	48.9312310	13	3	55.0209550	147.9949000	.0045	.0069	.0641	
OTAY70	7062	32	36	2.6691940	243	9	32.9204900	988.4559000	.0004	.0005	.0079	
BEAR70	7082	41	56	.9033020	248	34	45.6764070	1962.9621000	.0005	.0006	.0115	
MCDO70	7086	30	40	37.3172640	255	5 <del>9</del>	2.6237780	1961.4321000	.0003	.0004	.0070	
YARA70	7090	-29	2	47.4181370	115	20	48.2616950	241.3112000	.0005	.0004	.0058	
GORF71	7105	39	1	14.1759610	283	10	20.3081650	19.1326000	0.0000	0.0000	.0056	
QUIN71	7109	39 32	58 53	30.0120480	239	3	19.0883170	1106.3763000	.0003	.0004	.0072	
MOUN71 PLAT71	7110 7112	32 40	10	30.2554220 58.0123570	243 255	34	38.3995410 26.4803120	1838.9422000	.0002	.0004 .0004	.0056 .0069	
HUAH71	7121	-16	44	.6698510	208	16 57	31.9277720	1501.4104000 43.6264000	.0003 .0003	.0004	.0056	
MAZA71	7121	23	20	34.2593520	253	32	27.3001240	30.8898000	.0003	.0004	.0053	
LURE72	7210	20	42	25.9769520	203	44	38.7398930	3067.5261000	0.0002	.0004	.0033	
MOUN72	7210	32	53	30.2364270	243	34	37.7886060	1838.8494000	.0002	.0004	.0064	
KIRK78	7805	60	13	2.2827260	24	23	40.3835970	79.1331000	.0079	.0143	.1299	
HELW78	7831	29	51	32.4003070	31	20	33.6603300	131.2880000	.0075	.0143	.1765	
KOOT78	7833	52	10	42.2395460	5	48	35.2934190	93.2901000	.0110	.0202	1920	
WETT78	7834	49	8	41.7666590	12	52	41.1300430	661.1389000	.0006	.0005	.0065	
SHAN78	7837	31	5	51.1349650	121	11	30.2396310	28.1460000	.0225	.0213	.3823	
SIMO78	7838	33	34	39.7027910	135	56	13.3313590	99.4015000	.0004	.0006	.0056	
GRAZ78	7839	47	4	1.6748220	15	29	36.0772310	539.4050000	.0006	.0004	.0065	
ROYA78	7840	50	52	2.5556620	0	20	10.0272360	75.3453000	.0005	.0005	.0066	
AREQ79	7907	-16	27	56.6797220	288	30	24.7484690	2492.2816000	.0002	.0005	.0034	
MATE79	7939	40	38	55.7819560	16	42	16.8486120	535.9256000	.0006	.0004	.0062	
										.500.		

								S	caled St	nd. Devi	ations	
<b></b>		τ.		٠.	Īor	ıgitı	ıdo	Height	Lat.	Lon.	Ht.	
Statio			titu					(m)	(")	(")	(m)	
Name	Num.	(°) (	(')	(")	(°) (	<u>.,                                    </u>	( )	(1117		<del>`</del>	(/	
January	- Mar	ch 8	24	M S.665	-01	63	78137.00	298.257				
		CII O	77 	48.9319550	13	3	55.0240150	147.8645000	.0044	.0070	.0677	
POTS11	1181 7062	52 32	22 36	2.6688880	243	9	32.9226650	988.3429000	.0014	.0009	.0278	
OTAY70 BEAR70	7082	41	56	.9056580	248	34	45.6759390	1963.0439000	.0015	.0013	.0476	
MCDO70	7086	30	40	37.3175110	255	59	2.6269930	1961.5270000	.0005	.0007	.0105 .0057	
YARA70	7090	-29	2	47.4199050	115	20	48.2644540	241.3767000	.0006	.0004	.0057	
GORF71	7105	39	1	14.1759440	283	10	20.3079690	19.1722000	0.0000	0.0000 .0004	.0061	
QUIN71	7109	39	58	30.0125320	239	3	19.0909380	1106.3503000	.0003	.0004	.0051	
MOUN71	7110	32	53	30.2557190	243	34	38.4017080	1838.9657000	.0004	.0005	.0090	
PLAT71	7112	40	10	58.0125410	255	16	26.4821370	1501.4634000 43.5346000	.0004	.0006	.0076	
HUAH71	7121	-16	44	.6688980	208	57	31.9303870	30.7865000	.0002	.0004	.0044	
MAZA71	7122	23	20	34.2589450	253	32	27.3011920	3067.5088000	0.0000	.0006	.0058	
LURE72	7210	20	42	25.9776960	203	44	38.7413750	896.0064000	.0003	.0004	.0064	
BARS72	<b>726</b> 5	35	19	52.3812640	243	6	31.3637680	725.4559000	.0007	.0014	.0153	
SANT74	7400	-33	8	58.7462730	289	19 23	52.9261660 40.4311190	77.8189000	.0106	.0146	.1340	
KIRK78	7805	60	13	2.2606190	24 5	48	35.2808880	93.2819000	.0184	.0148	.3247	
KOOT78	7833	52	10	42.2401410	12	52	41.1298160	661.1350000	.0007	.0006	.0070	
WETT78	7834	49 ~~	8	41.7652010	135	56	13.3278800	99.4150000	.0005	.0008	.0070	
SIMO78	7838	33	34	39.7013120	155	29	36.0779310	539.3733000	.0007	.0006	.0106	
GRAZ78	7839	47	4	1.6738710 2.5555290	0	20	10.0299310	75.3416000	.0006	.0006	.0070	
ROYA78	7840	50 22	52 55	3.1813490	250	8	8.0709590	111.2946000	.0004	.0006	.0094	
CABO78	7882 7907	-16	27	56.6795590	288	30	24.7484710	2492.3395000	.0007	.0010	.0142	
AREQ79	7907 7939	40	38	55.7816490	16	42	16.8506780	535.8787000	.0007	.0005	.0065	
MATE79	7337	<b>₩</b>	30	33.7010170								
								00.055				
April -	Tune 8	4	M	S.543-01	63	781	37.00 2	98.257			0000	
POTS11	1181	52	22	48.9327730	13	3	55.0176220	147.8401000	.0072	.0079	.0976	
EAST70	7061	-27	-8	52.1442000	250	36	59.1468210	115.8685000	.0062	.0070	.1251	
MCDO70	7086	30	40	37.3172160	255	59	2.6262120	1961.4697000	.0002	.0003	.0072	
YARA70	7090	-29	2	47.4163190	115	20	48.2634420	241.3671000	.0002	.0002	.0028 .0034	
GORF71	7105	39	1	14.1759620	283	10	20.3077920	19.1814000	0.0000	0.0000	.0025	
QUIN71	7109	39	58	30.0124140	239	3	19.0882570	1106.3414000	.0001	.0002 .0002	.0029	
MOUN71	7110	32	53	30.2562350	243	34	38.3995540	1838.9621000	.0001 .0002	.0002	.0029	
PLAT71	7112	40	10	58.0132610	255	16	26.4807100	1501.4232000	.0002	.0003	.0039	
HUAH71	7121	-16	44	.6681990	208	57	31.9257630	43.6065000	.0002	.0003	.0069	
MAZA71	7122	23	20	34.2595250	253	32	27.3013180	30.8246000 3067.4708000	0.0000	.0003	.0022	
LURE72	<b>7210</b>	20	42	25.9780810	203	44	38.7397970	725.4607000	.0002	.0004	.0054	
SANT74	7400	-33	8	58.7497370	289	19	52.9278710	2158.7138000	.0002	.0003	.0036	
CERR74	<b>74</b> 01	-30		20.9166310	289	11	59.8743920	78.5685000	.0398	.0567	.8169	
KIRK78	7805	60			24	23	40.5053040 54.7587510	951.0621000	.0006	.0010	.0125	
BERN78	7810	46	52	38.0156630	7 5	27	35.2806990	93.4280000	.0033	.0037	.0592	
KOOT78	7833	52			12	48 52		661.1035000	.0003	.0004	.0046	
WET178	7834	49			135			99.4372000	.0003	.0005	.0066	
SIMO78	7838	33 47					36.0786600	539.4089000	.0004	.0005	.0070	
GRAZ78	7839 7840							75.3600000	.0003		.0038	
ROYA78	7907				288			2492.2987000	.0002		.0028	
AREQ79 MATE79	7939							535.8314000	.0003		.0037	
KOOT88	8833							88.6193000	.0004	.0007	.0073	
KOO100	0000	-										

									Scaled S	tnd. Dev	riations
Statio	on	L	atit	ude	L	onei	tude	Height	Lat.	Lon.	Ht.
Vame	Num.			(")			(")	. ~			·
vairie	1 VUIII.	· \ /	<u> </u>	()	. ( )	<u> </u>		(m)	(")	(")	(m)
July - S	eptem	ber	84	M S.51	9-01	6	378137.00	298.257			
POTS11	1181	52	22	48.9338420	13	3	55.0219000	148.0231000	.0044	.0057	.0543
EAST70	7061	-27	8	52.1450100	250	36	59.1484250	115.8129000	.0031	.0044	.0644
ACDO70	7086	30	40	37.3142920	255	59	2.6266500	1961.5331000	.0002	.0003	.0053
(ARA70	7090	-29	2	47.4164310	115	20	48.2633860	241.3517000	.0003	.0002	.0031
GORF71	7105	39	1	14.1759620	283	10	20.3076080	19.1737000	0.0000	0.0000	.0039
QUIN71	7109	39	58	30.0125160	239	3	19.0887780	1106.3396000	.0001	.0002	.0029
MOUN71	7110	32	53	30.2558190	243	34	38.3990430	1838.9558000	.0001	.0002	.0030
LAT71	7112	40	10	58.0121850	255	16	26.4803240	1501.4444000	.0002	.0004	.0055
HUAH71	7121	-16	44	.6684640	208	57	31.9241580	43.6025000	.0002	.0003	.0048
AZA71	7122	23	20	34.2607480	253	32	27.3009480	30.8232000	.0002	.0003	.0045
URE72	7210	20	42	25.9787610	203	44	38.7384590	3067.4713000	0.0000	.0003	.0029
CIRK78	7805	60	13	2.2818730	24	23	40.4284720	78.0664000	.0162	.0232	.1678
ERN78	7810	46	52	38.0181440	7	27	54.7643830	951.0240000	.0003	.0004	.0043
COO178	7833	52	10	42.2364610	5	48	35.2907140	93.4091000	.0065	.0110	.0897
VETT78	7834	49	8	41.7677380	12	52	41.1321920	661.1117000	.0003	.0004	.0039
HAN78	7837	31	5	51.1549520	121	11	30.2359770	27.8111000	.0104	.0122	.1624
IMO78	7838	33	34	39.7029000	135	56	13.3305430	99.4139000	.0003	.0004	.0043
RAZ78	7839	47	4	1.6740210	15	29	36.0776930	539.4113000	.0004	.0004	.0047
OYA78	7840	50	52	2.5565530	0	20	10.0310280	75.3727000	.0003	.0004	.0036
REQ79	7907	1/	22								
INEQ/3	/70/	-10	2/	20.00 I 044U	288	.40	24-7504280	7447 7XX7(¥¥)	(887)	{ T T T Z	
	7939	-16 40	27 38	56.6816440 55.7824270	288 16	30 42	24.7504280 16.8521290	2492.2882000 535.8222000	.0002 .0003	.0003 .0003	.0024 .0032
AATĒ79	7939	40	38	55.7824270	16	42	16.8521290	535.8222000	.0003		
	7939	40	38	55.7824270	16	42	16.8521290 6378137.	535.8222000 00 <b>298.25</b>	.0003	.0003	.0032
лат <del>ё</del> 79 October	7939 - Dec	40 eml	38 oer	55.7824270 84 M S 48.9291670	16 .551- 13	42 ·01 3	16.8521290 6378137. 55.0228310	535.8222000 00 298.25 147.9414000	.0003 7 .0066	.0003	.0032
AATĒ79 October 201511 AST70	7939 - Dec	40 eml 52	38 oer 22	55.7824270 84 MS	<sup>16</sup> .551-	42	16.8521290 6378137. 55.0228310 59.1466390	535.8222000 00 298.25 147.9414000 115.8546000	.0003 7 .0066 .0039	.0003 .0106 .0060	.0032 .0738 .0817
AATĒ79 October OTS11 AST70 ICDO70	7939 - Dec 1181 7061	40 eml 52 -27	38 oer 22 8	55.7824270 84 M S 48.9291670 52.1451570	16 .551- 13 250	42 01 3 36	16.8521290 6378137. 55.0228310	535.8222000 00 298.25 147.9414000	.0003 7 .0066 .0039 .0003	.0003 .0106 .0060 .0004	.0032 .0738 .0817 .0055
October October OCTS11 AST70 ACDO70 ARA70 CORF71	7939 7 - Dec 1181 7061 7086 7090 7105	40 eml 52 -27 -30 -29 39	38 Der 22 8 40 2	55.7824270 84 M S 48.9291670 52.1451570 37.3163960	16 .551- 13 250 255	42 -01 3 36 59	16.8521290 6378137. 55.0228310 59.1466390 2.6230480	535.8222000  00 298.25  147.9414000  115.8546000  1961.4027000  241.3533000	.0003 7 .0066 .0039 .0003 .0003	.0003 .0106 .0060 .0004 .0003	.0032 .0738 .0817 .0055 .0033
October OTS11 AST70 ACDO70 ARA70 ORF71 UIN71	7939 - Dec 1181 7061 7086 7090	40 eml 52 -27 -30 -29 39 39	38 Der 22 8 40 2 1 58	55.7824270 84 M S 48.9291670 52.1451570 37.3163960 47.4153260	16 .551- 13 250 255 115	42 -01 3 36 59 20	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000	.0003 7 .0066 .0039 .0003 .0003	.0003 .0106 .0060 .0004 .0003 0.0000	.0032 .0738 .0817 .0055 .0033 .0047
October Ots11 AST70 ACDO70 ARA70 OORF71 UUN71	7939 7 - Dec 1181 7061 7086 7090 7105 7109 7110	40 eml 52 -27 30 -29 39 39	38 Der 22 8 40 2 1 58 53	55.7824270 84 M S 48.9291670 52.1451570 37.3163960 47.4153260 14.1759860	.551- 13 250 255 115 283	42 -01 3 36 59 20 10	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300	535.8222000  00 298.25  147.9414000  115.8546000  1961.4027000  241.3533000	.0003 7 .0066 .0039 .0003 .0003 0.0000 .0002	.0003 .0106 .0060 .0004 .0003 0.0000	.0032 .0738 .0817 .0055 .0033 .0047
October OTS11 AST70 ICDO70 ARA70 IORF71 IUIN71 IOUN71 LAT71	7939 7 - Dec 1181 7061 7086 7090 7105 7109 7110 7112	40 eml 52 -27 -30 -29 39 39 32 40	38 Oer 22 8 40 2 1 58 53 10	55.7824270 84 M S 48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970	.551- 13 250 255 115 283 239	42 01 3 36 59 20 10 3	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630	535.8222000 00 298.25 147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000	.0003 7 .0066 .0039 .0003 .0003	.0003 .0106 .0060 .0004 .0003 0.0000 .0003	.0032 .0738 .0817 .0055 .0033 .0047 .0040
October OTS11 AST70 ICDO70 ARA70 SORF71 PUIN71 IOUN71 LAT71 IUAH71	7939  - Dec 1181 7061 7086 7090 7109 7110 7112 7121	40 52 -27 30 -29 39 39 32 40 -16	38 Oer 22 8 40 2 1 58 53 10 44	55.7824270 84 M S 48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370	.551- 13 250 255 115 283 239 243 255 208	42 01 3 36 59 20 10 3 34 16 57	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740	535.8222000  00 298.25 147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000	.0003 7 .0066 .0039 .0003 .0003 .0000 .0002	.0003 .0106 .0060 .0004 .0003 0.0000	.0032 .0738 .0817 .0055 .0033 .0047
October OTS11 AST70 ICDO70 GRA70 GORF71 UUIN71 IOUN71 LAT71 IUAH71 IAZA71	7939  - Dec 1181 7061 7086 7090 7105 7109 7110 7112 7121 7122	40 52 -27 30 -29 39 39 32 40 -16 23	38 Oer 22 8 40 2 1 58 53 10 44 20	55.7824270 84 M S 48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020	16 .551- 13 250 255 115 283 239 243 255 208 253	42 01 3 36 59 20 10 3 34 16	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360	535.8222000 00 298.25 147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000	.0003 7 .0066 .0039 .0003 .0003 .0000 .00002 .0002 .0013	.0003 .0106 .0060 .0004 .0003 .0000 .0003 .0003	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198
October OTS11 AST70 ICDO70 ICDO70 ICRA70 ICRA71 ICUN71 ICUN71 ICUN71 IUAH71 IUAH71 IUAH71 IUAH71 IUAH71 IUAH71	7939  - Dec 1181 7061 7086 7090 7105 7109 7112 7121 7122 7210	40 52 -27 30 -29 39 39 32 40 -16 23 20	38 Oer 22 8 40 2 1 58 53 10 44 20 42	55.7824270 84 M S 48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820	16 .551- 13 250 255 115 283 239 243 255 208 253 203	42 01 3 36 59 20 10 3 34 16 57 32 44	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000	.0003 7 .0066 .0039 .0003 .0003 .0000 .0002 .0002 .0013 .0002	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0003	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036
October Orsi1 AST70 ICDO70 ARA70 CORF71 PUIN71 IOUN71 LAT71 IUAH71 IUAH71 IUAH71 IURE72 IRK78	7939  7 - Dec 1181 7061 7086 7090 7105 7109 7110 7112 7121 7122 7210 7805	40 52 -27 30 -29 39 39 32 40 -16 23 20 60	38 Oer 22 8 40 2 1 58 53 10 44 20 42 13	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 2.2929890	.551- 13 250 255 115 283 239 243 255 208 253 203 24	42 -01 3 36 59 20 10 3 34 16 57 32 44 23	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000	.0003 7 .0066 .0039 .0003 .0003 .0002 .0002 .0002 .0002	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031
October Otsii AST70 iCDO70 ARA70 ORF7i UIN71 iOUN71 LAT7i IUAH71 iAZA71 URE72 IRK78 ERN78	7939  7 - Dec 1181 7061 7086 7090 7105 7109 7112 7121 7122 7210 7805 7810	40 52 -27 30 -29 39 39 39 39 40 -16 23 20 60 46	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 225.9789820 2.2929890 38.0199900	.551- 13 250 255 115 283 239 243 255 208 253 203 24 7	42 01 3 36 59 20 10 3 34 16 57 32 44 23 27	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 3067.5082000	.0003 7 .0066 .0039 .0003 .0003 .0002 .0002 .0002 .0002 .0002	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0022 .0004 .0003	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773
October Ots11 AST70 ACDO70 ARA70 ORF71 UIN71 IOUN71 LAT71 IUAF71 IAZA71 URE72 IRK78 ERN78 OOT78	7939  - Dec 1181 7061 7086 7090 7105 7109 7110 7112 7121 7122 7210 7805 7810 7833	40 52 -27 30 -29 39 39 32 40 -16 23 20 60 46 52	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 2.2929890 38.0199900 42.2292670	.551- 13 250 255 115 283 239 243 255 208 253 203 24 7	42 01 3 36 59 20 10 3 34 16 57 32 44 23 27 48	6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 3067.5082000 78.0593000	.0003 7 .0066 .0039 .0003 .0003 .0002 .0002 .0002 .0002 .0002 .0002	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004 .0003	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031
October Otsi1 AST70 AST70 ACDO70 ARA70 ORF71 UIN71 IOUN71 LAT71 IUAH71 IAZA71 URE72 IRK78 ERN78 OOT78 /ETT78	7939  7 - Dec 1181 7061 7086 7090 7110 7112 7121 7122 7210 7805 7810 7833 7834	40 emlt 52 -27 30 -29 39 39 32 40 -16 23 20 60 46 52 49	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 2.2929890 38.0199900 42.2292670 41.7690300	16 .551- 13 250 255 283 239 243 255 208 253 203 24 7 5	01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 52	6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 3067.5082000 78.0593000 951.0570000	.0003 7 .0066 .0039 .0003 .0002 .0002 .0002 .0002 .0002 .0002 .0002	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004 .0003 .0004 .0617	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773
ATE79  October OTS11 AST70 ICDO70 ARA70 OORF71 IUIN71 IOUN71 LAT71 IUAH71 IAZA71 URE72 IRK78 ERN78 OOT78 /ETT78 RAS78	7939  - Dec 1181 7061 7086 7090 7105 7109 7110 7112 7121 7122 7210 7805 7810 7833 7834 7835	40 emle 52 -27 30 -29 39 39 32 40 -16 23 20 60 46 52 49 43	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8 45	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 2.2929890 38.0199900 42.2292670 41.7690300 16.8754320	16 .551- 13 250 255 115 283 239 243 255 208 253 203 24 7 5 12 6	01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 52 55	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940 35.2804070 41.1285430 16.0215900	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 30.67.5082000 78.0593000 951.0570000 93.4936000	.0003 7 .0066 .0039 .0003 .0002 .0002 .0013 .0002 .0002 .0002 .0002 .0003	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004 .0003 .0004 .0617 .0007	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773 .0068 .0882
October OTS11 AST70 (CDO70 (ARA70 CORF71 UUN71 HOUN71 LAT71 IUAH71 HAZA71 URE72 LIRK78 ERN78 OOT78 VETT78 ERA578 HAN78	7939  - Dec 1181 7061 7086 7090 7109 7110 7112 7121 7122 7210 7805 7810 7833 7834 7835 7837	40 emle 52 -27 30 -29 39 39 40 -16 23 20 60 45 49 43 31	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8 45 5 5	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 2.2929890 38.0199900 42.2292670 41.7690300 16.8754320 51.1483090	16 .551- 13 250 255 115 283 239 243 255 208 253 203 24 7 5 12 6 121	01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 52 55 11	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940 35.2804070 41.1285430	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 3067.5082000 78.0593000 951.0570000 93.4936000 661.1031000	.0003 7 .0066 .0039 .0003 .0003 .0002 .0002 .0013 .0002 .0002 .0002 .0003	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004 .0003 .0004 .0617 .0007 .0097	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773 .0068 .0882 .0047
October Octobe	7939  7 - Dec 1181 7061 7086 7090 7105 7109 7110 7112 7210 7805 7810 7833 7834 7835 7837 7838	40 eml 52 -27 30 -29 39 39 32 40 -16 22 20 46 52 49 43 31 33	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8 45 5 34	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 2.2922890 38.0199900 42.2292670 41.7690300 16.8754320 51.1483090 39.7027680	16 .551- 13 250 255 115 283 239 243 255 208 253 203 24 7 5 12 6 121 135	42 01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 55 55 11 56	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940 35.2804070 41.1285430 16.0215900	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 3067.5082000 78.0593000 951.0570000 93.4936000 661.1031000 1322.8358000	.0003 7 .0066 .0039 .0003 .0003 .0002 .0002 .0013 .0002 .0002 .0002 .0003 .0004	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004 .0003 .0004 .0617 .0007 .0007 .0005	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773 .0068 .0882 .0047 .0046 .0764
October Orsi1 AST70 ICDO70 ARA70 CORF71 PUIN71 IOUN71 LAT71 IUAH71 IAZA71 URE72 IRK78 ERN78 OOT78 VETT78 RAS78 HAN78 IMO78 IRAZ78	7939  7 - Dec 1181 7061 7080 7105 7109 7110 7112 7121 7805 7810 7833 7834 7835 7837 7838 7839	40 eml 52 -27 39 39 32 40 -16 23 40 45 43 31 33 47	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8 45 5 3 44 45 5 3 46 47 48 48 48 48 48 48 48 48 48 48	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 22.9789820 2.2929890 38.0199900 42.2292670 41.7690300 16.8754320 51.1483090 39.7027680 1.6750560	16 .551- 13 250 255 115 283 239 243 255 203 24 7 5 12 6 121 135 15	42 01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 55 55 55 55 55 57 57 57 57 57	6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940 35.2804070 41.1285430 16.0215900 30.2355890 13.3312570 36.0727590	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 3067.5082000 78.0593000 951.0570000 93.4936000 661.1031000 1322.8358000 27.8506000	.0003 7 .0066 .0039 .0003 .0003 .0002 .0002 .0013 .0002 .0002 .0002 .0002 .0004 .0004 .0004	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004 .0003 .0004 .0007 .0007 .0007	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773 .0068 .0882 .0047
October Otsii AST70 iCDO70 ARA70 ORF7i OUN71 IOUN71 LAT7i IUAH71 IAZA71 URE72 IRK78 ERN78 OOT78 /ETT78 RAS78 HAN78 IMO78 RAZ78 OYA78	7939  7 - Dec 1181 7061 7066 7090 7105 7109 7110 7112 7221 7210 7805 7810 7833 7834 7835 7837 7838 7839 7840	40 eml 52 -27 30 -29 39 32 40 -16 22 20 40 45 49 43 13 34 50	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8 45 53 40 44 55 53 10 44 55 56 56 56 56 56 56 56 56 56 56 56 56	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 225.9789820 2.2929890 38.0199900 42.2292670 41.7690300 16.8754320 51.1483090 39.7027680 1.6750560 2.5577330	16 13 250 255 115 283 239 243 255 208 253 203 24 7 5 12 6 121 135	01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 52 55 51 15 56 29 20	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940 35.2804070 41.1285430 16.0215900 30.2355890 13.3312570 36.0727590 10.0286300	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 3067.5082000 78.0593000 951.0570000 93.4936000 661.1031000 1322.8358000 27.8506000 99.4513000	.0003 7 .0066 .0039 .0003 .0003 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0004 .0004 .0003	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0004 .0003 .0004 .0007 .0007 .0007 .0005 .0005	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773 .0068 .0882 .0047 .0046 .0764
October Otsi1 AST70 ICDO70 ARA70 ION71 IOUN71 IAT71 IUAH71 IAZA71 UURE72 IRK78 ERN78 OOT78 /ETT78 RAS78 HAN78 IMO78 RAZ78 OYA78 UIN78	7939  - Dec 1181 7061 7086 7090 7105 7109 7110 7112 7121 7122 7210 7805 7810 7833 7834 7835 7837 7838 7839 7840 7886	40 eml 52 -27 30 -29 39 32 40 -16 23 20 60 46 52 49 43 31 33 47 50 39	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8 45 5 34 45 5 5 46 47 47 48 48 49 49 49 49 49 49 49 49 49 49 49 49 49	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 2.2929890 38.0199900 42.2292670 41.7690300 16.8754320 51.1483090 39.7027680 1.6750560 2.5577330 30.0551300	16 .551- 13 250 255 115 283 239 243 255 208 253 203 24 7 5 12 6 121 135 15 0 239	01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 52 55 11 56 59 20 3 3 4 59 20 3 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940 35.2804070 41.1285430 16.0215900 30.2355890 13.3312570 36.0727590 10.0286300 18.6344670	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 30.8212000 78.0593000 951.0570000 93.4936000 661.1031000 1322.8358000 27.8506000 99.4513000 539.3550000	.0003 7 .0066 .0039 .0003 .0002 .0002 .0002 .0002 .0002 .0002 .0005 .0062 .0004 .0004 .0003 .0003 .0003	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0004 .0017 .0007 .0007 .0005 .0005 .0004	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773 .0068 .0882 .0047 .0046 .0764 .0038 .0038
October Otsi1 AST70 ACDO70 ARA70 CORF1 PUIN71 AOUN71 LAT71 IUAH71 AZA71 UURE72 IIRK78 ERN78 COT78 VETT78 IRA578 HAN78 IMO78 IRA278 OYA78 PUIN78 RA278	7939  - Dec 1181 7061 7086 7090 7105 7109 7110 7112 7121 7122 7210 7805 7810 7833 7834 7835 7837 7838 7839 7840 7886 7907	40 eml 52 -27 30 -29 39 32 40 -16 23 20 60 45 43 31 33 47 50 39 -16	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8 45 5 3 4 5 5 3 4 4 5 5 5 5 6 5 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 8 7 8 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 8 7 8 7 8 8 7 8 8 7 8 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 8 7 8 7 8 7 8 7 8 7 8 7 8 7 8 8 7 8 8 7 7 8 7 8 7 8 7 8 7 7 8 7 7 8 7 8 7 8 7 8 7 7 8 8 7 8 7 8 7 8 8 7 8 7 8 8 7 8 7 8 8 7 8 7 8 8 7 8	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 22.929890 38.0199900 42.2292670 41.7690300 16.8754320 51.1483090 39.7027680 1.6750560 2.5577330 30.0551300 56.6801920	16 .551- 13 250 255 115 283 239 243 255 208 253 204 7 5 12 6 121 135 15 0 239 288	01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 52 55 11 56 29 3 3 3 4 3 3 3 3 4 3 3 3 3 3 3 3 3 3 3 3 3 3	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940 35.2804070 41.1285430 16.0215900 30.2355890 13.3312570 36.0727590 10.0286300 18.6344670 24.7501980	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 3067.5082000 78.0593000 93.4936000 661.1031000 1322.8358000 27.8506000 99.4513000 539.3550000 75.3887000 1109.6495000 2492.3206000	.0003 7 .0066 .0039 .0003 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0006 .0005 .0062 .0004 .0004 .0003 .0003	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004 .0007 .0007 .0007 .0005 .0005 .0004 .0005	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773 .0068 .0882 .0047 .0046 .0764 .0038 .0303 .0040
October Otsi1 AST70 ICDO70 ARA70 ORF71 UIN71 IOUN71 LAT71 IUAF71 IAZA71 UURE72 IRK78 ERN78 OOT78 /ETT78 RAS78 HAN78 iMO78 RAZ78 OYA78 UIN78	7939  - Dec 1181 7061 7086 7090 7105 7109 7110 7112 7121 7122 7210 7805 7810 7833 7834 7835 7837 7838 7839 7840 7886	40 eml 52 -27 30 -29 39 32 40 -16 23 20 60 46 52 49 43 31 33 47 50 39	38 Der 22 8 40 2 1 58 53 10 44 20 42 13 52 10 8 45 5 34 45 5 5 46 47 47 48 48 49 49 49 49 49 49 49 49 49 49 49 49 49	55.7824270  84 M S  48.9291670 52.1451570 37.3163960 47.4153260 14.1759860 30.0120710 30.2561590 58.0078970 .6680370 34.2601020 25.9789820 2.2929890 38.0199900 42.2292670 41.7690300 16.8754320 51.1483090 39.7027680 1.6750560 2.5577330 30.0551300	16 .551- 13 250 255 115 283 239 243 255 208 253 203 24 7 5 12 6 121 135 15 0 239	01 3 36 59 20 10 3 34 16 57 32 44 23 27 48 52 55 11 56 59 20 3 3 4 59 20 3 3 4 5 5 5 5 5 5 5 5 5 5 5 5 5	16.8521290 6378137. 55.0228310 59.1466390 2.6230480 48.2625750 20.3074300 19.0882630 38.3984740 26.4757360 31.9235430 27.3003510 38.7386580 40.4358430 54.7618940 35.2804070 41.1285430 16.0215900 30.2355890 13.3312570 36.0727590 10.0286300 18.6344670	535.8222000  00 298.25  147.9414000 115.8546000 1961.4027000 241.3533000 19.1625000 1106.3766000 1838.9850000 1501.5239000 43.6235000 30.8212000 30.67.5082000 951.0570000 93.4936000 661.1031000 1322.8358000 27.8506000 99.4513000 539.3550000 75.3887000 1109.6495000	.0003 7 .0066 .0039 .0003 .0002 .0002 .0002 .0013 .0002 .0002 .0003 .0005 .0062 .0004 .0004 .0031 .0003 .0003 .0003	.0003 .0106 .0060 .0004 .0003 .0003 .0003 .0002 .0004 .0007 .0007 .0007 .0005 .0004 .0005	.0032 .0738 .0817 .0055 .0033 .0047 .0040 .0036 .0198 .0043 .0031 .0032 .3773 .0068 .0882 .0047 .0046 .0764 .0038 .0303 .0040 .0074

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Statio	n	La	titu	de	Lo	ngitı	ıde	Height	Lat.	Lon.	Ht.	
Name	Num.	(°)	(')	(")	(°)	( <u>′</u> )	(")	(m)	(")	(")	(m)	
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January	- Mar	ch 8	5	M S.633			78137.00		0150	.0351	.3752	
POTS11	1181	52	22	48.9665450	13	3	55.0075530	148.1179000	.0150 .0004	.0004	.0082	
MCDO70	7086	30	40	37.3165840	255	59	2.6223130	1961.4674000 241.3608000	.0004	.0003	.0033	
YARA70	7090	-29	2	47.4139690	115 283	20 10	48.2640360 20.3072580	19.1645000	0.0000	0.0000	.0047	
GORF71	7105 7109	39 39	1 58	14.1760140 30.0118420	239	3	19.0874020	1106.3511000	.0003	.0003	.0049	
QUIN71 MOUN71	7110	32	53	30.2557550	243	34	38.3981270	1838.9617000	.0003	.0003	.0042	
HUAH71	7121	-16	44	.6706670	208	57	31.9256610	43.5744000	.0004	.0005	.0061	
MAZA71	7122	23	20	34.2594310	253	32	27.3003520	30.8226000	.0002	.0003	.0039	
LURE72	7210	20	42	25.9791110	203	44	38.7377940	3067.5309000	0.0000	.0005	.0067 .0341	
WETT75	7596	49	8	39.0555080	12	52	43.2367870	657.3310000	.0028 .0011	.0056 .0011	.0153	
WETT78	7834	49	8	41.7675560	12	52	41.1317150	661.1424000 1322.8301000	.0001	.0005	.0073	
GRAS78	7835	43	45	16.8763480	125	55 56	16.0240920 13.3332290	99.4104000	.0004	.0007	.0055	
SIMO78	7838	33	34 4	39.7033080 1.6753420	135 15	29	36.0724980	539.4801000	.0007	.0011	.0187	
GRAZ78 ROYA78	7839 7840	<b>47</b> 50	52	2.5585750	0	20	10.0284130	75.3885000	.0005	.0004	.0047	
AREQ79	7907	-16	27	56.6791500	288	30	24.7495590	2492.3428000	.0003	.0006	.0070	
MATE79	7939	40	38	55.7849580	16	42	16.8520760	535.8126000	.0006	.0005	.0073	
KOOT88	8833	52	10	41.4467900	5	48	36.5902470	88.6026000	.0008	.0012	.0118	
		_		0.544.01	(0)	701	27.00 20	0 257				
April - ]	June 8	5	M	S.566-01	63			8.257	0000	04770	25.00	
POTS11	1181	52	22	48.9246460	13	3	55.0366060	147.7436000	.0099	.0178 .0004	.2578 .0078	
MCDO70	7086	30	40	37.3142010	255	59	2.6232320	1961.4853000	.0003	.0004	.0025	
YARA70	7090	-29	2	47.4144540	115	20	48.2659350 20.3070680	241.3839000 19.1569000	0.0002	0.0000	.0034	
GORF71	7105	39	1	14.1760380	283 239	10 3	19.0865520	1106.3427000	.0001	.0002	.0030	
QUIN71	7109	39 32	58 53	30.0123530 30.2565450	243	34	38.3974280	1838.9882000	.0001	.0002	.0027	
MOUN71 HUAH71	7110 7121	-16	44	.6676890	208	57	31.9245080	43.5896000	.0005	.0006	.0157	
MAZA71	7122	23	20	34.2593460	253	32	27.3006310	30.8347000	.0001	.0002	.0030	
GORF71	7125	39	1	12.9664870	283	10	21.1960350	18.5279000	.0002	.0003	.0051	
LURE72	7210	20	42	25.9793430	203	44	38.7352080	3067.5238000	0.0000	.0003	.0032	
WETT78	7834	49	8	41.7665500	12	52	41.1296340	661.1666000	.0004	.0006 .0003	.0071 .0052	
GRAS78	7835	43	45	16.8750050	6	55	16.0236290	1322.8432000	.0003	.0004	.0032	
SIMO78	7838	33	34	39.7033200	135	56	13.3291540 36.0759840	99.4472000 539.4486000	.0004	.0005	.0085	
GRAZ78	7839	47 50	<b>4</b> 52	1.6744130 2.5562450	15 0	29 20	10.0314610	75,3933000	.0003	.0004	.0047	
ROYA78	7840 7843	-35	38	10.5223780	148	56	21.5134760	1349.9182000	.0002	.0003	.0036	
ORRO78 AREQ79	7907	-16	27	56.6792940	288	30	24.7501230	2492.3032000	.0002	.0003	.0029	
MATE79	7939	40	38	55.7820650	16	42	16.8503160	535.8457000	.0003	.0003	.0038	
WHITE,	,,,,,											
_		_					AE010E 00	200 257				
July - S	eptem	ber	85	M S.72	8-01	6	5378137.00					
POTS11	1181	52	22	48.9330640	13	3	55.0212390	147.8415000	.0086	.0138	.1122	
MCDO70	7086	30	40	37.3147480	255	59	2.6225650	1961.4902000	.0002	.0003 .0003	.0047 .0033	
YARA70	7090	-29	2	47.4142860	115	20	48.2654650	241.3680000 19.1808000	.0003		.0033	
GORF71	7105	39	1	14.1760320 30.0132380	283 239	10 3	20.3068750 19.0859140	1106.3465000	.0002		.0036	
QUIN71 MOUN71	7109 7110	39 32	58 53	30.0132380	243	34	38.3960490	1838.9955000	.0002		.0040	
HUAH71	7121	-16	44		208	57	31.9194370	43.5827000	.0016	.0014	.0238	
MAZA71	7122	23	20		253	32	27.3002450	30.8531000	.0002		.0045	
GORF71	7125	39	1	12.9658160	283	10	21.1958590	18.5442000	.0005		.0123	
LURE72	7210	20	42	25.9796750	203		38.7364970	3067.4987000	0.0000 .0004		.0035 .0067	
MONT75	7590	45	55		9		3.9356440	1648.3807000 950.9841000	.0004		.0101	
BERN78	7810	46	52		7 12		54.7755270 41.1332760	661.1468000	.0004		.0043	
WETT78	7834 7835	49 43	8 45		6			1322.9135000	.0003		.0040	
GRAS78 SIMO78	7835 7838	33	34		135			99.4890000	.0003	.0004	.0040	
GRAZ78	7839	47	4					539,3993000	.0004	.0005	.0066	
ROYA78	7840	50				20		75.4033000	.0003		.0042	
ORRO78	7843	-35		10.5219070	148			1349.8697000	.0003		.0051	
AREQ79	7907	-16			288			2492.3144000	.0002 .0004		.0031 .0036	
MATE79	7939	40	38	55.7816960	16	42	16.8531890	535.8504000	.0004	.000	.0000	

						,			Scaled S	tnd. Dev	iations
Station	n	La	atitı	ıde	Lo	ngit	ude	Height	Lat.	Lon.	Ht.
	Num.			(")	(°)		(")	(m)	(")	(")	(m)
		· · ·	<del>``</del>		`	<u>`</u>	· · · · · · · · · · · · · · · · · · ·	()	. ,		(224)
	_				<b></b>						
October -	- Dec	emt	oer	85 RM	S. <b>78</b> 0	)-01	<b>6378</b> 13	37.00 <b>2</b> 98.2	.57		
POTS11	1181	52	22	48.9321300	13	3	55.0257290	147.8831000	.0078	.0144	.11 <b>71</b>
MCDO70	7086	30	40	37.3146010	255	59	2.6248010	1961.4573000	.0002	.0004	.0040
ARA70	7090	-29	2	47.4142510	115	20	48.2660300	241.3520000	.0004	.0004	.0041
ORF71	7105	39	1	14.1760540	283	10	20.3066980	19.1647000	0.0000	0.0000	.0060
UIN71	7109	39	58	30.0128470	239	3	19.0871570	1106.3593000	.0002	.0004	.0044
10UN71 IUAH71	7110 7121	32	53	30.2571470	243 208	34 57	38.3973600 31.9224040	1838.9845000	.0002	.0004	.0045
IOAH/I IAZA71	7121	-16 23	44 20	.6651520 34.2596780	253	32	27.3005630	43.5680000 30.8576000	.0005 .0002	.0006 .0004	.0092 .0043
URE72	7210	20	42	25.9799730	203	32 44	38.7359820	3067.5045000	0.0002	.0004	.0043
UNT75	75 <b>4</b> 5	39	8	7.7747910	8	58	22.7409660	229.9782000	.0005	.0004	.0061
ONT75	7590	45	55	39.2525810	9	1	3.9351250	1648.4752000	.0004	.0006	.0061
ERN78	7810	46	52	38.0111160	7	27	54.7749460	951.0889000	.0005	.0007	.0076
/ETT78	7834	49	8	41.7691200	12	52	41.1316260	661.1185000	.0005	.0006	.0058
RAS78	7835	43	45	16.8766260	6	55	16.0258910	1322.9143000	.0004	.0005	.0051
IMO78	7838	33	34	39.7018080	135	56	13.3307810	99.4765000	.0003	.0005	.0038
RAZ78	7839	47	4	1.6720700	15	29	36.0831360	539.7217000	.0165	.0099	.4568
OYA78	7840	50	52	2.5584670	0	20	10.0314000	75.4057000	.0004	.0005	.0046
RRO78	7843	-35	38	10.5238670	148	56	21.5163020	1349.9882000	.0004	.0005	.0246
REQ79	7907	-16	27	56.6788410	288	30	24.7521630	2492.3581000	.0004	.0005	.0063
1ATE79	7939	<b>4</b> 0	38	55.7836120	16	42	16.8527100	535.8239000	.0004	.0004	.0039
Tames aure	Mar	l. (	07	DMC E0	0 01	4	(270127 0	0 200 257			
anuary				RMS.58			6378137.0				
OTS11	1181	52	22	48.9285970	13	3	55.0204990	147.8162000	.0056	.0090	.0914
ICDO70	7086	30	40	37.3145050	255	59	2.6233860	1961.4775000	.0002	.0003	.0032
ARA70	7090	-29	2	47.4137480	115	20	48.2640730	241.3433000	.0003	.0003	.0031
ORF71	7105	39	1	14.1760780	283	10	20.3065420	19.1416000	0.0000	0.0000	.0055
UIN71 10UN71	7109 7110	39 32	58 53	30.0118830 30.25 <b>73</b> 610	239 243	3 34	19.0869220 38.3964830	1106.34 <b>7</b> 9000 1838.9 <b>72</b> 2000	.0002 .0002	.0004 .0003	.0042 .0034
IUAH71	7121	-16	44	.6677880	208	57	31.9179430	43.6682000	.0002	.0003	.0060
AZA71	7122	23	20	34.2597760	253	32	27.2993470	30.8655000	.0003	.0003	.0030
URE72	7210	20	42	25.9805390	203	44	38.7345950	3067.4803000	0.0002	.0004	.0034
AATE75	7541	40	38	54.6942550	16	42	15.4159240	528.3682000	.0004	.0004	.0048
ERN78	7810	46	52	38.0103700	7	27	54.7697190	951.0454000	.0006	.0008	.0087
VETT78	7834	49	8	41.7702140	12	52	41.1288900	661.0828000	.0004	.0005	.0051
SRAS78	7835	43	45	16.8796550	6	55	16.0234050	1322.8930000	.0006	.0010	.0114
IMO78	7838	33	34	39.7029840	135	56	13.3305610	99.4590000	.0003	.0004	.0032
RAZ78	7839	47	4	1.6765960	15	29	36.0783200	539.4040000	.0004	.0005	.0062
OYA78	7840	50	52	2.5585220	0	20	10.0295880	75.3903000	.0003	.0004	.0038
DRRO78	7843	-35	38	10.5199440	148	56	21.5108680	1349.9735000	.0003	.0004	.0152
AREQ79	7907	-16	27	56.6814230	288	30	24.7477520	2492.3117000	.0004	.0005	.0060
ATE79	7939	40	38	55.7848650	16	42	16.8505410	535.8044000	.0004	.0004	.0041
	une 8	6	RN	1S.847-01	63	<b>378</b> :	137.00	298.257			
April - Jı	une 80								.0112	.0166	.2084
April - Ju		52	RN 22 40	1S.847-01 48.9360490 37.3150710	63 13 255	378: 3 59	55.0167740	147.5723000	.0112 .0003	.0166 .0005	.2084 .0074
April - Ju OTS11 ICDO70	1181		22	48.9360490 37.3150710 47.4134390	13	3			.0003	.0005	.0074
April - Ju otsu 1cdozo 1cdoz 1cdo	1181 7086 7090 7105	52 30 -29 39	22 40 2 1	48.9360490 37.3150710	13 255	3 59	55.0167740 2.6232900	147.5723000 1961.4601000			
April - Ju ots11 1cdo70 ARA70 1corf71 1guin71	1181 7086 7090 7105 7109	52 30 -29 39 39	22 40 2 1 58	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050	13 255 115 283 239	3 59 20 10 3	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240	147.5723000 1961.4601000 241.3539000	.0003 .0004 0.0000 .0003	.0005 .0003 0.0000 .0004	.0074 .0043 .0052 .0049
April - Ju OTS11 ICDO70 ARA70 SORF71 SUIN71 IOUN71	1181 7086 7090 7105 7109 7110	52 30 -29 39 39 32	22 40 2 1 58 53	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360	13 255 115 283 239 243	3 59 20 10 3 34	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000	.0003 .0004 0.0000 .0003 .0003	.0005 .0003 0.0000 .0004 .0004	.0074 .0043 .0052 .0049 .0044
April - Ju OTS11 ICDO70 ARA70 ORF71 JUIN71 IOUN71 IUAH71	1181 7086 7090 7105 7109 7110 7121	52 30 -29 39 39 32 -16	22 40 2 1 58 53 44	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670	13 255 115 283 239 243 208	3 59 20 10 3 34 57	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000	.0003 .0004 0.0000 .0003 .0003	.0005 .0003 0.0000 .0004 .0004 .0007	.0074 .0043 .0052 .0049 .0044 .0104
April - Ju OTS11 ICDO70 ARA70 OORF71 PUIN71 IOUN71 IUAH71 IAZA71	1181 7086 7090 7105 7109 7110 7121 7122	52 30 -29 39 39 32 -16 23	22 40 2 1 58 53 44 20	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580	13 255 115 283 239 243 208 253	3 59 20 10 3 34 57 32	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000	.0003 .0004 0.0000 .0003 .0003 .0006	.0005 .0003 0.0000 .0004 .0004 .0007 .0004	.0074 .0043 .0052 .0049 .0044 .0104
April - Ju OTS11 ICDO70 ARA70 IOR71 PUIN71 IOUN71 IUAH71 IAZA71 URE72	1181 7086 7090 7105 7109 7110 7121 7122 7210	52 30 -29 39 39 32 -16 23 20	22 40 2 1 58 53 44 20 42	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980	13 255 115 283 239 243 208 253 203	3 59 20 10 3 34 57 32 44	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000	.0003 .0004 0.0000 .0003 .0003 .0006 .0003	.0005 .0003 0.0000 .0004 .0004 .0007 .0004	.0074 .0043 .0052 .0049 .0044 .0104 .0050
April - Ju OTS11 ICDO70 ARA70 IORF71 PUIN71 IOUN71 IUAH71 IAZA71 URE72 OUM75	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517	52 30 -29 39 39 32 -16 23 20 35	22 40 2 1 58 53 44 20 42 24	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860	13 255 115 283 239 243 208 253 203 24	3 59 20 10 3 34 57 32 44 41	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000	.0003 .0004 0.0000 .0003 .0003 .0006 .0003 0.0000	.0005 .0003 0.0000 .0004 .0004 .0007 .0004 .0006	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065
April - Ju OTS11 ICDO70 ARA70 IORF71 PUIN71 IUAH71 IUAH71 URE72 OUM75 ARI75	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520	52 30 -29 39 39 32 -16 23 20 35 39	22 40 2 1 58 53 44 20 42 24 44	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930	13 255 115 283 239 243 208 253 203 24 20	3 59 20 10 3 34 57 32 44 41 39	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000	.0003 .0004 0.0000 .0003 .0003 .0006 .0003 0.0000 .0007	.0005 .0003 0.0000 .0004 .0004 .0007 .0004 .0006	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065 .0128
April - Ju OTS11 ICDO70 ARA70 ORF71 OUN71 IUAH71 IUAE72 OUM75 ARI75 ASO75	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550	52 30 -29 39 39 32 -16 23 20 35 39 45	22 40 2 1 58 53 44 20 42 24 44 38	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930 34.6311910	13 255 115 283 239 243 208 253 203 24 20 13	3 59 20 10 3 34 57 32 44 41 39 52	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000	.0003 .0004 0.0000 .0003 .0003 .0006 .0003 0.0000 .0007 .0006	.0005 .0003 0.0000 .0004 .0004 .0007 .0004 .0006 .0006	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065 .0128 .0067
April - Ju OTS11 (CDO70 (ARA70 (CORF71 (UIN71 (OUN71 (IUAH71 (IUAH71 (IUAH71 (IUAH75 (ARI75 (ARI75 (ASO75 (ERN78	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550 7810	52 30 -29 39 32 -16 23 20 35 39 45 46	22 40 2 1 58 53 44 20 42 24 44 38 52	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.27223860 3.2968930 34.6311910 38.0129360	13 255 115 283 239 243 208 253 203 24 20 13 7	3 59 20 10 3 34 57 32 44 41 39 52 27	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300 54.7723290	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000 951.0961000	.0003 .0004 0.0000 .0003 .0003 .0003 0.0000 .0007 .0006 .0006	.0005 .0003 0.0000 .0004 .0004 .0007 .0004 .0006 .0006 .0006	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065 .0128 .0067 .0081
April - Ju OTS11 (CDO70 (ARA70 (ARA70 (ARA71) (UIN71 (UUN71 (UAH71 (UAH71 (UAE72 (OUM75 (ARI75 (ASO75 ERN78 (VETT78	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550 7810 7834	52 30 -29 39 32 -16 23 20 35 39 45 46 49	22 40 2 1 58 53 44 20 42 24 44 38 52 8	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930 34.6311910 38.0129360 41.7702800	13 255 115 283 239 243 208 253 203 24 20 13 7	3 59 20 10 3 34 57 32 44 41 39 52 27 52	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300 54.7723290 41.1287020	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000 951.0961000 661.1313000	.0003 .0004 0.0000 .0003 .0003 .0003 0.0000 .0007 .0006 .0006	.0005 .0003 0.0000 .0004 .0004 .0007 .0004 .0006 .0006 .0006 .0008	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065 .0128 .0067 .0081 .0154
April - Ju OTS11 ICDO70 (ARA70 (ARA70 OUN71 IUUN71 IUUN71 IUAH71 IUAH71 IURE72 IOUM75 (ARI75 IASO75 IERN78 VETT78 GRAS78	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550 7810 7834 7835	52 30 -29 39 32 -16 23 20 35 39 45 46 49 43	22 40 2 1 58 53 44 20 42 24 44 38 52 8 45	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930 34.6311910 38.0129360 41.7702800 16.8815960	13 255 115 283 239 243 208 253 203 24 20 13 7 12 6	3 59 20 10 3 34 57 32 44 41 39 52 27 52 55	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300 54.7723290 41.1287020 16.0188500	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000 951.0961000 661.1313000 1322.9256000	.0003 .0004 0.0000 .0003 .0006 .0003 0.0000 .0007 .0006 .0006 .0011 .0006	.0005 .0003 0.0000 .0004 .0007 .0004 .0006 .0006 .0006 .0008	.0074 .0043 .0052 .0049 .0044 .0050 .0065 .0128 .0067 .0081 .0154 .0073
April - Ju OTS11 MCDO70 (ARA70 ORF71 OUN71 MOUN71 MAZA71 URE72 OUM75 (ARI75 SASO75 SERN78 VETT78 GRAS78 IMO78	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550 7810 7834 7835 7838	52 30 -29 39 39 32 -16 23 20 35 39 45 46 49 43 33	22 40 2 1 58 53 44 20 42 24 44 38 52 8 45 34	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930 34.63111910 38.0129360 41.7702800 16.8815960 39.7023200	13 255 115 283 239 243 208 253 203 24 20 13 7 12 6 135	3 59 20 10 3 34 57 32 44 41 39 52 27 52 55 56	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300 54.7723290 41.1287020 16.0188500 13.3329390	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000 951.0961000 661.1313000 1322.9256000 99.4759000	.0003 .0004 0.0000 .0003 .0003 .0000 .0007 .0006 .0006 .0011 .0006	.0005 .0003 0.0000 .0004 .0007 .0004 .0006 .0008 .0006 .0008 .0016 .0008	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065 .0128 .0067 .0081 .0154 .0073 .0205
April - Ju OTS11 MCDO70 'ARA70 GORF1 MOUN71 MOUN71 MAZA71 URE72 OUM75 ARI75 BASO75 BERN78 WETT78 GRAS78 IMO78 GRAS78	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550 7810 7834 7835 7838 7839	52 30 -29 39 39 32 -16 23 20 35 39 45 46 49 43 33 47	22 40 2 1 58 53 44 20 42 24 44 38 52 8 45 34 4	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930 34.63111910 38.0129360 41.7702800 16.8815960 39.7023200 1.6773150	13 255 115 283 239 243 208 253 203 24 20 13 7 12 6 135 15	3 59 20 10 3 34 57 32 44 41 39 52 27 52 55 56 29	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300 54.7723290 41.1287020 16.0188500 13.3329390 36.0765640	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1383.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000 951.0961000 661.1313000 1322.9256000 99.4759000 539.3844000	.0003 .0004 0.0000 .0003 .0003 .0000 .0007 .0006 .0001 .0006 .0011 .0004	.0005 .0003 0.0000 .0004 .0007 .0004 .0006 .0008 .0006 .0008 .0016 .0008 .0015 .0007	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065 .0128 .0067 .0081 .0154 .0073 .0205 .0059
April - Ju OTS11 MCDO70 'ARA70 GORF11 MOUN71 MUAH71 MAZA71 URE72 GOUM75 CARI75 EERN78 WETT78 GRAS78 IMO78 GRAZ78 GOYA78	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550 7810 7834 7835 7838 7839 7840	52 30 -29 39 32 -16 23 20 35 39 45 46 49 43 33 47 50	22 40 2 1 58 53 44 20 42 24 44 38 52 8 45 34 45 20	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930 34.6311910 38.0129360 41.7702800 16.8815960 39.7023200 1.6773150 2.5600140	13 255 115 283 239 243 208 253 203 24 20 13 7 12 6 135 15 0	3 59 20 10 3 34 57 32 44 41 39 52 27 52 55 56 29 20	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300 54.7723290 41.1287020 16.0188500 13.3329390 36.0765640 10.0298770	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000 951.0961000 661.1313000 1322.9256000 99.4759000 539.3844000 75.3988000	.0003 .0004 0.0000 .0003 .0003 .0003 0.0000 .0007 .0006 .0001 .0006 .0010 .0004	.0005 .0003 0.0000 .0004 .0004 .0006 .0006 .0006 .0006 .0006 .0006 .0008 .0016 .0007 .0007	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065 .0128 .0067 .0081 .0154 .0073 .0205 .0059
April - Ju OTS11 MCDO70 ARA70 GORF71 PUIN71 MOUN71 MAZA71 URE72 GOUM75 ARI75 ASO75 ERN78 WETT78 ERAS78 IMO78 ERAZ78 OYA78 DRRO78	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550 7810 7834 7835 7838 7839 7840 7843	52 30 -29 39 39 32 -16 23 20 35 39 45 49 43 33 47 50 -35	22 40 2 1 58 53 44 20 42 24 44 38 52 8 45 34 45 34 45 38	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930 34.6311910 38.0129360 41.7702800 16.8815960 39.7023200 1.6773150 2.5600140 10.5230110	13 255 115 283 239 243 208 253 203 24 20 13 7 12 6 6 135 15 0 148	3 59 20 10 3 34 57 32 44 41 39 52 27 55 56 29 20 56	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300 54.7723290 41.1287020 16.0188500 13.3329390 36.0765640 10.0298770 21.5126610	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000 951.0961000 661.1313000 1322.9256000 99.4759000 539.3844000 75.3988000 1349.9616000	.0003 .0004 0.0000 .0003 .0003 .0003 0.0000 .0007 .0006 .0011 .0006 .0010 .0004	.0005 .0003 0.0000 .0004 .0004 .0006 .0006 .0006 .0006 .0006 .0008 .0015 .0007 .0007	.0074 .0043 .0052 .0049 .0044 .0104 .0050 .0065 .0128 .0067 .0081 .0154 .0073 .0205 .0059 .0055
April - Jupotsi	1181 7086 7090 7105 7109 7110 7121 7122 7210 7517 7520 7550 7810 7834 7835 7838 7839 7840	52 30 -29 39 32 -16 23 20 35 39 45 46 49 43 33 47 50	22 40 2 1 58 53 44 20 42 24 44 38 52 8 45 34 45 20	48.9360490 37.3150710 47.4134390 14.1761070 30.0117050 30.2565360 .6664670 34.2596580 25.9804980 15.2723860 3.2968930 34.6311910 38.0129360 41.7702800 16.8815960 39.7023200 1.6773150 2.5600140	13 255 115 283 239 243 208 253 203 24 20 13 7 12 6 135 15 0	3 59 20 10 3 34 57 32 44 41 39 52 27 52 55 56 29 20	55.0167740 2.6232900 48.2645880 20.3063600 19.0856240 38.3961060 31.9187160 27.2993830 38.7336450 38.9918270 53.3892900 32.0104300 54.7723290 41.1287020 16.0188500 13.3329390 36.0765640 10.0298770	147.5723000 1961.4601000 241.3539000 19.1636000 1106.3146000 1838.9826000 43.7692000 30.8711000 3067.4442000 102.3862000 598.5863000 447.0707000 951.0961000 661.1313000 1322.9256000 99.4759000 539.3844000 75.3988000	.0003 .0004 0.0000 .0003 .0003 .0003 0.0000 .0007 .0006 .0001 .0006 .0010 .0004	.0005 .0003 0.0000 .0004 .0004 .0006 .0006 .0006 .0006 .0006 .0006 .0008 .0016 .0007 .0007	.0074 .0043 .0052 .0049 .0044 .01065 .0128 .0067 .0081 .0154 .0075 .0205 .0059

								S	caled St	nd. Dev	iations	
C1 . 41.		τ.		do	Ιo	ngitı	ıde	Height	Lat.	Lon.	Ht.	
Statio			titu			(ʻ)		(m)	(")	(")	(m)	
Name	Num.	<del>(°)</del>	<del>(')</del>	(")	<u>()</u>	<u> </u>	( )	(111)			(/	
T 1 C.			06	S.359-0	11	637	8137.00	298.257				
July - Se			00				2.6218720	1961.5422000	.0002	.0003	.0045	
MCDO70	7086	30	40	37.3149310	255	5 <del>9</del>	48.2666920	241.3429000	.0002	.0002	.0023	
YARA70		-29	2	47.4111230	115	20 10	20.3061680	19.1488000	0.0000	0.0000	.0036	
GORF71	7105	39	1	14.1761210	283 239	3	19.0852780	1106.3257000	.0002	.0002	.0023	
QUIN71	7109	39	58	30.0119760	243	34	38.3951500	1838.9820000	.0002	.0002	.0028	
MOUN71	7110	32	53	30.2571770	253	32	27.2984750	30.8283000	.0002	.0003	.0030	
MAZA71	7122	23	20	34.2598910		32 44	38.7333980	3067.4857000	0.0000	.0003	.0030	
LURE72	7210	20	42	25.9808650	203	33	58.3775530	182.5806000	.0018	.0032	.0389	
ASKI75	7510	40	55	40.8638040	25	35 46	50.8750460	73.9358000	.0028	.0040	.0662	
KATV75	7512	35	57	5.4668860	27			510.5590000	.0010	.0014	.0241	
NTUA75	<i>7</i> 515	38	4	42.9329380	23	55	56.8576750	102.4207000	.0013	.0015	.0246	
ROUM75	<i>7</i> 51 <i>7</i>	35	24	15.2725610	24	41	38.9906410	476.2329000	.0017	.0022	.0325	
XRIS75	<b>7525</b>	36	47	29.2001720	21	52	39.4005610	774.3873000	.0005	.0004	.0092	
BAR 75	7530	31	43	20.6100980	35	5	18.7483370	951.3579000	.0018	.0054	.1134	
BERN78	<b>7</b> 810	46	52	38.0117150	7	27	54.7602920	661.1301000	.0006	.0007	.0093	
WETT78	7834	49	8	41.7692830	12	52	41.1293970		.0027	.0029	.0771	
GRAS78	7835	43	45	16.8785190	6	55	16.0238270	1322.7925000	.0027	.0004	.0043	
SIMO78	7838	33	34	39.7040430	135	56	13.3278650	99.4845000		.0004	.0100	
GRAZ78	7839	47	4	1.6767110	15	29	36.0786460	539,3777000	.0005	.0004	.0024	
ROYA78	7840	50	52	2.5587880	0	20	10.0315990	75.3718000	.0002 .0002	.0003	.0083	
ORRO78	7843	-35	38	10.5209830	148	56	21.5136090	1349.9627000		.0003	.0024	
AREQ79	7907	-16	27	56.6788 <b>47</b> 0	288	30	24.7496350	2492.2947000	.0002	.0003	.0042	
MATE79	7939	40	38	55.7841120	16	42	16.8504340	535.8156000	.0003	.0003	.0042	
_	_				FO 0	4	Z270127 (	00 298.257				
Octobe	er - Dec	em	ber	86 5.4	52-0		6378137.	• •	.0056	.0095	.0871	
POTS11	1181	52	22	48.9345090	13	3	55.0347710	147.7512000		.0003	.0051	
MCDO70	7086	30	40	37.3150060	255	59	2.6218600	1961.5135000	.0002	.0002	.0028	
YARA70	7090	-29	2	47.4113420	115	20	48.2657220	241.3274000		0.0002	.0020	
GORF71	7105	39	1	14.1761530	283	10	20.3059940	19.1577000	0.0000	.0002	.0032	
QUIN71	7109	39	58	30.0110530	239	3	19.0853110	1106.3243000	.0002	.0002	.0029	
MOUN71	7110	32	53	30.2563410	243	34	38.3940090	1838.9606000	.0002	.0002	.0030	
MAZA71	7122	23	20	34.2591300	253	32	27.2984770	30.8314000	.0002	.0002	.0036	
LURE72	7210	20	42	25.9810870	203	44	38.7333230	3067.4884000	0.0000	.0016	.0279	
KATV75	<i>7</i> 512	35	57	5.4647590	27	46	50.8742290	73.9088000	.0011		.2618	
XRIS75	7525	36	47	29.1980100	21	52	39,3980120	476.2277000	.0198	.0436	.0041	
<b>BAR 75</b>	7530	31	43	20.6105750	35	5	18.7501730	774.3869000	.0004	.0004	1.3183	
KIRK78	7805	60	13	2.2791580	24	23	40.3095140	79.1765000	.0189	.1133 .0024	.0202	
BERN78	<b>7</b> 810	46	52	38.0130580	7		54.7579200	951.1367000	.0007			
WETT78	7834	49	8	41.7685370	12		41.1300040	661.1001000	.0004	.0004	.0040 .0040	
GRAS78	7835	43	45	16.8769640	6		16.0245050	1322.8067000	.0004	.0003		
SIMO78	7838	33	34	39.7028270	135	56	13.3287930	99.4620000	.0003	.0004	.0034	
GRAZ78	7839	47	4	1.6758430	15		36.0766800	539,4003000	.0005	.0005	.0083	
ROYA78	7840	50	52	2.5579610				75.3487000	.0003	.0003	.0041	
ORRO78	7843	-35			148			1350.0293000	.0003	.0004	.0194	
AREQ79	7907	-16		56.6787220	288			2492.2731000	.0002	.0003	.0030 .0039	
MATE79	7939	40	38	55.7831340	16	42	16.8510020	535.8257000	.0004	.0003	.0039	

									Scaled S	tnd. Dev	riations	
Statio	n	L	atiti	ude	Lo	ngit	ude	Height	Lat.	Lon.	Ht.	
Name	Num.	(°)	(')	(")	(°)	( <u>'</u> )	(")	(m)	(")	(")	(m)	
		` '	•	,		`_					()	
_												
January	' - Ma:	rch :	87	RMS.39	95-01	(	6378137.00	298.257				
POTS11	1181	52	22	48.9346560	13	3	55.0289300	148.0603000	.0039	.0055	.0704	
MCDO70	7086	30	40	37.3157390	255	59	2.6212440	1961.4991000	.0001	.0002	.0031	
YARA70	<b>709</b> 0	-29	2	47.4122590	115	20	48.2659490	241.3247000	.0003	.0002	.0030	
GORF71	7105	39	1	14.1761560	283	10	20.3058170	19.1938000	0.0000	0.0000	.0033	
QUIN71	7109	39	58	30.0126700	239	3	19.0854830	1106.3300000	.0002	.0002	.0035	
MOUN71 MAZA71	7110 7122	32 23	53 20	30.2577930 34.2603600	243 253	34 32	38.3941960 27.2984040	1838.9553000 30.8674000	.0002 .0001	.0002	.0033	
LURE72	7210	20	42	25.9811610	203	32 44	38.7336090	3067.5323000	0.0001	.0002 .0003	.0027 .0035	
KATV75	7512	35	57	5.4575660	27	46	50.8748920	73.8637000	.0061	.0075	.0747	
BAR 75	7530	31	43	20.6075080	35	5	18.7482000	774.3789000	.0025	.0028	.0393	
BERN78	7810	46	52	38.0385520	7	27	54.7107520	951.2205000	.0096	.0211	.0125	
<b>WET178</b>	7834	49	8	41.7676200	12	52	41.1332310	661.0760000	.0005	.0006	.0086	
GRAS78	7835	43	45	16.8742680	6	55	16.0258380	1322.8046000	.0009	.0013	.0235	
SHAN78	7837	31	5	51.1517980	121	11	30.2388020	27.9356000	.0086	.0096	.1682	
SIMO78	7838	33	34	39.7015500	135	56	13.3268080	99.4763000	.0003	.0004	.0034	
GRAZ78	7839	47	4	1.6731500	15	29	36.0773310	539.4348000	.0011	.0016	.0208	
ROYA78	7840	50	52	2.5572940	0	20	10.0328300	75.3820000	.0003	.0002	.0037	
ORRO78	7843	-35	38	10.5194620	148	56	21.5158890	1349.9933000	.0016	.0019	.0962	
AREQ79	7907	-16	27	56.6780470	288	30	24.7492180	2492.2531000	.0002	.0003	.0031	
MATE79	7939	40	38	55.7830410	16	42	16.8527600	535.8125000	.0004	.0002	.0038	
April - ]	Iune 8	7	S.	.331-01	6378	3137	7.00 298.2	257				
POTS11	1181	52	22	48.9351690	13	3	55.0199330	147.9684000	.0051	.0066	.0956	
MCDO70	7086	30	40	37.3152810	255	59	2.6232070	1961.5025000	.0001	.0002	.0025	
YARA70	7090	-29	2	47.4103850	115	20	48.2690390	241.3875000	.0003	.0002	.0030	
GORF71	7105	39	1	14.1761610	283	10	20.3056170	19.1734000	0.0000	0.0000	.0028	
QUIN71	7109	39	58	30.0124110	239	3	19.0858130	1106.3246000	.0001	.0002	.0026	
MOUN71	7110	32	53	30.2576650	243	34	38.3949670	1838.9562000	.0001	.0002	.0023	
MAZA71	7122	23	20	34.2603610	253	32	27.3002750	30.8832000	.0001	.0002	.0026	
LURE72	7210	20	42	25.9817140	203	44	38.7332000	3067.4807000	0.0000	.0002	.0021	
ASKI75	7510	40	55	40.8630780	25	33	58.3778940	182.6459000	.0026	.0047	.0572	
KATV75	7512	35	57	5.4640290	27	46	50.8736380	73.9192000	.0011	.0014	.0220	
BAR 75	7530 7575	31 37	<b>43</b> 55	20.6122410	35	5	18.7481060	774.4455000	.0004	.0003	.0039	
DIYA75 MELE75	7580	37	22	12.8494310 39.5766860	40 33	11 11	41.5816760 28.5011220	724.9863000	.0016	.0022	.0288	
YOZG75	7585	39	48	1.8927660	34	48	46.8350940	1357.7628000 1677.1022000	.0010 .001 <i>7</i>	.0015 .0023	.0298 .0468	
YIGI75	7587	40	56	13.1758710	31	26	19.6567980	822.6839000	.0017	.0023	.0337	
KIRK78	7805	60	13	2.2771380	24	23	40.3745970	77.5713000	.0253	.0907	.4479	
BERN78	7810	46	52	38.0123440	7	27	54.7751230	951.0664000	.0003	.0003	.0044	
HELW78	7831	29	51	32.3977710	31	20	33.6766380	131.5884000	.0028	.0450	.1490	
WETT78	7834	49	8	41.7712770	12	52	41.1311000	661.0624000	.0004	.0004	.0073	
GRAS78	7835	43	45	16.8774210	6	55	16.0261850	1322.7531000	.0010	.0011	.0264	
SHAN78	7837	31	5	51.1398060	121	11	30.2515460	28.2503000	.0162	.0225	.3612	
SIMO78	7838	33	34	39.7033500	135	56	13.3307940	99.4364000	.0003	.0004	.0053	
GRAZ78	7839	47	4	1.6770410	15	29	36.0807700	539.4208000	.0003	.0002	.0037	
ROYA78	7840	50	52	2.5585550	0	20	10.0326000	75.3911000	.0002	.0002	.0030	
ORRO78	7843	-35	38	10.5205010	148	56	21.5158070	1350.0168000	.0003	.0004	.0182	
AREQ79	7907	-16	27	56.6778000	288	30	24.7522430	2492.2689000	.0002	.0003	.0039	
MATE79	7939	40	38	55.7854990	16	42	16.8520780	535.8166000	.0003	.0002	.0028	

<del></del>									Scaled St	nd. Dev	iations	
C4		τ.		do	Lo	ngitu	ıde	Height	Lat.	Lon.	Ht.	
Statio			titu		(°)	_	(")	(m)	(")	(")	(m)	
Name	Num.	(*) (	()	(")	( )	( )	( )	(111)				
								<b></b>				
July - Se	eptemb	er 8	37	S.345-0	1	637	8137.00	298.257				
POTS11	1181	52	22	48.9352940	13	3	55.0262830	147.8964000	.0034	.0056	.0503 .0028	
MCDO70	7086	30	40	37.3147010	255	59	2.6226520	1961.5134000	.0001 .0003	.0002 .0002	.0026	
YARA70		-29	2	47.4103740	115	20	48.2636150	241.4319000 19.15 <b>79</b> 000	0.0000	0.0000	.0027	
GORF71	7105	39	1	14.1761830	283 239	10 3	20.3054370 19.0857940	1106.3076000	.0001	.0002	.0024	
QUIN71	710 <del>9</del> 7110	39 32	58 53	30.0115180 30.2569460	243	34	38.3941410	1838.9543000	.0001	.0002	.0022	
MOUN71 MAZA71	7122	23	20	34.2589850	253	32	27.2993630	30.8944000	.0002	.0002	.0034	
HUAH71		-16	44	.6685260	208	57	31.9172790	45.2972000	.0003	.0003	.0055 .0026	
LURE72	7210	20	42	25.9822540	203	44	38.7327150	3067.4703000	0.0000	.0002 .0013	.0026	
ASKI75	7510	40	55	40.8670560	25	33	58.3795440	182.5744000 510.5391000	.0008 .0008	.0013	.0164	
NTUA75	7515	38	4	42.9327290	23	55 41	56.8604020 38.9934060	102.3683000	.0008	.0011	.0218	
ROUM75	7517 7505	35 36	24 47	15.2739260 29.1989100	24 21	41 52	39.4042730	476.1254000	.0027	.0048	.0799	
XRIS75	7525 7530	<i>3</i> 6	43	20.6119310	35	5	18.7522080	774.3838000	.0003	.0003	.0033	
BAR 75 LAMP75	7544	35	31	3.9305170	12	34	2.7878800	111.8783000	.0024	.0030	.0477	
YOZG75	7585	39	48	1.8880630	34	48	46.8338530	1677.2857000	.0065	.0129	.1907	
YIGI75	7587	40	56	13.1751740	31	26	19.6561530	822.6676000	.0022	.0039 .0003	.0589 .0033	
BERN78	7810	46	52	38.0137460	7	27	54.7753750	951.0202000	.0003 .0013	.0024	.0285	
HELW78	7831	29	51	32.4131880	31	20	33.7192480	131.8324000 661.0889000	.0003	.0003	.0032	
WETT78	7834	49	8	41.7702190	12 6	52 55	41.1330620 16.0281780	1322.7394000	.0036	.0043	.1021	
GRAS78	7835	43	45 34	16.8790030 39.7042400	135	56	13.3324800	99.3637000	.0002	.0004	.0036	
SIMO78 GRAZ78	7838 7839	33 47	34 4	1.6780510	15	29	36.0806610	539.3663000	.0003	.0003	.0033	
ROYA78	7840	50	52	2.5595170	0	20	10.0323950	75.3644000	.0002	.0002	.0030	
ORRO78	7843	-35	38	10.5201100	148	56	21.5128470	1349.9272000	.0002	.0003	.0157	
AREQ79	7907	-16	27	56.6788200	288	30	24.7506450	2492.2545000	.0001	.0002 .0002	.0026 .0025	
MATE79	7939	40	38	55.7865200	16	42	16.8526500	535.8081000	.0003	.0002	.0023	
Octobe	er - Dec	em	ber	87 RM	S.36	3-01	637813	37.00 <b>29</b> 8.5	257			
POTS11	1181	52	22	48.9349000	13	3	55.0244640	147.8518000	.0032	.0048	.0510	
MCDO70	7086	30	40	37.3144480	255	59	2.6211760	1961.5033000	.0001	.0002	.0028 .0037	
YARA70	7090	-29	2	47.4118440	115	20	48.2673770	241.3075000	.0003	.0002 .0003	.0037	
EAST70	7097	-27	8	52.1459650	250	36	59.1557 <b>43</b> 0 20.3052800	117.5281000 19.1600000	0.0002	0.0000	.0031	
GORF71	7105	39	1	14.1762080	283 239	10 3	19.0845670	1106.3291000	.0001	.0002	.0036	
QUIN71	7109	39 32	58 53	30.0112370 30.2576280	243	34	38.3934010	1838.9217000	.0001	.0002	.0030	
MOUN71 MAZA71	7110 7122	23	20	34.2589700	253	32	27.2978380	30.8650000	.0001	.0002	.0027	
HUAH71	7123	-16	44	6603550	208	57	31.9130400	45.5819000	.0006	.0007	.0110	
LURE72	7210	20	42	25.9823490	203	44	38.7303190	3067.5188000	0.0000		.0029	
NTUA75	7515	38	4	42.9310810	23	55	56.8585720	510.5534000	.0013	.0019 .0014	.0280 .0207	
ROUM75	7517	35	24	15.2728880	24	41	38.9937290	102.3779000 476.1499000	.0010	.0014	.0210	
XRIS75	7525	36	47	29.1995530	21	52	39.4020030	774.3862000	.0005	.0003	.0051	
BAR 75	7530	31	43	20.6132370	35 12		18.7501210 2.7880250	111.8925000	.0012	.0017	.0237	
LAMP75	7544 7810	35 46		3.9296790 38.0137090	7		54.7743310	951.0608000	.0004	.0004	.0055	
BERN78 WETT78	7834	49		41.7703010	12		41.1321460	661.0953000	.0003		.0041	
GRAS78	7835	43		16.8779500	6		16.0268100	1322.8790000	.0008		.0174	
SIMO78	7838	33		39.7018470	135		13.3291280	99.4344000	.0003		.0033	
GRAZ78	7839	47	4				36.0790260	539,3916000	.0004 .0003		.0043	
ROYA78	7840	50						75.3732000 1350.3110000	.0021		.1795	
ORRO78	7843				148 288			2492.2612000	.0021		.0035	
AREQ79	7907 7939	-16 40						535.8229000	.0004		.0035	
MATE79	/939	40	30	33.7030330	**	, 12	.0.0022000					

									Scaled S	tnd. Dev	<i>r</i> iations	
Statio	n	L	.atiti	ude	Lo	ngi	tude	Height	Lat.	Lon.	Ht.	
Name	Num.	(°)	(')	(")		_	(")	(m)	(")	(")	(m)	
			<del>`</del>			` ′		(111)			(111)	
January	- Ma	rch	88	RMS.30	7-01		6378137.0	00 298.257				
POTS11	1181	52	22	48.9354770	13	3	55.0258290	147.7713000	.0039	.0057	.0609	
CUBA19	1953	20	0	42.9998150	284	14	15.9783280	18.2278000	.0058	.0446	.4893	
MLRS70	7080	30	40	48.9673170	255	59	5.2890420	2004.2926000	.0007	.0008	.0157	
MCDO70	7086	30	40	37.3152100	255	59	2.6222500	1961.4811000	.0002	.0003	.0032	
YARA70	7090	-29	2	47.4113380	115	20	48.2677780	241.3345000	.0002	.0002	.0023	
EAST70	7097	-27	8	52.1445750	250	36	59.1564480	117.5087000	.0002	.0003	.0040	
GORF71	7105	39	1	14.1762100	283	10	20.3051400	19.1258000	0.0000	0.0000	.0031	
QUIN71	7109	39	58	30.0120800	239	3	19.0844240	1106.3160000	.0002	.0002	.0025	
MOUN71	7110	32	53	30.2583760	243	34	38.3917760	1838.9413000	.0001	.0002	.0023	
MAZA71	7122	23	20	34.2595060	253	32	27.2982320	30.8596000	.0002	.0002	.0022	
LURE72	7210	20	42	25.9828000	203	44	38.7306000	3067.4912000	0.0000	.0003	.0027	
BARS72	7288 7205	35 25	19	52.4516500	243	6	30.5178940	896.1475000	.0021	.0032	.0594	
RICH72 PUNT75	7295 7545	39	36	48.0826960	279	36	57.1835890	-22.9296000	.0089	.0066	.1443	
BERN78	7810	46	8 52	7.7762980 38.0114550	8 7	58 27	22.7430330 54.7639020	229.9786000	.0011	.0016	.0200	
WETT78	7834	49	8	41.7699100	12	52	41.1335110	951.2734000	.0013	.0043	.0819	
GRAS78	7835	43	45	16.8769620	6	55	16.0261990	661.0874000 1322.8675000	.0004 .0006	.0005 .0007	.0049	
SIMO78	7838	33	34	39.7009690	135	56	13.3290790	99.3896000	.0003	.0007	.0123 .0040	
GRAZ78	7839	47	4	1.6769530	15	29	36.0803060	539.3584000	.0003	.0003	.0037	
ROYA78	7840	50	52	2.5593550	0	20	10.0330090	75.3963000	.0002	.0003	.0027	
UNKN78	7844	27	5	30.3754580	142	13	.3635160	262.8173000	.0037	.0050	.0804	
AREQ79	7907	-16	27	56.6796810	288	30	24.7513360	2492.2460000	.0002	.0003	.0037	
MATE79	7939	40	38	55.7852890	16	42	16.8533350	535.8233000	.0003	.0003	.0035	
April - J	une 8	8	RN	<b>4</b> S.273-01	6	378	137.00	298.257				
POTS11	1181	52	22	48.9366240	13	3	55.0158090	147.8604000	.0035	.0115	.2038	
CUBA19	1953	20	0	42.9398470	284	14	16.0068960	18.5921000	.0626	.0089	.2728	
MLRS70	7080	30	40	48.9666650	255	59	5.2884530	2004.3162000	.0011	.0012	.0222	
YARA70	7090	-29	2	47.4078380	115	20	48.2679600	241.3661000	.0003	.0002	.0034	
GORF71	7105	39	1	14.1762350	283	10	20.3049670	19.1929000	0.0000	0.0000	.0031	
QUIN71	7109	39	58	30.0122470	239	3	19.0837160	1106.3479000	.0001	.0002	.0030	
MOUN71	7110	32	53	30.2583200	243	34	38.3919130	1838.9982000	.0001	.0002	.0026	
MAZA71	7122	23	20	34.2582650	253	32	27.2985710	30.9126000	.0002	.0003	.0038	
HUAH71	7123	-16	44	.6631090	208	57	31.9161460	45.3888000	.0013	.0014	.0337	
LURE72	7210	20	42	25.9829810	203	44	38.7292100	3067.5506000	0.0000	.0002	.0025	
BARS72	7288	35	19	52.4520690	243	6	30.5197690	896.1775000	.0007	.0010	.0147	
RICH72	7295	25	36	48.0744720	279	36	57.1865670	-22.7375000	.0009	.0012	.0186	
BOLO75 BERN78	7546 7810	44 46	31 52	12.1178980	11	38	47.3479640	49.4725000	.0024	.0044	.0373	
				38.0104610	7	27	54.7719100	951.0231000	.0003	.0004	.0064	
BORO78 WETT78	7811 7834	52 49	16 8	37.1458270 41.7669070	17 12	4 52	28.4438520	123.6441000	.0093	.0177	.3584	
GRAS78	7835	43	45	16.8750000	6	52 55	41.1313360 16.0242830	661.1157000	.0004	.0005	.0081	
SHAN78	7837	31	43 5	51.1429720	121	55 11	30.2305280	1322.8427000 27.8711000	.0006	.0010	.0140	
SIMO78	7838	33	34	39.7036560	135	56	13.3271160	99.4131000	.0061 .0003	.0095 .0004	.0978	
GRAZ78	7839	47	4	1.6749650	155	29	36.0751560	539.5057000	.0003	.0004	.0053 .0157	
ROYA78	7840	50	52	2.5579290	0	20	10.0302200	75.3939000	.0004	.0002	.0037	
CABO78	7882	22	55	3.1846130	250	8	8.0619510	111.5571000	.0007	.0002	.0171	
AREQ79	7907	-16	27	56.6783710	288	30	24.7492630	2492.2678000	.0001	.0003	.0026	
MATE79	7939	40	38	55.7828380	16	42	16.8515280	535.8619000	.0003	.0002	.0034	
KOOT88	8833	52	10	41.4413520	5	48	36.5967640	88.6341000	.0139	.0608	.1364	

Name   Num. (*) (*) (*) (*) (*) (*) (*) (*) (*) (*)													
Station   Latitude   Longitude   Height   Lat.   Lon.   Ht.									S	caled St	nd. Devi	iations	
Name   Num. (*) (*) (*) (*) (*) (*) (*) (*) (*) (*)	C4 41-		т.		da	Loi	noiti	ıde					
July - September 88									_			(m)	
POTS11	Name	Num.	(°) (	<u>.,                                    </u>	(")	(-)	<u> </u>	( )	(111)			<u> </u>	
POTS11													
POTS11	July - So	ntemb	er 8	88	RMS.26	5-01	(	6378137.00	298.257				
CTAINTO   1785   32   36   2.4530180   243   9   32.9526440   988.6504000   .0006   .0009   .00185     MLRST   7080   30   48.9661840   255   95   5.2883900   .2004.3457000   .0013   .0012   .0317     MLRST   7080   29   2   47.4085480   255   95   5.2883900   .2004.3457000   .0002   .0002   .0006     MARATO   7090   42   37   21.701270   283   30   44.895350   29.2883000   .0000   .0000   .0006   .0007     MARATO   7109   39   1   14.1762740   283   10   20.3047460   19.1895000   .0000   .0000   .0002   .0007     QUINTI   7110   39   83   30.12230   239   31   19.883620   1106.3573000   .0001   .0002   .0002   .0002     QUINTI   7110   32   33   30.2587820   243   34   38.3914380   1839.000600   .0001   .0002   .0002   .0002   .0002   .0002   .0002   .0003   .0			50	22					147.7627000	.0035			
MILESTO   7080   30   40   44 9660480   255   59   5.2883900   2004.3457000   .0013   .0012   .0012			30	36									
TARA70							59	5.2883900					
HAYS70			-29	2	47.4085480								
GOR77 7105 39 1 14/102/39 239 3 19.0838c20 1106.3573000 0001 00022 0022 0010NO1N71 7110 32 53 30.2587820 248 34 33.3914380 1839.0006000 0001 0002 00022 0010NO1N71 7110 32 53 30.2587820 248 34 33.3914380 1839.0006000 0001 0002 0003 0005 0016 0017 0017 0017 0017 0017 0017 0017													
QUIN71 7109 39 58 30.012293 259 36 78.055502 243 34 38.3914380 1839.0006000 .0001 0.0022 .0022 .000171 7110 32 53 30.2587820 243 34 38.3914380 1839.0006000 .0001 0.0002 .0022 .0033 .0055 .0024 .0037 .0038 .0038													
MOUN71													
MAZA71 7122 22 03 42-614710 233 22 77-2965580 30.8957000 .0002 .0003 .0055												.0136	
HUAHTI 7123 -16 44 5631990 208 57 31.9154850 45.3848000 .0017 .0022 .0017													
Current										.0017			
RICH72 795 25 36 48 0761510 279 36 57.1869080									3067.5453000	0.0000			
BERN78 7810 46 52 38.0105530 7 27 54.7742030 951.0087000 .00026 .0038 .0352 BORO78 7811 52 16 37.1204710 17 4 28.4632200 12.27768000 .0026 .0038 .0352 WETT78 7834 49 8 41.7675200 12 52 41.1327540 661.1344600 .0030 .0002 .0032 .0032 .0034 .0035 .0038 .00352 .0036 .0037 .0038 .00352 .0036 .0037 .0038 .00352 .0036 .0037 .0038 .00352 .0036 .0038 .00352 .0036 .0036 .0038 .00352 .0036 .0036 .0038 .00352 .0036 .0036 .0038 .00352 .0036			25					57.1869080					
BORO78 7811 52 16 37.1204710 17 4 28.4632200 122.7768000 .0003 .0002 .0032 CRAS78 7834 49 8 41.7657500 12 52 41.327540 66.1346000 .0003 .0002 .0032 CRAS78 7835 43 45 16.8751620 6 55 16.0243960 1322.850200 .0004 .0005 .0080 SHAN78 7838 33 34 39.7031680 135 56 13.3274610 99.4613000 .0002 .0033 .0039 SIMO78 7838 33 34 39.7031680 135 56 13.3274610 99.4613000 .0002 .0033 .0039 CRAZ78 7839 47 4 1.6750190 15 29 36.0787690 539.4099000 .0003 .0002 .0002 .0029 CROYA78 7840 50 52 2.5573790 0 20 10.0368200 75.3899000 .0003 .0002 .0029 CROYA78 7840 50 52 2.5573790 0 20 10.0368200 75.3899000 .0002 .0002 .0029 CROYA78 7842 22 55 3.1863510 250 8 8.099690 111.5382000 .0002 .0022 .0029 CROYA78 7842 22 55 3.1863510 250 8 8.099690 111.5382000 .0002 .0022 .0021 .0475 CABC78 7882 22 55 3.1863510 250 8 8.099690 111.5382000 .0002 .0002 .0024 MATE79 7939 40 38 55.7825550 16 42 16.8519230 535.8883000 .0003 .0002 .0024 MATE79 7939 40 38 55.7825550 16 42 16.8519230 535.8883000 .0003 .0002 .0024 MATE79 7939 40 38 55.7825550 16 42 16.8519230 535.8883000 .0003 .0002 .0024 MATE79 7939 40 39 55.7825550 16 42 16.8519230 535.8883000 .0003 .0002 .0024 MATE79 7939 40 39 55.7825550 16 42 16.8519230 535.8883000 .0003 .0002 .0024 MATE79 7939 40 39 55.7825550 16 42 16.8519230 535.8883000 .0003 .0002 .0024 MATE79 7939 40 39 55.7825550 16 42 16.8519230 535.883000 .0003 .0002 .0024 MATE79 7939 40 40 48.9663840 255 59 5.2894060 .0004 .0002 .0004 .0002 .0004 MATE79 7930 40 48.9663840 255 59 5.2894060 .0004 .0002 .0004 .0003 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0004 .0002 .0002 .0004 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0							27						
WETT78 7834 49 8 4 1.7675200 12 52 41.1327540 681.1349000 .003 .0003 .0003 .0003 .0005 .0080 GRA578 7835 34 55 16.8751620 6 55 16.0243960 1322.850200 .0004 .0005 .0080 SIMANT8 7837 31 5 51.1502870 121 11 30.2384810 27.8385000 .0051 .0037 .0696 SIMANT8 7838 33 34 39.7031680 135 56 13.3274610 99.4613000 .0002 .0003 .0003 .0003 .0003 .0003 .0004 .0005 .0004 .0005 .0008					37.1204710	17							
SHAN78 7837 31 5 511502870 121 11 30.2384810 27.885000 .0051 .0037 .0696 SHAN78 7837 33 5 511502870 121 11 30.2384810 27.885000 .0051 .0037 .0696 SHAN78 7838 33 34 39.7031680 135 56 13.3274610 99.4613000 .0002 .0002 .0002 .0002 SRAZ78 7840 50 52 2.5573790 0 20 10.0308200 75.3899000 .0002 .0002 .0002 .0002 SROYA78 7840 50 52 2.5573790 0 20 10.0308200 75.3899000 .0002 .0002 .0002 .0002 SROYA78 7843 -35 38 10.5216730 148 56 21.5107020 1350.1112000 .0031 .0047 .2352 CABO78 7882 22 55 3.1863510 250 8 8.0599690 .111.5382000 .0002 .0002 .0002 MATEP 7907 -16 27 56.6781370 288 30 24.7487730 .2492.2262000 .0001 .0002 .0024 MATEP 7939 40 38 55.7825550 16 42 16.8519230 535.8883000 .0003 .0002 .0028 KOOT88 8833 52 10 41.4406360 5 48 36.5896520 88.690000 .0009 .0015 .0147   **October - December 88 RMS.376-01 6378137.00 298.257  POTS11 1181 52 22 48.9260460 13 3 55.0292540 147.7013000 .0038 .0062 .0069 RICA18 1884 56 56 54.7684590 24 3 32.6535510 30.0543000 .0003 .0003 .0001 .004 CUBA19 1953 20 0 42.9862560 284 14 16.0008180 17.8324000 .0018 .0015 .0319 MLRS70 7080 30 40 48.9663840 .255 59 5.2894060 2004.3095000 .0006 .0008 .0142 YARA70 7090 -29 2 47.4601630 115 20 48.2683530 17.8324000 .0018 .0015 .0319 MLRS70 7091 42 37 21.6998740 288 30 44.4900800 92.1970000 .0004 .0002 .0044 YARA70 7097 -27 8 52.1887160 .250 36 59.1112380 116.9922000 .0004 .0067 .2085 CORF71 7105 39 11 41.762990 .283 10 20.045360 119.0274000 .0000 .0000 .0003 QUIN71 7110 32 53 30.2584270 .293 31 19.0835690 1106.3936000 .0002 .0002 .0003 GUIN71 7110 32 53 30.2584270 .293 31 19.0835690 1106.3936000 .0002 .0003 .0044 BORO78 7811 52 16 37.1005420 12 52 41.3107190 661.1970000 .0001 .0004 .0005 CRAS78 7838 33 34 39.7006420 135 56 16.0257800 .309577000 .0004 .0003 .0004 GRAS78 7838 33 34 39.7006420 135 56 16.0257800 .30957000 .0004 .0003 .0004 GRAS78 7838 33 34 39.7006420 135 56 16.0257800 .30957000 .0004 .0003 .0004 GRAS78 7840 50 52 2.5583640 0 20 10.0307990 753773000 .0004 .0003 .0004 GRAS78 7840 50 52 2.5583640 0 20 10.0307990 753773000 .0004 .0003 .0004 GRA			49	8	41.7675200								
SHAN78 7837 31 5 31.192470 121 11 10.305207 39.4613000 .0002 .0003 .0003 .0009 SIMO78 7838 33 34 39.7031680 135 56 13.3274610 99.4613000 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .0002 .00007 .0000 .0000 .0000 .0002 .0002 .0002 .0000	GRAS78		43										
SIMO78 7889 37 44 1.6750190 15 29 36.0787690 539.4995000 .0003 .0002 .0029 ROYA78 7840 50 52 2.5573790 0 20 10.0306200 75.3899000 .0002 .0													
ROYA78 7849 50 52 2.5573790 0 20 10.0308200 75.3899000 .0002													
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16. Abstract

Laser ranging measurements to the LAGEOS satellite from 1976 through 1989 are related via geodetic and orbital theories to a variety of geodetic and geodynamic parameters. This document explains the SL7.1 analyses of this data set including the estimation process for geodetic parameters such as the Earth's gravitational constant (GM), those describing the Earth's elasticity properties (Love numbers), and the temporally varying geodetic parameters such as Earth orientation (polar motion and  $\Delta$ UT1) and tracking site horizontal tectonic motions. Descriptions of the reference systems, tectonic models, and adopted geodetic constants are provided; these are the framework within which the SL7.1 solution takes place. Estimates of temporal variations in non-conservative force parameters are included in these SL7.1 analyses as well as parameters describing the orbital states at monthly epochs. This information is useful in further refining models used to describe close-Earth satellite behavior. Estimates of intersite motions and individual tracking site motions computed through a network adjustment scheme are given. Tabulations of tracking site eccentricities, data summaries, estimated monthly orbital and force model parameters, polar motion, Earth rotation, and tracking station coordinate results are provided as appendices.

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